

**TEACH-IN
2004
PART 1 INSIDE**

THE No.1 MAGAZINE FOR ELECTRONICS TECHNOLOGY & COMPUTER PROJECTS

EVERYDAY

Vol.32 No.11

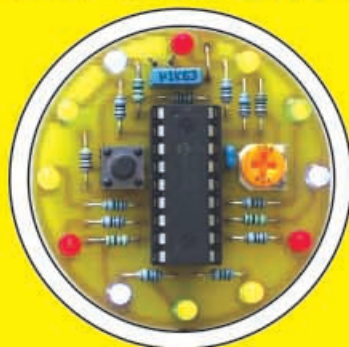
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TEACH-IN 2004

**A hands-on
introduction
to electronics**



PIC RANDOM L.E.D. FLASHER

**Christmas and
party decoration**

CARDBOARD CLOCK

**An inexpensive
novel timepiece**



PLUS

PRACTICAL RADIO CIRCUITS - 6



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ISSN 0262 3617

PROJECTS ... THEORY ... NEWS ...
COMMENTS ... POPULAR FEATURES ...

VOL. 32. No. 11 NOVEMBER 2003

Cover illustration by jgr22



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Our December 2003 issue will be published on Thursday, 13 November 2003. See page 731 for details

EVERYDAY **PRACTICAL ELECTRONICS**

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NEXT MONTH

CHRISTMAS CHEEKS

A Christmas, disco or party project with a difference! Instead of enhancing your Christmas decorations, it is designed to enhance . . . you! With recent advances in semiconductor technology, the maximum luminous intensity of red l.e.d.s has increased to several candelas. Now consider that human flesh is translucent to red light. Combine these two facts, and we have the basis for this project. The average facial cheek has a thickness of between one and two centimetres, and this makes it possible to "backlight" a cheek from the gums with a high intensity l.e.d., causing it to glow in the subdued light of a Christmas party or disco etc. The slimline circuit featured in this article is slipped between the gums and cheek, and is activated by the presence of saliva. Just think of the attention you will attract with flashing cheeks!



PIC NIM MACHINE

An ultra-modern version of the age-old game of NIM. There have been many electrical or electronic versions of NIM over the years since the Nimatron was demonstrated at the New York Trade Fair in 1940. This PIC-based project is simple to build, easy to play and has a switched range of difficulty levels from easy-to-beat to nigh-on-impossible-to-beat. It should keep everyone fascinated for hours at Christmas.

VIRUS ZAPPER Mk2

Imagine, if you will, a simple battery-operated device capable of stopping the common cold and many other afflictions in their tracks. At the onset of a sore throat, say, the user would simply grasp a pair of electrodes, switch on, and in no time become perfectly well again. Sounds like an impossible pipedream, doesn't it. Yet this is the claim for the Clark Virus Zapper, versions of which are widely available from internet sources. Many enthusiasts swear by its effectiveness, so it's just possible it does work, at least for some users. The Virus Zapper is the invention of Dr. Hulda Regehr Clark, an American lady who claims it can destroy all manner of viruses, bacteria and parasites within the body. This project is an updated and improved development of the Virus Zapper we published in the March '02 issue which proved to be very popular with readers. Build it and judge the results for yourself.

PLUS

TEACH-IN 2004 – PART 2
RADIO CIRCUITS – PART 7: THE SUPERHET

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Programmer Accessories:

40-pin Wide ZIF socket (ZIF40W) £15.00

18VDC Power supply (PSU201) £5.95

Leads: Parallel (LEAD108) £4.95 / Serial (LEAD76) £4.95 / USB (LEADUAA) £2.95

NEW! USB 'All-Flash' PIC Programmer

USB PIC programmer for all 'Flash' devices. No external power supply making it truly portable. Supplied with box and Windows Software. ZIF Socket and USB Plug A-A lead not incl.

Kit Order Code: 3128KT – £29.95

Assembled Order Code: AS3128 – £39.95



Enhanced "PICALL" ISP PIC Programmer



Will program virtually ALL 8 to 40 pin PICs plus certain ATMEL AVR, SCENIX SX and EEPROM 24C devices. Also supports In System

Programming (ISP) for PIC and ATMEL AVR's. Free software. Blank chip auto detect for super fast bulk programming. Requires a 40-pin wide ZIF socket (not included)

Kit Order Code: 3144KT – £54.95

Assembled Order Code: AS3144 – £59.95

ATMEL 89xxx Programmer

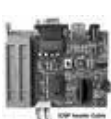
Uses serial port and any standard terminal comms program. 4 LEDs display the status. ZIF sockets not included. Supply: 16VDC.

Kit Order Code: 3123KT – £29.95

Assembled Order Code: AS3123 – £34.95



NEW! USB & Serial Port PIC Programmer



USB/Serial connection. Header cable for ICSP. Free Windows software. See website for PICs supported. ZIF Socket and USB Plug A-A lead extra. 18VDC.

Kit Order Code: 3149KT – £27.95

Assembled Order Code: AS3149 – £44.95

Introduction to PIC Programming

Go from a complete PIC beginner to burning your first PIC and writing your own code in no time!

Includes a 49-page step-by-step Tutorial Manual, Programming Hardware (with LED bench testing section), Win 3.11-XP Programming Software (will Program, Read, Verify & Erase), and a rewritable PIC16F84A that you can use with different code (4 detailed examples provided for you to learn from). Connects to PC parallel port.

Kit Order Code: 3081KT – £14.95

Assembled Order Code: AS3081 – £24.95



ABC Mini Microcontroller Board

Currently learning about microcontrollers? Need to do more than flash a LED or sound a buzzer?

The ABC Mini Starter Kit is based on ATMEL's AVR 8535 RISC technology and will interest both the beginner and expert alike.

Beginners will find that they can write and test a simple program, using the BASIC programming language, within an hour or two of connecting it up. Experts will like the power and flexibility of the ATMEL microcontroller, as well as the ease with which the board can be "designed-in" to a project.

The ABC Mini STARTER PACK includes everything you need to get up and experimenting right away. On the hardware side, there's a pre-assembled ABC Mini Board with parallel and serial cables for connection to your PC. Windows software included on CD-ROM features an Assembled, BASIC compiler and in-system programmer. Order Code ABCMINISP – £49.95

The ABC Mini boards only can also be purchased separately at £29.95 each.



ABC Mini Starter Pack

Controllers & Loggers

Here are just a few of the controller and data acquisition and control units we have.

See website for full details. Suitable PSU for all units: Order Code PSU203 – £9.95

Rolling Code 4-Channel UHF Remote

State-of-the-Art. High security.

4 channels. Momentary or latching relay output. Range up to 40m. Up to 15 TXs can be learned by one Rx (kit includes one Tx but more available separately).

4 indicator LEDs.

Rx: PCB 77x85mm, 12VDC/6mA (standby). Two & Ten Channel versions also available.

Kit Order Code: 3180KIT – £41.95

Assembled Order Code: AS3180 – £49.95



Computer Temperature Data Logger



Serial port 4-channel temperature logger. °C or °F. Continuously logs up to 4 separate sensors located 200m+ from board. Wide range of free software applications for storing/using data. PCB just 38x38mm. Powered

by PC. Includes on DS1820 sensor and four header cables.

Kit Order Code: 3145KT – £22.95

Assembled Order Code: AS3145 – £29.95

Additional DS1820 Sensors – £3.95 each

NEW! DTMF Telephone Relay Switcher

Call your phone number using a DTMF phone from anywhere in the world and remotely turn on/off any of the 4 relays as desired. User settable

Security Password, Anti-Tamper, Rings to Answer, Auto Hang-up and Lockout. Includes plastic case. 130 x 110 x 30mm.

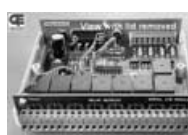
Power: 12VDC.

Kit Order Code: 3140KT – £39.95

Assembled Order Code: AS3140 – £59.95



Serial Port Isolated I/O Module



Computer controlled 8-channel relay board. 5A mains rated relay outputs and 4 opto-isolated digital inputs (for monitoring switch states, etc). Useful in a

variety of control and sensing applications. Programmed via serial port (use our new Windows interface, terminal emulator or batch files). Serial cable can be up to 35m long. Once programmed, unit can operate without PC. Includes plastic case 130 x 100 x 30mm. Power: 12VDC/500mA.

Kit Order Code: 3108KT – £54.95

Assembled Order Code: AS3108 – £64.95

Infra-red RC 12-Channel Relay Board



Control 12 on-board relays with included infra-red remote control unit. Toggle or momentary. 15m+ range. 112 x 122mm.

Supply: 12VDC/0.5A.

Kit Order Code: 3142KT – £41.95

Assembled Order Code: AS3142 – £59.95

PC Data Acquisition & Control Unit

Monitor and log a mixture of analogue and digital inputs and control external devices via the analogue and digital outputs. Monitor pressure, temperature, light intensity, weight, switch state, movement, relays, etc. with the appropriate sensors (not supplied). Data can be processed, stored and the results used to control devices such as motors, sirens, relays, servo motors (up to 11) and two stepper motors.



Features

- 11 Analogue Inputs – 0-5V, 10 bit (5mV/step)
- 16 Digital Inputs – 20V max. Protection 1K in series, 5-1V Zener
- 1 Analogue Output – 0-2.5V or 0-10V. 8 bit (20mV/step)
- 8 Digital Outputs – Open collector, 500mA, 33V max
- Custom box (140 x 110 x 35mm) with printed front & rear panels
- Windows software utilities (3-1 to XP) and programming examples
- Supply: 12V DC (Order Code PSU203)

Kit Order Code: 3093KT – £69.95

Assembled Order Code: AS3093 – £99.95

Most items are available in kit form (KT suffix) or pre-assembled and ready for use (AS prefix).

Hot New Kits This Summer!

Here are a few of the most recent kits added to our range. See website or join our email Newsletter for all the latest news.

NEW! EPE Ultrasonic Wind Speed Meter



Solid-state design wind speed meter (anemometer) that uses ultrasonic techniques and has no moving parts and does not need

calibrating. It is intended for sports-type activities, such as track events, sailing, hang-gliding, kites and model aircraft flying, to name but a few. It can even be used to monitor conditions in your garden. The probe is pointed in the direction from which the wind is blowing and the speed is displayed on an LCD display.

Specifications

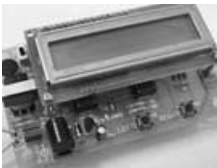
- Units of display: metres per second, feet per second, kilometres per hour and miles per hour
- Resolution: Nearest tenth of a metre
- Range: Zero to 50mph approx.

Based on the project published in Everyday Practical Electronics, Jan 2003. We have made a few minor design changes (see web site for full details). Power: 9VDC (PP3 battery or Order Code PSU203).

Main PCB: 50 x 83mm.

Kit Order Code: 3168KT – £34.95

NEW! Audio DTMF Decoder and Display



Detects DTMF tones via an on-board electret microphone or direct from the phone lines through an audio transformer. The

numbers are displayed on a 16-character, single line display as they are received. Up to 32 numbers can be displayed by scrolling the display left and right. There is also a serial output for sending the detected tones to a PC via the serial port. The unit will not detect numbers dialled using pulse dialling. Circuit is microcontroller based.

Supply: 9-12V DC (Order Code PSU203).

Main PCB: 55 x 95mm.

Kit Order Code: 3153KT – £17.95

Assembled Order Code: AS3153 – £29.95

NEW! EPE PIC Controlled LED Flasher



This versatile PIC-based LED or filament bulb flasher can be used to flash from 1 to 160

LEDs. The user arranges the LEDs in any pattern they wish. The kit comes with 8 superbright red LEDs and 8 green LEDs. Based on the Versatile PIC Flasher by Steve Challinor, EPE Magazine Dec '02. See website for full details. Board Supply: 9-12V DC. LED supply: 9-45V DC (depending on number of LED used). PCB: 43 x 54mm.

Kit Order Code: 3169KT – £10.95

Most items are available in kit form (KT suffix) or assembled and ready for use (AS prefix)

FM Bugs & Transmitters

Our extensive range goes from discreet surveillance bugs to powerful FM broadcast transmitters. Here are a few examples. All can be received on a standard FM radio and have adjustable transmitting frequency.

MMTX' Micro-Miniature 9V FM Room Bug



Our best selling bug! Good performance. Just 25 x 15mm. Sold to detective agencies worldwide. Small enough to hide just about anywhere.

Operates at the 'less busy' top

end of the commercial FM waveband and also up into the more private Air band.

Range: 500m. Supply: PP3 battery.

Kit Order Code: 3051KT – £8.95

Assembled Order Code: AS3051 – £14.95

HPTX' High Power FM Room Bug

Our most powerful room bug.

Very Impressive

performance. Clear and stable output signal thanks to the extra circuitry employed.

Range: 1000m @ 9V. Supply: 6-12V DC (9V PP3 battery clip supplied). 70 x 15mm.

Kit Order Code: 3032KT – £9.95

Assembled Order Code: AS3032 – £17.95

MTTX' Miniature Telephone Transmitter



Attach anywhere along phone line. Tune a radio into the signal and hear

exactly what both parties are saying.

Transmits only when phone is used. Clear, stable signal. Powered from phone line so completely maintenance free once installed. Requires no aerial wire – uses phone line as antenna. Suitable for any phone system worldwide. Range: 300m. 20 x 45mm.

Kit Order Code: 3016KT – £7.95

Assembled Order Code: AS3016 – £13.95

4 Watt FM Transmitter



Small, powerful FM transmitter. Audio preamp stage and three RF stages deliver 4 watts of RF power. Can be used with the electret

microphone supplied or any line level audio source (e.g. CD or tape OUT, mixer, sound card, etc). Aerial can be an open dipole or Ground Plane. Ideal project for the novice wishing to get started in the fascinating world of FM broadcasting. 45 x 145mm.

Kit Order Code: 1028KT – £22.95

Assembled Order Code: AS1028 – £34.95

25 Watt FM Transmitter

Four transistor based stages with a Philips BLY89 (or equivalent) in the final stage. Delivers a mighty 25 Watts of RF power. Accepts any line level audio source (input sensitivity is adjustable). Antenna can be an open dipole, ground plane, 5/8, J, or YAGI configuration. Supply 12-14V DC, 5A. Supplied fully assembled and aligned – just connect the aerial, power and audio input. 70 x 220mm.

Order Code: 1031M – £124.95



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Order Code EPL500 – £149.95

30, 130-200 and 300-in-1 project labs also available – see website for details.



Number 1 for Kits!

With over 300 projects in our range we are the UK's number 1 electronic kit specialist. Here are a few other kits from our range.

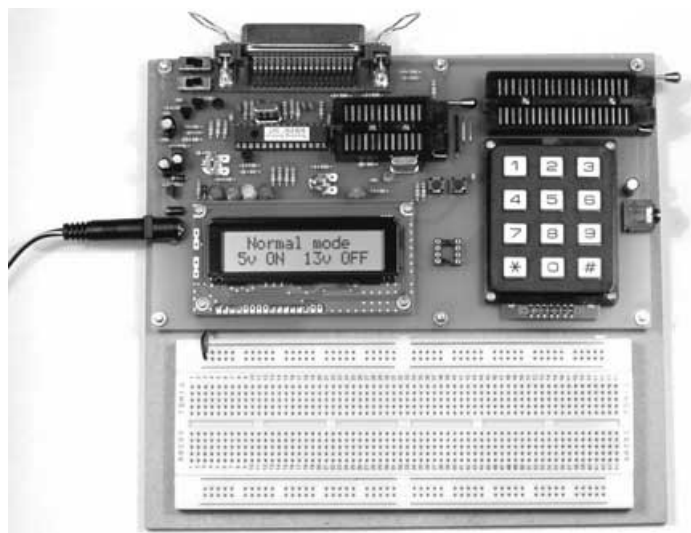
- 1046KT – 25W Stereo Car Booster £26.95
- 3087KT – 1W Stereo Amplifier £4.95
- 3105KT – 18W BTL mono Amplifier £9.95
- 3106KT – 50W Mono Hi-fi Amplifier £19.95
- 3143KT – 10W Stereo Amplifier £9.95
- 1011KT – Motorbike Alarm £11.95
- 1019KT – Car Alarm System £10.95
- 1048KT – Electronic Thermostat £9.95
- 1080KT – Liquid Level Sensor £5.95
- 3005KT – LED Dice with Box £7.95
- 3006KT – LED Roulette Wheel £8.95
- 3074KT – 8-Ch PC Relay Board £29.95
- 3082KT – 2-Ch UHF Relay £26.95
- 3126KT – Sound-Activated Relay £7.95
- 3063KT – One Chip AM Radio £10.95
- 3102KT – 4-Ch Servo Motor Driver £15.95
- 3160KT – PIC16F62x Experimenter £8.95
- 1096KT – 3-30V, 5A Stabilised PSU £30.95
- 3029KT – Combination Lock £6.95
- 3049KT – Ultrasonic Detector £13.95
- 3130KT – Infra-red Security Beam £12.95
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- SG10 MKT – Animal Sounds £5.95
- 1131KT – Robot Voice Effect £8.95
- 3007KT – 3V FM Room Bug £6.95
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- 3033KT – Telephone Recording Adpt £9.95
- 3112KT – PC Data Logger/Sampler £18.95
- 3118KT – 12-bit Data Acquisition Unit £52.95
- 3101KT – 20MHz Function Generator £69.95

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Learn About Microcontrollers



PIC Training & Development System

The best place to start learning about microcontrollers is the PIC16F84. This is easy to understand and very popular with construction projects. Then continue on using the more sophisticated PIC16F877 family.

The heart of our system is a real book which lies open on your desk while you use your computer to type in the programme and control the hardware. Start with four very simple programmes. Run the simulator to see how they work. Test them with real hardware. Follow on with a little theory....

Our complete PIC training and development system consists of our universal mid range PIC programmer, a 306 page book covering the PIC16F84, a 262 page book introducing the PIC16F877 family, and a suite of programmes to run on a PC. The module is an advanced design using a 28 pin PIC16F872 to handle the timing, programming and voltage switching requirements. The module has two ZIF sockets and an 8 pin socket which between them allow most mid range 8, 18, 28 and 40 pin PICs to be programmed. The plugboard is wired with a 5 volt supply. The software is an integrated system comprising a text editor, assembler disassembler, simulator and programming software. The programming is performed at normal 5 volts and then verified with plus and minus 10% applied to ensure that the device is programmed with a good margin and not poised on the edge of failure. DC version (shown) for UK, battery version for overseas. UK orders include a plugtop power supply.

- Universal mid range PIC programmer module
 - + Book Experimenting with PIC Microcontrollers
 - + Book Experimenting with the PIC16F877 (2nd edition)
 - + Universal mid range PIC software suite
 - + PIC16F84 and PIC16F872 test PICs. £139.00
- (Postage & insurance UK £9, Europe £14, Rest of world £24)

Experimenting with PIC Microcontrollers

This book introduces the PIC16F84 and PIC16C711, and is the easy way to get started for anyone who is new to PIC programming. We begin with four simple experiments, the first of which is explained over ten and half a pages assuming no starting knowledge except the ability to operate a PC. Then having gained some practical experience we study the basic principles of PIC programming, learn about the 8 bit timer, how to drive the liquid crystal display, create a real time clock, experiment with the watchdog timer, sleep mode, beeps and music, including a rendition of Beethoven's *Für Elise*. Finally there are two projects to work through, using the PIC16F84 to create a sinewave generator and investigating the power taken by domestic appliances. In the space of 24 experiments, two projects and 56 exercises the book works through from absolute beginner to experienced engineer level.

Hardware & Ordering Information

Our PIC software is supplied as a self installing programme which will operate on any modern PC whichever operating system is used. For full information click onto 'Using PIC Software' on our web site.

Telephone with Visa, Mastercard or Switch, or send cheque/PO over immediate despatch. All prices include VAT if applicable.

Web site:- www.brunningsoftware.co.uk

NEW 32 bit PC Assembler

Experimenting with PC Computers with its kit is the easiest way ever to learn assembly language programming. If you have enough intelligence to understand the English language and you can operate a PC computer then you have all the necessary background knowledge. Flashing LEDs, digital to analogue converters, simple oscilloscope, charging curves, temperature graphs and audio digitising.

Kit now supplied with our 32 bit assembler with 84 page supplement detailing the new features and including 7 experiments PC to PIC communication. Flashing LEDs, writing to LCD and two way data using 3 wires from PC's parallel port to PIC16F84.

Book + made up kit 1a + software £73.50

Book + unmade kit 1u + software £66.50

(PP UK £4, Europe £10, Rest of world £14)

C & C++ for the PC

Experimenting with C & C++ Programmes teaches us to programme by using C to drive the simple hardware circuits built using the materials supplied in the kit. The circuits build up to a storage oscilloscope using relatively simple C techniques to construct a programme that is by no means simple. When approached in this way C is only marginally more difficult than BASIC and infinitely more powerful. C programmers are always in demand. Ideal for absolute beginners and experienced programmers.

Book + made up kit 2a + software £57.50

Book + unmade kit 2u + software £51.50

Book + top up kit 2t + software £37.98

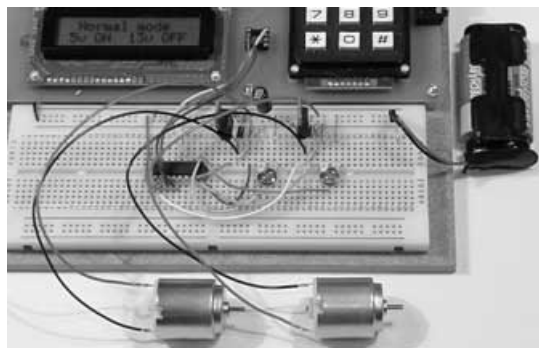
(PP UK £4, Europe £10, Rest of world £14)

The Kits

The assembler and C & C++ kits contain the prototyping board, lead assemblies, components and programming software to do all the experiments. The 'made up' kits are supplied ready to start. The 'top up' kit is for readers who have already purchased kit 1a or 1u.

Assembler and C & C++

Click on 'Special Offers' on our website for details of how to save by buying a combined kit for assembler and C & C++.



Experimenting with the PIC16F877

The second PIC book starts with the simplest of experiments to give us a basic understanding of the PIC16F877 family. Then we look at the 16 bit timer, efficient storage and display of text messages, simple frequency counter, use a keypad for numbers, letters and security codes, and examine the 10 bit A/D converter.

The 2nd edition has two new chapters. The PIC16F627 is introduced as a low cost PIC16F84. We use the PIC16F627 as a step up switching regulator, and to control the speed of a DC motor with maximum torque still available. Then we study how to use a PIC to switch mains power using an optoisolated triac driving a high current triac.

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16C84/16F84/16C71 - £5.90

16F876/877 - £10.00

All inc. VAT and Postage

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- Easy to build & use
- No ground effect, works in seawater



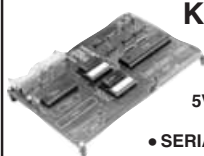
- Detects gold, silver, ferrous & non-ferrous metals

- Efficient quartz controlled microcontroller pulse generation.
- Full kit with headphones & all hardware

KIT 847 £63.95

68000 DEVELOPMENT TRAINING KIT

- NEW PCB DESIGN
- 8MHz 68000 16-BIT BUS
- MANUAL AND SOFTWARE
- 2 SERIAL PORTS
- PIT AND I/O PORT OPTIONS
- 12C PORT OPTIONS



KIT 621

£99.95

- ON BOARD 5V REGULATOR
- PSU £6.99
- SERIAL LEAD £3.99

Stepping Motors

MD100...Std 100 step...£9.99

MD200...200 step...£12.99

MD24...Large 200 step...£22.95



PIC PIPE DESCALER

- SIMPLE TO BUILD
- HIGH POWER OUTPUT
- AUDIO & VISUAL MONITORING
- SWEPT FREQUENCY

An affordable circuit which sweeps the incoming water supply with variable frequency electromagnetic signals. May reduce scale formation, dissolve existing scale and improve lathering ability by altering the way salts in the water behave.

Kit includes case, P.C.B., coupling coil and all components. High coil current ensures maximum effect. L.E.D. monitor.



KIT 868 £22.95

POWER UNIT.....£3.99

MICRO PEST SCARER

Our latest design - The ultimate scarer for the garden. Uses special microchip to give random delay and pulse time. Easy to build reliable circuit. Keeps pets/pests away from newly sown areas, play areas, etc. uses power source from 9 to 24 volts.

- RANDOM PULSES
- HIGH POWER
- DUAL OPTION



Plug-in power supply £4.99

KIT 867.....£19.99

KIT + SLAVE UNIT.....£32.50

WINDICATOR

A novel wind speed indicator with LED readout. Kit comes complete with sensor cups, and weatherproof sensing head. Mains power unit £5.99 extra.

KIT 856.....£28.00

★ TENS UNIT ★

DUAL OUTPUT TENS UNIT

As featured in March '97 issue.

Magenta have prepared a FULL KIT for this excellent new project. All components, PCB, hardware and electrodes are included. Designed for simple assembly and testing and providing high level dual output drive.

KIT 866. . Full kit including four electrodes £32.90

Set of
4 spare
electrodes
£6.50

1000V & 500V INSULATION TESTER



Superb new design. Regulated output, efficient circuit. Dual-scale meter, compact case. Reads up to 200 Megohms.

Kit includes wound coil, cut-out case, meter scale, PCB & ALL components.

KIT 848..... £32.95

EPE TEACH-IN 2000

Full set of top quality NEW components for this educational series. All parts as specified by EPE. Kit includes breadboard, wire, croc clips, pins and all components for experiments, as listed in introduction to Part 1.

*Batteries and tools not included.

TEACH-IN 2000 -

KIT 879 £44.95

MULTIMETER £14.45

SPACEWRITER

An innovative and exciting project. Wave the wand through the air and your message appears. Programmable to hold any message up to 16 digits long. Comes pre-loaded with "MERRY XMAS". Kit includes PCB, all components & tube plus instructions for message loading.

KIT 849 £16.99

12V EPROM ERASER

A safe low cost eraser for up to 4 EPROMs at a time in less than 20 minutes. Operates from a 12V supply (400mA). Used extensively for mobile work - updating equipment in the field etc. Also in educational situations where mains supplies are not allowed. Safety interlock prevents contact with UV.

KIT 790 £29.90

SUPER BAT DETECTOR

1 WATT O/P, BUILT IN
SPEAKER, COMPACT CASE

20kHz-140kHz

NEW DESIGN WITH 40kHz MIC.

A new circuit using a 'full-bridge' audio amplifier i.c., internal speaker, and headphone/tape socket. The latest sensitive transducer, and 'double balanced mixer' give a stable, high performance superheterodyne design.



KIT 861 £24.99

ALSO AVAILABLE Built & Tested... £39.99

MOSFET MkII VARIABLE BENCH POWER SUPPLY 0-25V 2.5A

Based on our Mk1 design and preserving all the features, but now with switching pre-regulator for much higher efficiency. Panel meters indicate Volts and Amps. Fully variable down to zero. Toroidal mains transformer. Kit includes punched and printed case and all parts. As featured in April 1994 EPE. An essential piece of equipment.



Kit No. 845 £64.95

ULTRASONIC PEST SCARER

Keep pets/pests away from newly sown areas, fruit, vegetable and flower beds, children's play areas, patios etc. This project produces intense pulses of ultrasound which deter visiting animals.

- KIT INCLUDES ALL COMPONENTS, PCB & CASE
- EFFICIENT 100V TRANSDUCER OUTPUT
- COMPLETELY INAUDIBLE TO HUMANS

- UP TO 4 METRES RANGE
- LOW CURRENT DRAIN



KIT 812..... £15.00

SIMPLE PIC PROGRAMMER

KIT 857... £12.99

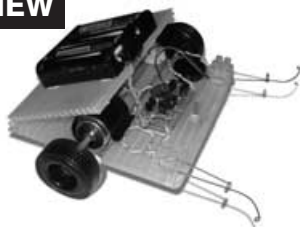
Includes PIC16F84 chip disk, lead, plug, p.c.b., all components and instructions

Extra 16F84 chips £3.84
Power Supply £3.99

MAGENTA BRAINBOT I & II

NEW

- Full kit with ALL hardware and electronics
- As featured in *EPE* Feb '03 – KIT 910
- Seeks light, beeps, avoids obstacles
- Spins and reverses when 'cornered'
- Uses 8-pin PIC
- ALSO KIT 911 – As 910 PLUS programmable from PC serial port – leads and software CD provided



KIT 910 £16.99 KIT 911 £24.99

PIC 16F84 MAINS POWER 4-CHANNEL CONTROLLER & LIGHT CHASER

- ZERO VOLT SWITCHING
- OPTO ISOLATED 5 Amp
- 12 KEYPAD CONTROL
- HARD-FIRED TRIACS
- WITH SOURCE CODE
- SPEED & DIMMING POT.
- EASILY PROGRAMMED

Kit 855 £39.95

PIC 16F84 LCD DISPLAY DRIVER

INCLUDES 1-PIC16F84 WITH DEMO PROGRAM SOFTWARE DISK, PCB, INSTRUCTIONS AND 16-CHARACTER 2-LINE LCD DISPLAY

Kit 860 £19.99

Power Supply £3.99

FULL PROGRAM SOURCE CODE SUPPLIED – DEVELOP YOUR OWN APPLICATION!

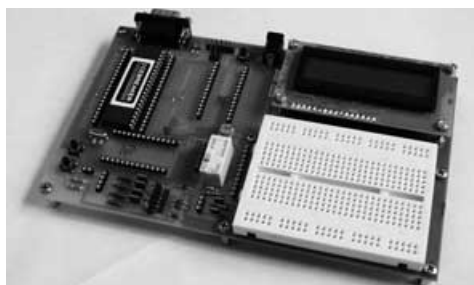
Another super PIC project from Magenta. Supplied with PCB, industry standard 2-LINE x 16-character display, data, all components, and software to include in your own programs. Ideal development base for meters, terminals, calculators, counters, timers – Just waiting for your application!

8-CHANNEL DATA LOGGER

As featured in Aug./Sept. '99 *EPE*. Full kit with Magenta redesigned PCB – LCD fits directly on board. Use as Data Logger or as a test bed for many other 16F877 projects. Kit includes programmed chip, 8 EEPROMs, PCB, case and all components.

KIT 877 £49.95 inc. 8 x 256K EEPROMS

ICEBREAKER



PIC Real Time In-Circuit Emulator

- Icebreaker uses PIC16F877 in circuit debugger
- Links to Standard PC Serial Port (lead supplied)
- Windows™ (95+) Software included
- Works with MPASM and MPLAB Microchip software
- 16 x 2 L.C.D., Breadboard, Relay, I/O devices and patch leads supplied

As featured in March '00 *EPE*. Ideal for beginners AND advanced users. Programs can be written, assembled, downloaded into the microcontroller and run at full speed (up to 20MHz), or one step at a time.

Full emulation means that all I/O ports respond exactly and immediately, reading and driving external hardware.

Features include: Reset; Halt on external pulse; Set Breakpoint; Examine and Change registers, EEPROM and program memory; Load program, Single Step with display of Status, W register, Program counter, and user selected 'Watch Window' registers.

KIT 900 ... £34.99

POWER SUPPLY £3.99 STEPPING MOTOR 100 STEP £9.99

EPE PIC TOOLKIT 3

NEW

- THE LATEST TOOLKIT BOARD – 8, 18, 28 AND 40-PIN CHIPS
- MAGENTA DESIGNED P.C.B. WITH COMPONENT LAYOUT AND EXTRAS
- L.C.D., BREADBOARD AND PIC CHIP INCLUDED
- ALL TOP QUALITY COMPONENTS AND SOFTWARE SUPPLIED

KIT 880 ... £34.99 with 16F84 ... £39.99 with 16F877

PIC TOOLKIT V2

- SUPER UPGRADE FROM V1 • 18, 28 AND 40-PIN CHIPS
- READ, WRITE, ASSEMBLE & DISASSEMBLE PICS
- SIMPLE POWER SUPPLY OPTIONS 5V-20V
- ALL SWITCHING UNDER SOFTWARE CONTROL
- MAGENTA DESIGNED PCB HAS TERMINAL PINS AND OSCILLATOR CONNECTIONS FOR ALL CHIPS
- INCLUDES SOFTWARE AND PIC CHIP

KIT 878 ... £22.99 with 16F84 ... £29.99 with 16F877

EPE PIC Tutorial

At last! A Real, Practical, Hands-On Series

- **Learn Programming from scratch using PIC16F84**
- **Start by lighting I.e.d.s and do 30 tutorials to Sound Generation, Data Display, and a Security System.**
- **PIC TUTOR Board with Switches, I.e.d.s, and on board programmer**

PIC TUTOR BOARD KIT

Includes: PIC16F84 Chip, TOP Quality PCB printed with Component Layout and all components* (*not ZIF Socket or Displays). Included with the Magenta Kit is a disk with Test and Demonstration routines.

KIT 870 £27.95, Built & Tested £42.95

Optional: **Power Supply – £3.99, ZIF Socket – £9.99**

LCD Display £7.99 LED Display £6.99

Reprints Mar/Apr/May 98 – £3.00 set 3

SUPER PIC PROGRAMMER

- READS, PROGRAMS, AND VERIFIES
- WINDOWS™ SOFTWARE
- PIC16C AND 16F – 6X, 7X, AND 8X
- USES ANY PC PARALLEL PORT
- USES STANDARD MICROCHIP • HEX FILES
- OPTIONAL DISASSEMBLER SOFTWARE (EXTRA)
- PCB, LEAD, ALL COMPONENTS, TURNED-PIN SOCKETS FOR 18, 28, AND 40 PIN ICs

- SEND FOR DETAILED INFORMATION – A SUPERB PRODUCT AT AN UNBEATABLE LOW PRICE.

Kit 862 £29.99

Power Supply £3.99

DISASSEMBLER SOFTWARE £11.75

PIC STEPPING MOTOR DRIVER

INCLUDES PCB, PIC16F84 WITH DEMO PROGRAM, SOFTWARE DISC, INSTRUCTIONS AND MOTOR.

Kit 863 £18.99

FULL SOURCE CODE SUPPLIED ALSO USE FOR DRIVING OTHER POWER DEVICES e.g. SOLENOIDS

Another Magenta PIC project. Drives any 4-phase unipolar motor – up to 24V and 1A. Kit includes all components and 48 step motor. Chip is pre-programmed with demo software, then write your own, and re-program the same chip! Circuit accepts inputs from switches etc and drives motor in response. Also runs standard demo sequence from memory.

MAGENTA

All prices include VAT. Add £3.00 p&p. Next day £6.99

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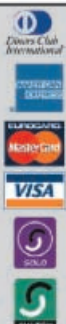
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COMPONENT ACCESSORIES

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4016B	£0.20	74HC133	£0.34	74LS148	£0.64
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4018B	£0.26	74HC138	£0.29	74LS151	£0.31
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4020B	£0.26	74HC151	£0.33	74LS156	£0.36
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SSM2151P

SSM2152P

SSM2153P

SSM2154P

SSM2155P

SSM2156P

SSM2157P

SSM2158P

SSM2159P

SSM2160P

SSM2161P

SSM2162P

SSM2163P

SSM2164P

SSM2165P

SSM2166P

SSM2167P

SSM2168P

SSM2169P

SSM2170P

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SSM2180P

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SSM2182P

SSM2183P

SSM2184P

SSM2185P

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SSM2193P

SSM2194P

SSM2195P

SSM2196P

SSM2197P

SSM2198P

SSM2199P

SSM2200P

SSM2201P

SSM2202P

SSM2203P

SSM2204P

SSM2205P

SSM2206P

SSM2207P

SSM2208P

SSM2209P

EVERYDAY PRACTICAL ELECTRONICS

THE No.1 MAGAZINE FOR ELECTRONICS TECHNOLOGY & COMPUTER PROJECTS

VOL. 32 No. 11 NOVEMBER 2003

Editorial Offices:

EVERYDAY PRACTICAL ELECTRONICS EDITORIAL
WIMBORNE PUBLISHING LTD., 408 WIMBORNE ROAD EAST,
FERNDOWN, DORSET BH22 9ND
Phone: (01202) 873872. Fax: (01202) 874562.

Email: enquiries@epemag.wimborne.co.uk

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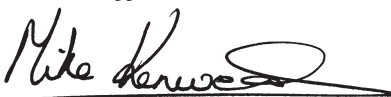
The Approximate Cost we give for projects is just that – approximate. We do not supply components for projects but we do make sure you can buy everything you need to build any of our projects – see *Shoptalk* for information on buying unusual items. However, the Approximate Cost we work out can vary over a very wide range. Take, for instance, the *PIC Random L.E.D. Flasher* by Andy Flind in this issue, if you buy the pre-programmed chip rather than programming it yourself and buy all the components from the most expensive supplier the cost could be as much as 50% more than we suggest. On the other hand if you program the PIC yourself, make your own p.c.b. using chemicals etc. you already have and buy the resistors and l.e.d.s in bulk then you could probably get the cost of the components down to about £7, or 65% of our Approximate Cost.

We tend to take the middle line and suggest what we feel is a reasonable price, including the cost of the p.c.b. from our *PCB Service*, but please don't take it as gospel and please be prepared to shop around for components. Also note that we do not include any minimum order charges or post and packing charges in any of our calculations.

TEACH-IN

Sometimes pricing projects is difficult for various reasons and usually we will leave out the cost of the case because the price will vary so much with the style of case chosen. This month the price of components for the *Teach-In 2004* series has presented such a headache. The Components List shows what we expect to be the range of items needed but, because the designs of some of the later projects covered in the series are yet to be finalised, the list, particularly of Miscellaneous items, is still a little vague.

There is also the point that few readers will wish to build every project in the series and, even if they do, it is unlikely that they will want to complete them all in exactly the same way as we describe. After all, half the fun of project building is in tailoring the design to meet your own specific needs. With this in mind, we have priced the "regular" components for *Teach-In* (those that most readers will require) whilst leaving out the more specialised items under Miscellaneous which will be needed to build some of the later projects like the Electronic Lock or Automatic Curtain Winder. Thus the Approximate Cost that is shown will allow readers to follow the series but not to build some of the later projects.



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All reasonable precautions are taken to ensure that the advice and data given to readers is reliable. We cannot, however, guarantee it and we cannot accept legal responsibility for it.

A number of projects and circuits published in *EPE* employ voltages that can be lethal. **You should not build, test, modify or renovate any item of mains powered equipment unless you fully understand the safety aspects involved and you use an RCD adaptor.**

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We do not supply electronic components or kits for building the projects featured, these can be supplied by advertisers (see *Shoptalk*). We advise readers to check that all parts are still available before commencing any project in a back-dated issue.

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PIC RANDOM L.E.D. FLASHER



ANDY FLIND

Enjoy the fun of an interesting and attractive pattern display

FOR many years the author has wondered if a bunch of l.e.d.s flashing at apparently random intervals might produce an interesting and attractive display. Occasionally consideration was given to the construction of a suitable circuit, but the project always foundered because of the complexity of the electronics required.

As with so many other ideas, the PIC microcontroller has changed this since much of the complexity can now be achieved at virtually no cost (other than time!) through software. Since the PIC outputs can supply sufficient current to drive l.e.d.s directly, the hardware consists of just a PIC, some clock components and the l.e.d.s with their current limiting resistors.

A RANDOM NUMBER

In addition, since the random pattern generating software takes up only part of the PIC's program memory, a conventional pattern sequence can be included with a pushbutton switch to make the selection.

Electronics is an exact science of course, and a truly random output is difficult to achieve. When Premium Bonds were introduced many years ago a large and costly computer system was developed to make the random winning selections. This was called *Ernie*, an acronym for Electronic Random Number Indicating Engine, and was probably intended to impress the prospects.

Today's punters must be less easily impressed because the National Lottery has reverted to a sort of tombola machine in which the technology consists of numbered balls in a drum! Most "random" projects for home construction, such as electronic dice, rely on external factors such as tiny variations in the period for which the user presses a switch and do not actually generate a random output of their own.

PRBS GENERATOR

A method of producing an apparently random stream of digital bits is to use a PRBS generator. The acronym stands for

Pseudo Random Bit Sequence and, as *pseudo* implies, the output is not truly random, it is a regularly repeating sequence. However, the sequence is so long that it seems to be random and PRBSs are increasingly being found in noise generation and other randomising circuits.

The actual length of the sequence depends on the number of shift register stages and the tapping points. For any given number of register stages there is an optimum tapping arrangement to obtain the longest sequence. The mathematics for finding this are complex, but fortunately the required factors are readily available from various books.

Two such sources are *The CMOS Cookbook* and *The Art of Electronics*,

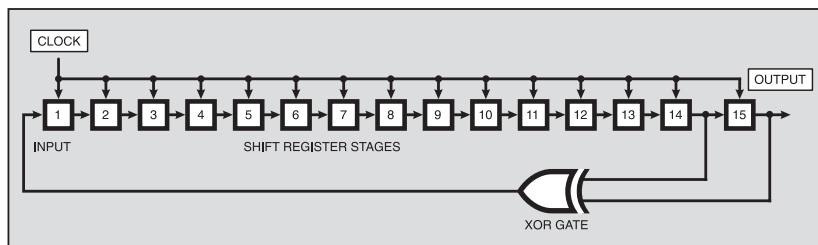


Fig.1. Block schematic of the Pseudo Random Bit Sequence Generator.

A PRBS normally consists of a shift register with taps at one or more stages, the outputs of which are exclusive-ORed (XOR) with the output and fed back into the input. When the register is clocked, the resulting output is a stream of high and low bits with a fixed sequence, but the pattern of this sequence can be so long before it is repeated that for most purposes it appears to be random.

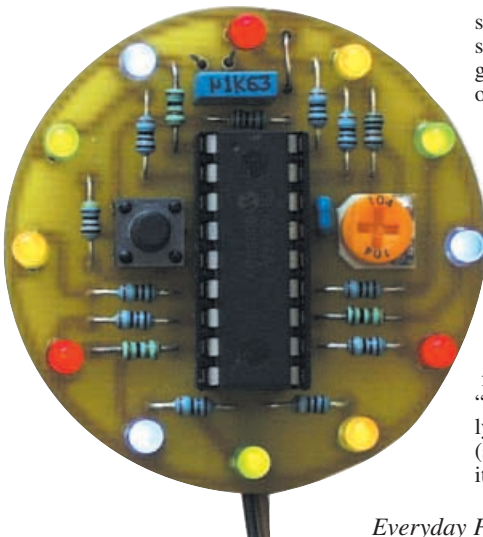
though no doubt there are others. Digital audio "noise" generation usually requires a hardware circuit clocked at fairly high speed, but for randomly flashing some l.e.d.s the speed can be much lower and the PRBS itself can be implemented using software in a PIC.

VIRTUAL RANDOMNESS

The PRBS in this design uses a "virtual" shift register with fifteen stages, tapped at stage fourteen, as shown in the block diagram of Fig.1. This produces a sequence of over thirty two thousand steps, so there is little chance of a pattern being noticed in flashing l.e.d.s driven by it.

The way in which the PRBS is implemented in software is illustrated in the flow diagram of Fig.2. Two 8-bit PIC registers, named in the software as SR1 and SR2, are used as the shift register. The last, or MSB (most significant bit), bit of SR2 is ignored as only fifteen bits are required.

A third register named EXOR is used for implementing the XOR function. To "step" the PRBS register, EXOR is initially cleared. Then the state of SR2 bit 5 (stage 14 of the shift register) is read and if it is high, EXOR is incremented. The same



is done for SR2 bit 6 (stage 15, or the output).

If only one of these two bits is high, bit 0 (LSB – least significant bit) of EXOR will be high, but if neither or both are high it will be zero, so the state of this bit represents the XORed result of bits 5 and 6 of SR2, stages 14 and 15 of the shift register.

If EXOR is high, the STATUS CARRY bit is now set, if low, it is cleared. This becomes the input to the shift register when SR1 and SR2 are sequentially rotated left, the equivalent of clocking a hardware shift register. All of this requires just eleven lines of assembly code, including the RETURN statement since it is written as the subroutine, SHIFT. The statement CALL SHIFT is now all that is required to clock the virtual PRBS.

ILLEGAL

A feature of PRBS generators is that there is usually an “illegal state” in which, depending on the design, all logic 0s or logic 1s are continuously circulating. Precautions must be taken to prevent this condition from occurring.

At the beginning of the random program a check is made for an “all zero” state in SR1 and SR2, and if this is detected SR1 is pre-loaded with a pattern. This is only done when such a state is detected as normally the random patterns found in these registers at power-up will contribute to the apparently random output from them.

RANDOMISED FLASHING

Now that the PRBS has been implemented, the next step is to translate its output into randomly flashing l.e.d.s. The

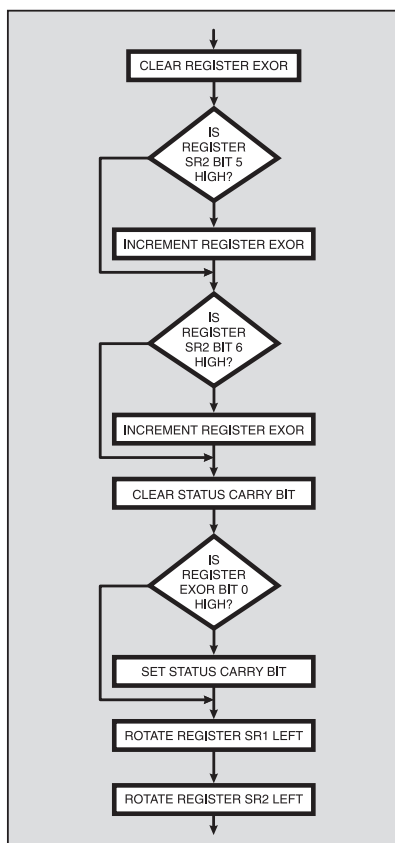


Fig.2. Pseudo random bit sequence generator in software.

method for this is shown in the flow diagrams of Fig.3 and Fig.4, which show the action for the first l.e.d.

The flow chart in Fig.3 illustrates the decision as to whether the first l.e.d. output should be updated. It starts by stepping the PRBS. Then it decrements register TM1, used as a counter. If this has reached zero the output subroutine for the first l.e.d. (LED1) is called, otherwise the program continues on to the next l.e.d.

Assuming the output subroutine of Fig.4 is called, firstly LED1 is turned on if the output of the PRBS is high, or off if it is low. Next the first three bits of register SR1 of the PRBS are taken and one is added to their value to give an apparently random factor between 1 and 8, which is placed into the counter TM1.

Program control then returns to the main loop where it continues by performing the same process for LED2 through LED12. The overall result is a random number of from one to eight complete loops between the updating of each l.e.d., and a random selection of whether each will be on or off after each update. Consequently, the effect is about as random as can be achieved with such a simple program.

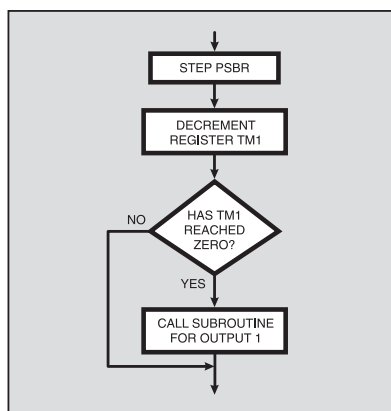


Fig.3. Output action decision making.

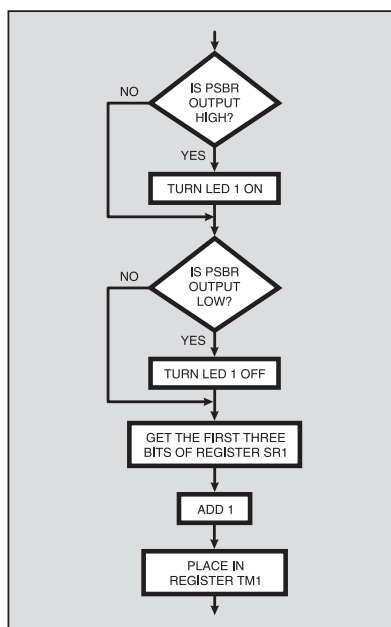


Fig.4. Flow diagram showing the output process.



COMPONENTS

Resistors

R1, R2 10k (2off)
R3 4k7
R4, R5, R7 to R9, R11 to R13, R15 390Ω (9 off)

R6, R10, R14 100Ω (3 off)

All 0.25W 5% carbon film or better.

Potentiometer

VR1 100k sub-min enclosed preset, 6mm, round

Capacitors

C1 1n resin-dipped ceramic, 2.5mm pitch

C2 100n polyester layer or resin-dipped ceramic, 5mm pitch

Semiconductors

D1, D5, D9 3mm yellow l.e.d., low-current, (3 off)

D2, D6, D10 3mm red l.e.d., low-current, (3 off)

D3, D7, D11 3mm blue l.e.d., hi-intensity, diffused, (3 off)

D4, D8, D12 3mm green l.e.d., low-current, (3 off)

IC1 PIC16F84 microcontroller, pre-programmed (see text)

Miscellaneous

S1 push-to-make tactile switch, projected shaft, p.c.b. mounting

Printed circuit board, available from the EPE PCB Service, code 424; 18-pin d.i.l. socket; battery clip to hold 4 x AAA cells; solder etc.

Approx. Cost
Guidance Only

£11
excl. batts

SINGLE-USE DIGITAL CAMERAS

Handy snapping takes another step forward – but who owns the technology's patent? asks Barry Fox

SINGLE-USE digital cameras are now going on sale in the US from Dakota Digital. The camera costs \$11 and the prints cost another \$11. Already two companies are claiming patent rights on the basic idea and more are likely to come out of the woodwork.

Pure Digital Technologies of San Francisco is hoping to win potentially very valuable worldwide rights with patents filed in September 2001 (WO 03/024083). Instead of film, the recyclable camera has a memory chip; instead of cracking open the camera to process the film, a lab sucks out the stored images and makes paper prints.

Pure Digital claims legal monopoly on "a limiting-use component" that "limits use to a single use cycle". To stop people re-using the camera and making their own prints with a home computer, the patented camera uses non-standard connections and digital coding. So, in theory at least, only an approved print centre can access the pictures, charge for prints and wipe the camera's memory clean for re-use.

Meanwhile DVC (Australia) of Auckland in New Zealand also has world filings on a similar theme, dated November 2001 (WO 03/047245). Encryption is used to lock the recording inside the camera.

Cardboard Video

DVC is the same company, then called Disposable Video Camcorders, that was patenting (WO 98/26586) a throw-away video camcorder five years ago.

The idea then was to cut the cost by avoiding the need to lace the tape round the recording heads and rewind it. The DVC plan was to make the body from reinforced cardboard, with a simple recording mechanism and factory-loaded cassette tape. The lens and image sensor could either be cheap, with low resolution, or easily replaceable.

A tourist who had forgotten to bring a camcorder on holiday, would buy a disposable unit, shoot a video and then either throw it away or return it to a reconditioning centre for credit. To stop people trying to beat the system and re-loading their own tapes, the cardboard camcorder was to be sold with a seal which must be broken to remove the cassette. This shorts an electrical circuit to melt a plastic guide pin without which the tape cannot run. The cardboard camcorder did not need a battery. Instead it used a clockwork motor to drive the tape and power the video circuitry.

Cardboard clockwork cameras never caught on, but disposable digital

cameras might. If so there could be patent battles ahead, with lawyers trying to prove who did, said and wrote what first.

Intriguingly, Pentax and Sanyo announced plans in Japan in October 2001, between the filing dates of the two world patent applications. Very probably Pentax and Sanyo had by then filed their own patent applications.

FML'S CAT

THE latest copy of FML Electronics' catalogue has been received, offering as usual the wide variety of electronic components that all enthusiasts need, including good ranges of semiconductors and passive devices. It's a useful cat to have on your workbench – 18 pages of A4 cram-packed with products. Tel: 01677 425840.

CHALLENGE THE ROBOTS!



Can you build a robot car and enter a challenge? If you can then why not enter the Melexis Safety Trophy 2004! Belgian microelectronics Melexis company and the Flemish hands-on centre for science and technology Technopolis are organising the second edition of this international contest. The participants build a robot car that is able to negotiate an obstacle course as safely as possible by means of sensors and software.

The next Melexis Safety Trophy takes place on 24 and 25 April 2004 in the Brabant, close to Leuven, Belgium. In several heats the robots must attempt to negotiate a 20-metre by 10-metre route as quickly as possible. In this they will encounter obstacles placed through the route: bricks, warm and cold cans, as well as another robot. Colliding with warm cans (or with a bit of imagination, pedestrians!) and with the other robot yields penalty time. Knocking over cold cans on the other hand is rewarded with bonus time. In addition, road signs indicate where many cold and warm cans are located along the route.

Students and hobbyists may participate for free. Moreover, Melexis will provide them with sensors and test signs and on-line advice. Those who register before 31 October will receive a free pack of Melexis sensors. Participants may also use other sensors from any manufacturer. Not only will the three fastest robots win prizes, but the best looking, the most innovative, and the unluckiest robots, will also be rewarded.

The idea for this competition was inspired by the quick growth of active safety applications in cars, to practically acquaint creative students and hobbyists with this fascinating but complex issue. It might even yield usable ideas for real applications as the contest is just a simplified simulation of a real traffic situation.

More information on the competition, its prizes valued at 10,000 Euros, the previous edition, products etc. can be found at www.melexis.com/trophy.

TINY CCD CAMERA



SHARP have developed a mega-pixel CCD camera module said to be the smallest (1.44cc) and thinnest (9.7mm) in the industry. This module makes it possible to incorporate mega-pixel class cameras into mobile phones with minimal changes to their current standard size and thickness.

The number of output pixels is 1144(H) x 880(V), the maximum frame rate is 7.5fps, power consumption 650mW, and the lens number F2.8.

For more information browse www.sharpsme.com.

OBSERVANT DATASTATION

OBSERVANT Electronics tell us that they have released a new development board for their range of DataStation products, making them even easier to use. The new board, which can be "piggy-backed" onto any standard DataStation module, gives the user full control of its analogue and digital I/Os while still allowing access to the screw terminals.

DataStation is a family of software-configurable, mixed signal I/O products that bring unique flexibility to control and data acquisition applications. By combining software-configurable channels with a compact instruction set, the DataStation family overcomes the two main problems of traditional serial I/O solutions: limited choice of channel configurations, and low sample rates.

Delivering a 12-bit sample rate of greater than 500 samples a second, DataStation is suitable for applications as diverse as machine control, industrial automation, environmental monitoring and robotics, making it possible for designers to meet the needs of virtually any application with just one software compatible family of products.

DataStation's 16 software-configurable channels can be configured to give any combination of up to six analogue inputs (with selectable 8-bit or 12-bit resolution), two PWM outputs, 16 digital inputs and 16 digital outputs, giving a total of 391 different I/O configurations from a single product.

DataStation can be purchased in one-off quantities online for £89.00 + VAT and £2.95 P&P (per order). The user manual and software development tools, templates and examples can be downloaded free of charge from Observant's website.

For more information contact Observant Electronics Ltd., Dept EPE, Unit F2B, Avonside Enterprise Park, Melksham SN12 8BS. Tel: 01225 704631. Web: www.ObservantWorld.com.

ROTO-VIEWING MOBILES

INNOVENTIONS, a Houston-based private company, has developed a new display "tilt-navigation" technology for PDAs, cell phones and other devices. With RotoView enabled, the user overcomes the display navigation challenge by simply changing the orientation at which the device is held.

It has been developed to answer the demand for cell phone manufacturers to pack more and more information into their tiny displays.

For more information browse www.rotoview.com.

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THREE-COMPONENT METAL DETECTOR – TRI-UMPHAL TREASURE

THE circuit shown in Fig.1 must represent the limits of simplicity for a metal detector – yet the design works surprisingly well. It uses just one 40106 hex Schmitt inverter i.e., a capacitor, and a search coil – and of course the batteries. A lead from IC1b pin 4 needs to be attached to a medium wave (MW) radio aerial, or it should be wrapped around the radio.

As shown, the metal detector gives a respectable range for beat frequency operation (b.f.o.) – up to 90mm for a bottle-top. In fact, for the ultimate in simplicity, capacitor C1 may be omitted. In this way the author achieved an amazing 150mm range for the bottle-top. However, with the frequency then being raised to more than 4MHz, instability becomes a significant problem.

As shown, the circuit oscillates at around 230kHz. One may also experiment with the

frequency by changing the value of C1. A Faraday shield may be added to reduce ground effect and capacitive coupling, and this is wired to 0V.

Since an inductor resists rapid changes in voltage (called reactance), the charging of capacitor C1 is slightly delayed as the logic level at IC1a pin 2 changes. This sets up a rapid oscillation, which is picked up by a MW radio. Any changes in the inductance of the search coil (through the presence of metal) bring about a change to the oscillator frequency. Although 230kHz is out of range of the Medium Wave band, an MW radio will clearly pick up harmonics of this frequency. IC1b serves as a buffer.

The making of search coil L1 allows a lot of room for error, and is far from critical. The author used seventy turns of 30s.w.g. (0.315mm) enamelled copper wire on a 120mm diameter former.

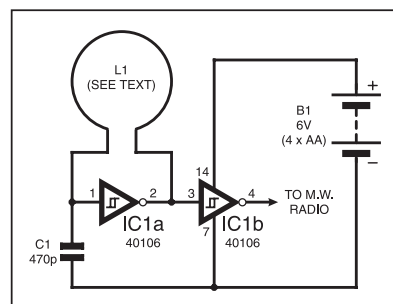


Fig.1. Three-component Metal Detector circuit.

The metal detector is set up by tuning the MW radio to pick up a whistle (a harmonic of 230kHz). Not every such harmonic works well, and the most suitable one needs to be found. The presence of metal will clearly change the tone of the whistle.

Thomas Scarborough,
South Africa

EMERGENCY LIGHT – BRIGHTENING AUNTY

THE idea for this circuit came when I was repairing my aunt's emergency light. Bulb-based emergency lighting has a low efficiency and ultrabright i.e.d.s provide greater efficiency and more illumination, with a much extended battery life. It was therefore decided to change from a 12V light bulb to a pack of i.e.d.s.

To get constant light, a constant voltage technique was adopted, using the circuit in Fig.2. For more power saving, step-down switching is used in preference to step-up. This function is provided by IC1 in conjunction with diode D3, inductor L1 and capacitors C3 and C4.

The resulting output is a stable 5V and powers the 12 ultrabright yellow i.e.d.s D4 to D15. The i.e.d.s are grouped in pairs, each pair buffered by a resistor, R4 to R9. Diode D3 is a high-efficiency type – do not change it to a 1N4000 series type as they are less efficient in this role.

The network consisting of R1 and D1 is a power-on indicator. The network around VR1, TR1, R2, R3 and D2 is a low-battery indicator. Preset VR1 should be adjusted until i.e.d. D2 turns on when the battery voltage is low.

Inductor L1 should be a toroid type in order to reduce radiated r.f. interference caused by the switching regulator IC1. It should be glued to the circuit board to prevent it from vibrating.

A small heatsink should be fitted to IC1. The circuit efficiency was found to be around 80%, i.e. about 10% better than with the step-up switching technique. The circuit operates for about four times longer than the bulb-based one in respect of battery life.

Myo Min, Yangon, Myanmar

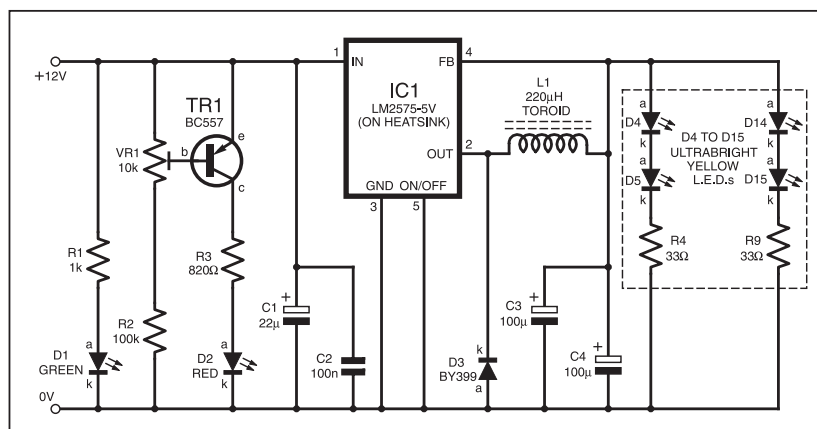


Fig.2. Circuit diagram for an Emergency L.E.D. Light.

Power Supply Tester – Taking the Strain

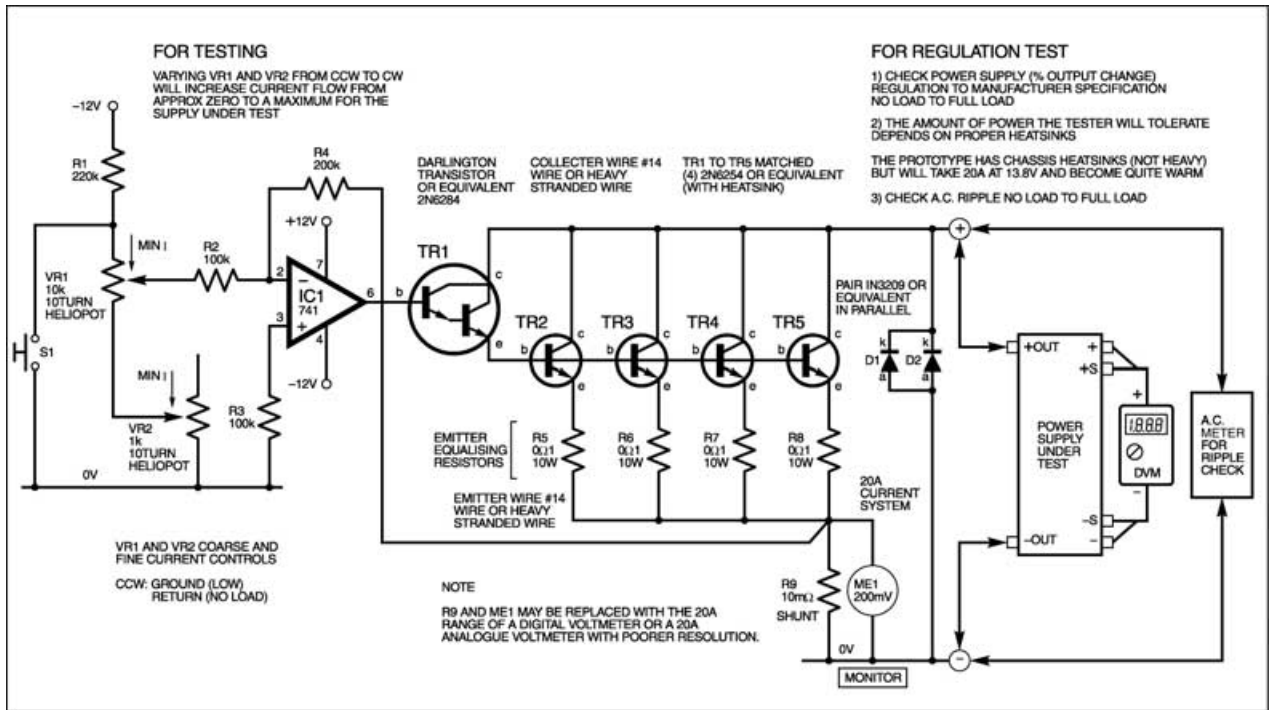


Fig.3. Circuit diagram for the Power Supply Load Tester.

As with many tinkerers and junk electronics collectors, a variety of “acquired” power supplies wind up on the author’s shelves to await attention. But are they worth keeping? Testing them with a resistive load is messy and difficult, and with high current supplies it is nearly impossible, unless you have a carbon pile!

The tester whose circuit diagram is shown in Fig.3 controls supply currents to 20A, and voltages from 1.7V to over 50V. Current control is so stable that once the current is set, a supply voltage can be varied across this range and the current will remain constant. Maximum power will depend upon how well the pass transistors utilise heatsinks.

How It Works

The circuit operates as a loop. At the control end, a -12V regulated supply provides approximately 50µA to R1, VR1 and VR2. Resistor R2 sees this as a range of 0V to 5V, or 0µA to 5µA at pin 2 of IC1, the inverting input.

With no power supply connected to the test terminals, the output at IC1 pin 6 will be at -10V with the wipers of VR1 and VR2 at ground (0V). As their wipers are moved away from 0V, pin 6 of IC1 will change to 2.0V. When a power supply is connected for test and VR1 and VR2 are adjusted away from 0V, essentially the same thing will happen, except IC1 pin 6 will be at 1.2V as soon as the unit under test starts to draw current.

When the current controls are increased, say for a 20A supply, pin 6 of IC1 will rise to approximately 3V. The output of IC1 drives the Darlington transistor TR1, which has an H_{fe} (current gain) of 2500, and this turns on transistors TR2 to TR5, resulting in a current across shunt resistor R9. The resulting

voltage drop across R9 produces a current through R4 equal and opposite to the current through R2. This opposing action keeps pin 2 of IC1 at virtual ground and the loop is completed for feedback control.

Note that diode D1 (in parallel with D2) provides reverse voltage protection for the tester. Ensure that these diodes are connected the correct way round.

This circuit was designed around a 0.01Ω shunt and a DVM with 199.9mV full scale for R9 and ME1. For different shunt values, an op.amp can amplify the shunt voltage.

Using the Tester

This tester can check to see how well the supply regulates to keep the voltage constant under load. When first using it, use a power supply with a known current limit, preferably one with meters that monitor both voltage and current. It is also a good idea to check the voltages quoted earlier, under no-load conditions.

First set the wipers of VR1 and VR2 to 0V, then connect the tester to the power supply to be tested and switch on its power. Monitor the output of the supply with a digital voltmeter (DVM). Increase the settings of VR1 and VR2 for a slight current increase, as shown by meter ME1. This meter can be another

DVM with full scale at 199.9mV (the equivalent to 20A).

Now increase VR1 and VR2 to the known current limit, noting the slight drop in the output voltage. Push on switch S1 to short the reference current to ground and note the change in the output. This test gives a *no load to full load* change. This should be done briefly, returning VR1 and VR2 wipers to ground after testing.

The power supply’s regulation can be calculated as:

$$\% \text{ regulation} = \frac{V_{NL} - V_{FL}}{V_{FL}} \times 100$$

where V_{NL} = voltage no load
 V_{FL} = voltage full load

Caution

Testing a power supply for regulation at maximum ratings can be hazardous. The hazards can be minimized by being brief when at maximum current. Look for a slight drop in the supply output voltage when at maximum current, and immediately return the wipers of VR1 and VR2 to 0V if a drop is observed. A regulated supply can usually handle currents of 1A or greater.

Duane W. Clairmont,
Conway, USA

INGENUITY UNLIMITED BE INTERACTIVE

IU is *your* forum where you can offer other readers the benefit of your Ingenuity. Share those ideas, earn some cash and possibly a prize!



Strike Force Nine

Why is lightning so potent, and can you protect your gizmos?

Andy Emerson offers some answers.

CHANCES are you've had at least one household appliance destroyed by lightning. It might be a video recorder or the modem in your computer. Chips designed for 5V or 3V operation are fried instantly by the monster voltage surges induced by lightning, which can also take out perhaps an entire PC, including the disk controller circuitry on a hard drive.

Apart from the pain of shelling out for new devices (assuming they're not covered by household insurance), there's more grief too if the strike destroys irreplaceable data (no – hang on, everyone makes back-ups now, don't they?). Perhaps you reckon manufacturers should put more protection into devices vulnerable to lightning damage, but if so, then you underestimate the destructive force of thunderbolts.

HORROR STORY

Not convinced? Then just hear what a telephone engineer told me recently . . .

"I spent the whole five days of last week clearing up after a lightning strike in a quiet residential area in south London. The bolt struck a tree that was a metre away from a telegraph pole and the damage was as follows:

1. The entire pole top was a mass of melted plastic.

2. The 20-pair cable feeding the distributor at the top of the pole was completely fused into one mass of melted plastic and copper.

3. The joint at the base of the pole exploded.

4. Every one of the 18 customer drop-wires from this pole melted for approximately two metres away from the pole.

5. The 20-pair feeder cable (which was underground in a duct) feeding the base of the pole had the insulation of each individual pair melted within the cable.

6. The 100-pair joint that this cable fed (70 metres away on the other side of the road) was blackened inside and had melted pairs.

7. All 18 customers suffered their input terminal blocks explode inside their homes, with the lids being found the other side of the rooms.

8. All 18 main sockets inside the houses were destroyed internally (burnt out).

9. Ten of the homes required total internal rewiring jobs.

10. Eleven modems, five complete computers, seven video recorders and eight cordless telephones were beyond repair.

11. One poor lady closest to the pole was hit in the back when the mains transformer of her cordless phone shot across her kitchen.

12. In the same household the power wiring melted and the mains sockets were blown out of their wallboxes.

13. No less than 14 similar faults were reported in homes not fed by this pole at distances up to 700 metres away along the road.

Not a happy story, but at least now you needn't feel so sore if your sole loss is a frazzled modem costing £30. And no, you cannot sue British Telecom or the electricity company for taking inadequate care, as this incident would be termed an "Act of God". In any case, phone companies do take precautions; every phone socket contains a so-called spark gap to minimise the effect of over-voltages and all lines in BT exchanges are protected by an argon-filled gas discharge tube that conducts down to earth at high voltages. But when the over-voltage is in the region of six kilovolts at 200kA (200 thousand amps!), there's little that any safety component can do. Your only hope then is to pray.

ANY ANSWERS?

But what can you do? Certainly avoid using telephones and computers during thunderstorms and keep clear of video recording devices, TVs and mains radios. Tedious though it is, unplugging these devices may save you a lot of expense and inconvenience. It makes good sense to install surge-arresting plugs and telephone line filters too; the products made by a firm called Belkin (www.belkin.com) have a good reputation. Modern protection devices are remarkably sophisticated in fact and can work wonders. They don't guard against direct lightning hits, however, so don't be too judgmental if they fail to stop a 200 kilo-amp surge!

Of course, cheapskates always try to cut costs by assessing the likelihood of danger. For them saving £15 on surge arresters means far more than losing £1,000 on a multimedia computer system. They probably wouldn't take the same gamble with smoke detectors, yet the cost of surge protection is minimal by comparison with the benefits.

Lightning is not the only culprit, incidentally, and your equipment is at risk from less obvious hazards. Almost "invisible" spikes of very short duration but high voltage may lead to gradual deterioration or complete failure of the equipment. Repeated surges above normal line voltage but below the specified cut-off figure may also have a long-term effect of weakening components and lead to premature failure of semiconductor devices by altering their molecular structure.

SOME MYTHS DISPELLED

Lightning is not a problem round here... don't bank on it. Every day Britain sees more than 150 lightning strikes to ground and on average the country sees six hits per square mile annually. No district is immune, either, although some hotspots do exist. In summer the lion's share of thunderstorms occurs in eastern England, whilst in winter the epicentre is Cornwall (information from the Met. Office)

Our communications cables are all underground so they cannot be hit by lightning or contacts with power cables . . . A common misconception but entirely false, for two reasons:

When lightning strikes the ground it takes the path of least resistance; an underground copper cable will do very nicely and the massive electrical forces involved are quite capable of bursting through plastic sheathing. Additionally, floods in roadside cable chambers are common occurrences when water mains burst, with potentially disastrous consequences.

The insurance will pay out, so what the heck . . . ? An "All Risks" insurance policy will cover the cost of replacing damaged equipment; a "Fire and Special Perils" policy will not. It's vitally important to check for exclusions.

For anyone who works from home, however, the cost of disruption and lost work is far more important than is the replacement cost of equipment. Anyone totally reliant on the telephone or their computers for their livelihood may not be able to survive the consequent loss of income; while you recover lost data and replace ruined equipment your customers will take their business elsewhere.

NO FLASH IN THE PAN

Since 1989 the UK National Lightning Location Service has identified the position of lightning within the UK. This information is supplied to the insurance industry for evaluating actual lightning risk to property and has the possibility to validate insurance claims by referring to actual records of activity.

The service is provided by EA Technology Ltd (www.eatechnology.com), which has also developed a novel system that gives up to two hours prediction of the location of individual lightning strikes. This can locate strikes typically within 1km to a time accuracy of 0.01 seconds. Latest figures show that the number of lightning strikes that will affect an area can be predicted with an accuracy as high as a remarkable 85 per cent.

TEACH-IN 2004

Part One – At the Beginning

MAX HORSEY



How to apply electronics meaningfully – the aim of this 10-part series is to show, experimentally, how electronic components function as part of circuits and systems, demonstrating how each part of a circuit can be understood and tested, and offering advice about choosing components

A FIRST glance at an electronic circuit can be very off-putting; there are no moving parts, and it is impossible to know what is happening without a sound knowledge of how the components function and interact.

Throughout this series we ignore what is happening inside a component since all that matters in a circuit is the effect the component has on the current flowing. In other words we use the systems approach and examine what components do, and how they interact with other components.

MEASURING QUANTITIES

When you buy any item, its size or weight determines its suitability and cost. So you may buy 1kg of sugar, and 100m of string. Similarly, resistors are sold according to their resistance in ohms and their power in watts. Capacitors are measured in farads, and their working voltages in volts. We will discuss all these units in detail later, but since each unit has multiples, the chart shown in Table 1.1 may be helpful.

Note that micro (μ) is often written “u” if symbols are not supported by a printing system, and Ω is often written as “R”. For example, a 27 ohms resistor may be written 27 Ω or 27R. A 33,000 ohms resistor may be written 33k Ω or 33k.

(It used to be common to write 33k Ω as 33K. However, capital K has come to mean a kilobyte as used in computers, and this in turn means 1024 bytes – the nearest binary multiple of 10.)

PASSIVE COMPONENTS

When electricity flows through a resistance, electrical energy is converted into heat energy. This is how an electric fire works. The element of an electric fire is a resistor. Electronic circuits employ many resistors to reduce the flow of current and provide the range of voltages needed around the circuit – hopefully they do not become as hot as the electric fire element!

Electricity can produce several effects, including a “field effect”. For example, when you rub a balloon on your sleeve the

Table 1.1. Useful symbols and values

V = volts
A = amps
 Ω = ohms
F = farads

multiply by 1,000,000 10^6 M (mega) e.g. 1M Ω
multiply by 1,000 10^3 k (kilo) e.g. 1k Ω
multiply by 1 e.g. 1V
divide by 1,000 10^{-3} m (milli) e.g. 1mA
divide by 1,000,000 10^{-6} μ (micro) e.g. 1 μ F
divide by 1,000,000,000 10^{-9} n (nano) e.g. 1nF
divide by 1,000,000,000,000 10^{-12} p (pico) e.g. 1pF

balloon becomes charged with electricity and then attracts objects with a different charge. Hence the balloon will stick to a wall, which is neutral (which counts as a different charge to the balloon). The field effect is exploited in a capacitor, and in some types of semiconductor.

A flow of electricity produces a magnetic effect. When a wire is wound into a coil the magnetism is concentrated. A coil wound around a piece of soft iron is called an electromagnet; it can be turned on and off as required. A hollow coil is called a solenoid and can pull pieces of iron or steel into its centre. This mechanism is employed in electric locks.

In electronic circuits coils of wire are often known as inductors. In practice you will rarely, if ever, need an inductor (other than in radio circuits, or as an output device – like a solenoid), and so we will cover this area briefly.

The preceding components all lose energy – in other words they are *passive*. However, the invention of the thermionic valve – an *active* device – increased the potential of electronic circuits immensely and led to the “radio set” complete with “radio valves” and loudspeaker. For many years, electronics was essentially for radio; one of the most famous component suppliers, RS Components, was originally called Radio Spares.

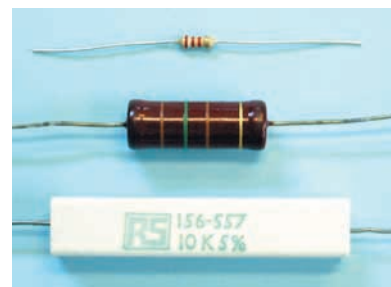


Photo 1.1. Examples of typical resistors. Top to bottom 0.25W, 2W, 11W.

RESISTORS

Resistors are probably the most common component in electronic circuits. Three resistors are shown in Photo 1.1, the most common of which is the smallest. Resistors are designed to waste electrical energy, and in the process they convert it into heat. Hence they are employed to reduce the flow of current, and help create the correct voltage for a particular section of a circuit. A resistor obeys Ohm’s Law, whereby:

Resistance (in ohms) = Voltage/Current

For example, we can calculate the current flowing in Fig. 1.1 if we know the value of the resistor, and the voltage across the resistor – which in this case is the supply voltage. So, with 9V across the resistor, and a resistance value of 100 ohms, we can change round the formula, namely:

Current = Voltage/Resistance

hence:

Current = 9/100 = 0.09 amps = 90mA

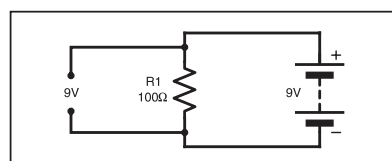


Fig. 1.1. Current flow example.

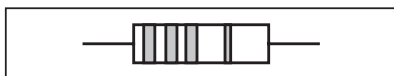


Fig.1.2. A 4-band resistor.

COLOUR CODES

The value of a resistor is indicated by means of a colour code. Consider a 4-band resistor as shown in Fig.1.2, where the last colour is gold.

Assuming that the last band is gold, the value should be read with the gold band on the right-hand side. The first band indicates the first digit, the second band indicates the second digit, and the third band indicates the "multiplier".

Table 1.2 illustrates this. Each colour represents a value, from lowest – black, to highest – white. The last band indicates the tolerance of the resistor, i.e. an indication of its accuracy. Gold means 5% tolerance (good enough for most purposes), red indicates 2% and brown indicates 1%. A 5% resistor whose colours indicate 100 ohms could have a value from 95 ohms to 105 ohms, i.e. 5% either way. For example:

red, red, red, gold = 2 2 00 ohms (2k2 ohms), 5% tolerance

brown, black, green, gold = 1 0 00000 ohms (1M ohms), 5%

brown, black, black, gold = 1 0 ohms (10 ohms), 5%

orange, orange, orange, gold = 3 3 000 ohms (33k ohms), 5%

Note how in the first instance the letter *k* is used in place of the decimal point.

FIVE-BAND RESISTORS

Five-band resistors (see Table 1.3) simply contain an extra digit, but otherwise they are similar to the four-band types. The extra band allows a more accurate value to be indicated, and so five-band resistors will generally have a tolerance of 1%. This means that the fifth band is brown, making it much harder to know which way round the resistor is read.

Resistor values conform to a system, e.g. the E24 series, and so if the value you have read is not included in the series, you must have the resistor the wrong way round. If all else fails, use a multimeter to measure the resistance!

POWER RATING

Resistors convert electrical energy into heat energy. In most circuits the current

PANEL 1.1. SCHEDULE FOR THIS SERIES

Part 1: At the Beginning

Revisiting passive components, and a few input/output devices.

Part 2: Transistors

Bipolar and MOSFET transistors, with example circuits, including a voltage controller and a simple amplifier.

Part 3: Operational Amplifiers

Useful op.amp circuit configurations, plus example circuits for an audio mixer and microphone amplifier.

Part 4: Logic Gates

Basic logic gates and how to use them in practical applications, including a Quiz Game Controller.

Part 5: Logic Gates as Switches

Logic gates as switches, with special reference to audio applications, and introducing PIC microcontrollers to reduce the chip count.

Part 6: Sound Level Measurement

Sound level measurement, with example detection and display circuits using op.amps, i.e.d.s and bargraphs, and illus-

trating how data sheets can be turned into real circuits.

Part 7: Moisture Detection and Radio Links

Methods for detecting moisture, and how data can be reliably transmitted via a variety of radio link modules.

Part 8: Movement Detection

Exploring methods for detecting movement, with special regard to avoiding Deep Vein Thrombosis, associated with personal immobility on a coach or aircraft, concluding with a PIC-based "movement reminder".

Part 9: Lock and Alarm Systems

Hard-wired and logic gate control of alarm and lock systems, including use of thyristors and matrixed keypads, and how to use PICs for decoding keypads.

Part 10: Motor Control

Exploring reversible motor control, with the use of switches, light and current sensing to provide automatic "stop" constraint, concluding with an example of a PIC-based curtain winder.

flowing through each resistor is so small that the heat produced can be ignored. But low-value resistors can produce significant amounts of heat, as can higher value resistors operating at high voltage. The power formula is:

$$\text{Power} = \text{Voltage} \times \text{Current}$$

So if you know the current flowing through a resistor, and the voltage across it, the power (in watts) can be calculated.

The power rating of a typical resistor used in circuits is around 0.25W. Looking again at Photo 1.1 a resistor of this rating is shown at the top, together with a 2W resistor, and 11W resistor.

VARIABLE RESISTORS (POTENTIOMETERS)

As the name suggests, a variable resistor is a resistor whose resistance can be varied from zero to the value stamped on its case. It is common practice to build variable resistors with connections at both ends, and a "wiper" in the centre. A symbol for this device is shown in Fig.1.3.

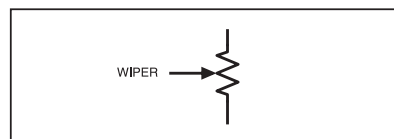


Fig.1.3. Basic symbol for a potentiometer.

If you use the wiper, and one end of the device, it behaves as a variable resistor. If you use all three connections, the device can be used as a potentiometer (often abbreviated to *pot*). The term potentiometer is that normally used irrespective of the application.

The pots shown in Photo 1.2 illustrate some examples, including the linear slider, popular in mixers and graphic equalisers. Photo 1.3 shows some miniature pots, known as presets. These are operated with a screwdriver, and are useful if their values are changed very infrequently. Note that some are designed for horizontal mounting on a circuit board, and others stand vertically. Dual-gang pots are available as shown in Photo 1.4, and are useful as the volume controls in stereo amplifiers.

Table 1.2. 4-band resistor colour coding

	1st digit	2nd digit	multiplier	tolerance
GOLD			divide by 10	5%
BLACK	0	0	none	
BROWN	1	1	× 10	1%
RED	2	2	× 100	2%
ORANGE	3	3	× 1000	
YELLOW	4	4	× 10000	
GREEN	5	5	× 100000	
BLUE	6	6	× 1000000	
VIOLET	7	7	× 10000000	
GREY	8	8	× 100000000	
WHITE	9	9	× 1000000000	

Table 1.3. 5-band resistor colour coding

	1st digit	2nd digit	3rd digit	multiplier	tolerance
GOLD				divide by 10	5%
BLACK	0	0	0	none	
BROWN	1	1	1	× 10	1%
RED	2	2	2	× 100	2%
ORANGE	3	3	3	× 1000	
YELLOW	4	4	4	× 10000	
GREEN	5	5	5	× 100000	
BLUE	6	6	6	× 1000000	
VIOLET	7	7	7	× 10000000	
GREY	8	8	8	× 100000000	
WHITE	9	9	9	× 1000000000	



Photo 1.2. Example of panel mounting single potentiometers.

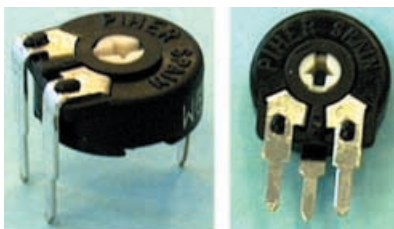


Photo 1.3. Example of p.c.b. mounting preset potentiometers.

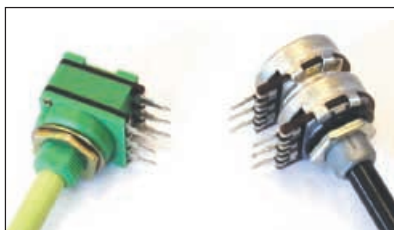


Photo 1.4. Example of panel mounting dual potentiometers.

LINEAR OR LOG

Most potentiometer values are available as linear (lin) or logarithmic (log) types. For most purposes the linear type is best, since the resistance changes evenly as the control is rotated. Log pots are generally used as volume controls in amplifiers, where the sound level needs to rise in ever greater steps – in tune with the way in which humans hear sound.

RHEOSTATS

A rheostat is a type of variable resistor, and will be looked at in more detail in Part 2, next month.

CAPACITORS

A capacitor temporarily stores electricity. This should not be confused with the function of a battery, which chemically



Photo 1.5. A dramatic (but dangerous) illustration that a capacitor stores electrical charge (see text).

PANEL 1.2. TOOLS AND EQUIPMENT

One of the advantages of experimental electronics is that it need cost very little. In fact, now that digital multimeters have fallen in price, the most expensive single item may well be a prototype board – a system which enables components to be plugged into it and connected together temporarily for testing and trialling. So a basic shopping list would be as follows:

- Prototype board (plug-in breadboard)
- Wire strippers/cutters
- Screwdrivers
- Small pliers
- Digital multimeter

A proposed list of the electronic components required for this series is shown

below. The quantities given assume that components are re-used between the different parts of the series. Be aware that there may be minor changes or additions to the list as the series progresses.

Throughout this series a 9V PP3 battery can power most of the circuits, even where 12V is suggested.

If serious experimental or faultfinding work is planned for the future, an oscilloscope will be useful, though this will cost far more than everything else put together! It is not necessary to the successful following of this series.

Anyone wishing to construct circuits permanently will need a few small stripboards, a small soldering iron and multi-core solder.

COMPONENTS

Approx. Cost
Guidance Only

£27
excl. misc.

(Assumes that some components are re-used between different parts)

Resistors

- 8 Ω 3W
- 12 Ω
- 100 Ω
- 330 Ω (7 off)
- 470 Ω (2 off)
- 680 Ω
- 1k (5 off)
- 2k2
- 4k7 (4 off)
- 10k (3 off)
- 22k (6 off)
- 47k (3 off)
- 51k
- 82k
- 100k (4 off)
- 680k (2 off)
- 1M (3 off)

All 0.25W 5% unless marked.

Potentiometers

- 1k
- 10k (3 off)
- 22k
- 47k
- 100k
- 470k
- 1M

All preset or panel mounting rotary linear.

Capacitors

- 100n disc or polylayer etc. (6 off)
- 470n disc or polylayer etc.
- 1 μ polylayer (2 off)
- 1 μ radial elect. 16V
- 2.2 μ radial elect. 16V
- 4.7 μ radial elect. 16V (2 off)
- 10 μ radial elect. 16V (3 off)
- 100 μ radial elect. 16V
- 220 μ radial elect. 16V (2 off)
- 470 μ radial elect. 16V
- 1000 μ radial elect. 16V

All working voltages quoted are the minimum. Higher voltage ratings may be used.

Semiconductors

- 1N4001 rectifier diode (4 off)
- 1N4148 signal diode (3 off)
- 3V9 Zener diode, e.g. BZVC3V9

See
SHOP
TALK
page

- BC549 npn transistor (or any high-gain npn type, e.g. 2N3704) (3 off)
- BC214 pnp transistor (or any high gain pnp type, e.g. 2N3702)
- TIP122 (or TIP121) npn Darlington transistor (3 off)
- TIP127 pnp Darlington transistor
- TIP41A npn power transistor (2 off)
- TIP42A pnp power transistor (2 off)
- BUZ11A n-channel MOSFET
- 741 op.amp
- 4001B quad 2-input NOR gate
- 4011B quad 2-input NAND gate
- 4069UB hex inverter
- 4081B quad 2-input AND gate
- 4071B quad 2-input OR gate
- 4050B hex buffer
- 4052B dual 4-input analogue multiplexer
- PICAXE-18 or PIC16F627 microcontroller (see text Part 8)
- LB1412 VU i.c.
- HT12E encoder
- HT12F decoder
- 78L05 +5V 100mA voltage regulator
- ICL7660 voltage converter

Miscellaneous

- AM-RT4-433 radio transmitter module
- AM-HRR3-433 radio receiver module
- d.p.d.t. toggle switch
- s.p. push-to-make switch (4 off)
- Microswitch (optional)
- Torch bulb (e.g. 3V) (2 off)
- Electret microphone insert
- Red l.e.d. (12 off)
- Green l.e.d. (2 off)
- Bi-colour l.e.d.
- Relay, 12V coil (optional)
- Shrouded 3-pin header (only required for PICAXE)
- Stripboard for moisture sensor (4cm x 3cm) (see text Part 4)
- Buzzer (solid state)
- Siren (loud buzzer), any 6V to 12V type
- Vibration switch, any type
- Matrix keypad, 12-key
- Solenoid lock (optional), any 12V type
- Thermal fuse 1A
- Motor and gearbox, e.g. Rapid 37-1238 or RS 336-337
- Miniature 12 l.d.r.
- Thermistor, n.t.c., 5k Ω at 25°C

generates electricity. A capacitor can be likened to the water storage tank in your loft; a battery is like the central heating pump pumping the water around the radiators.

You can conduct a very crude experiment to show that a capacitor stores electricity, as shown in Photo 1.5. Here we have taken a large electrolytic capacitor, and charged it from a power unit by connecting its terminals directly to the 12V supply from a power supply unit.

WARNINGS:

- This experiment may damage the capacitor, so use an old one!
- Always check that the capacitor is connected the correct way round i.e. positive of the capacitor to positive of the power supply, and check that the working voltage of the capacitor is higher than the voltage of the supply.

Now disconnect the capacitor from the supply, and place a screwdriver across its terminals. The large spark illustrates that it was charged. (NOTE: shorting a capacitor in this way may cause it damage).

Photo 1.6 shows a more elegant, if less dramatic illustration. A buzzer is connected to the capacitor and it will sound for some time, though the changing note from the buzzer indicates that the voltage is falling quite rapidly.

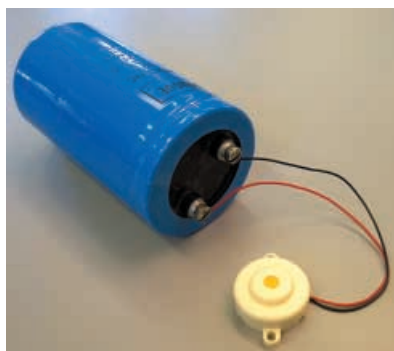


Photo 1.6. Audibly demonstrating that a capacitor stores electrical charge.

A battery of the same physical size as the capacitor would work the buzzer for very much longer. Hence capacitors are not very effective when used as rechargeable batteries. They can only be employed in this way for use in very low consumption circuits – such as keeping the clock going for an hour in your video recorder during a power cut!

The storage ability of a capacitor is measured in farads (in honour of Michael Faraday, one of Britain's greatest scientists). In practice we require smaller units such as microfarads (μF), nanofarads (nF) and picofarads (pF):

$$\begin{aligned} 1\text{F} &= 1,000,000\mu\text{F} \\ 1\text{F} &= 1,000,000,000\text{nF} \\ 1\text{F} &= 1,000,000,000,000\text{pF} \end{aligned}$$

or put another way:

$$\begin{aligned} 1\mu\text{F} &= 10^{-6}\text{F} \\ 1\text{nF} &= 10^{-9}\text{F} \\ 1\text{pF} &= 10^{-12}\text{F} \end{aligned}$$

USING CAPACITORS

Capacitors, like resistors, are so widely used that whole books are written about

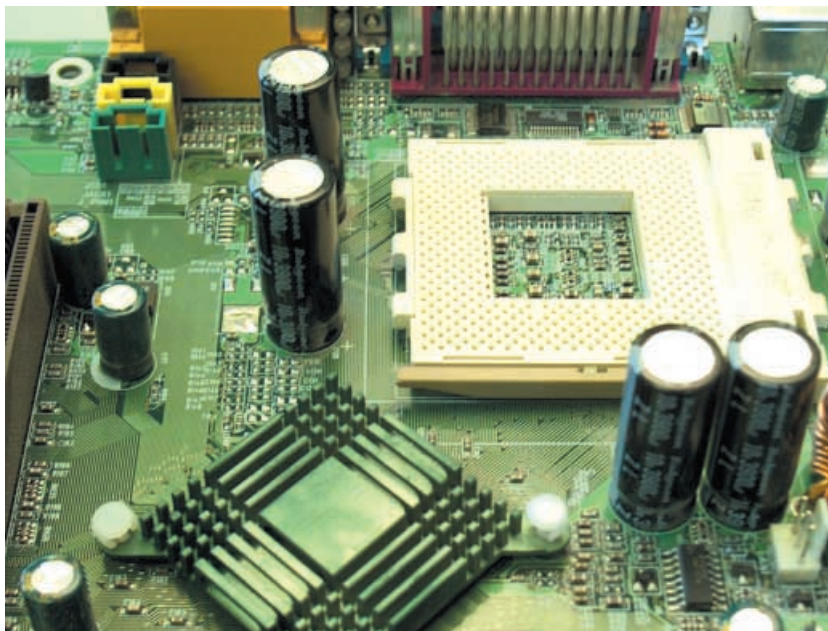


Photo 1.7. Electrolytic capacitors can dominate even the most sophisticated of circuit boards.

them. So we will just summarise some applications, and see them in action throughout this series. Capacitors are used for:

- storing small amounts of electrical energy
- smoothing (decoupling) power supplies
- removing voltage spikes from power supplies
- timing circuits
- oscillator circuits
- radio tuning
- tone control circuits
- blocking d.c. whilst coupling a.c.

TYPES OF CAPACITORS

Capacitors tend to be rather bulky when compared with other components. The circuit board in Photo 1.7 shows part of a computer motherboard, where the black dots are tiny surface mount resistors, transistors and diodes. As the name suggests, these components are soldered on the upper surface of the p.c.b. and are ideal for mass production.

But standing like sky-scrapers are the capacitors (electrolytic in this instance), almost as if from another age. Some very small capacitors are capable of being surface mounted like resistors, but large value capacitors take up a large amount of space. Open up a hi-fi amplifier and you will find that nearly half the case is filled with the power transformer and capacitors.

The reason for an electrolytic capacitor's size is that it is comprised of two metal foil conductors, separated by an insulator. The whole thing can be rolled up like a Swiss roll, and although the conductors and insulator can be made very thin, there comes a point where the insulator is so thin that it breaks down when voltage is applied. So capacitors have a voltage rating known as a *working voltage*, above which you **should not** go!

Non-electrolytic (i.e. "normal") capacitors tend to have a reasonably high working voltage, typically 100V. The insulator may be made of polyester, polystyrene, mica, etc., and the size, shape, price and

effectiveness tend to depend on the type of insulation employed.

Rolled-up capacitors can have an inductive effect. This may be of no consequence in many circuits, but is best avoided where possible. So particular capacitors, such as "polylayer" types, are available which are not rolled-up and are useful in many circuits, including audio amplifiers and tone networks.

Using a non-electrolytic capacitor of a type different to that specified in a given component list is unlikely to prevent most circuits from working, providing the working voltage of the capacitor is sufficiently high, and it physically fits into the space provided on the circuit board. The price of "expensive" types of capacitor has fallen over recent years, and so there is often little point in the home-constructor using "cheaper" types.

ELECTROLYTIC CAPACITORS

Electrolytic capacitors are polarised – in other words – they must be connected the correct way round with respect to positive and negative voltages. If you connect an electrolytic capacitor the wrong way round it is likely to explode. Photo 1.8 shows an

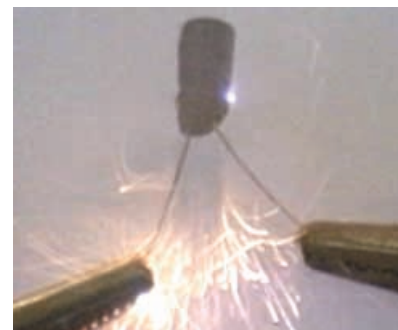


Photo 1.8. The dangerous effects of connecting an electrolytic capacitor to the wrong power supply polarity (photo created in a protected environment – see text).

experiment where a small electrolytic capacitor was connected with the wrong polarity to a 12V supply.

WARNING: The experiment was conducted inside a sealed container, in a laboratory – do NOT try this at home!

Electrolytic capacitors provide a large storage capacity in a reasonably compact case and at a reasonable cost, when compared with non-electrolytic capacitors. Their voltage ratings can be as low as 3V, so watch this when selecting your capacitor. In general, buy a capacitor with a voltage rating (i.e. working voltage) higher than the power supply voltage employed in your circuit.

There are two package types commonly employed – axial capacitors, and radial capacitors, as shown in Photo 1.9. An axial type (on the right-hand side) is designed to lie down like a resistor; a radial type has both its leads extending from the same end, and so stands upright and takes up less space on the circuit board. For this reason, radial capacitors are more commonly used.

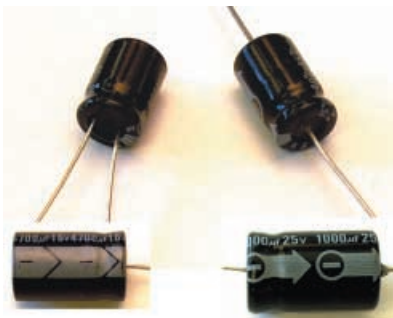


Photo 1.9. Examples of radial (left) and axial (right) electrolytic capacitors.

Notice that a band on the side of the body indicates the negative side of both types of capacitor. Additionally, in the case of a radial capacitor, positive is indicated by the longer lead

TOLERANCE

No component can be manufactured perfectly, and all are made to a certain accuracy or tolerance. Electrolytic capacitors are notoriously imperfect and the actual value may be between half the stated value, or up to double the stated value. Fortunately, the *actual* value of an electrolytic capacitor is often not important, and circuit designers are used to making allowances for electrolytic capacitors!

LEAKAGE

The plates of an electrolytic capacitor are not as well insulated as non-electrolytic types, and current can “leak” between the plates. This can adversely affect some circuits. For example, a popular timing circuit based on a chip known as a 555 timer measures the rising voltage on a capacitor, which is being charged via a resistor.

If times of several minutes are required, the resistor needs to restrict the flow of current so that the capacitor charges very slowly. You can use a larger capacitor to increase the timed period still further, but the size required to permit times of up to one hour, for instance, increases the risk of “leakage” which in turn affects the accuracy.

This can be very frustrating, when your calculations no longer work in practice!

TANTALUM BEAD CAPACITORS

Tantalum bead capacitors are a form of electrolytic capacitor but have a better tolerance rating, and are generally smaller. They also have better leakage ratings (i.e. leak less), but – as you would expect – are more expensive.

INDUCTORS

An inductor is a coil of wire either hollow, or wound around some ferrous (magnetic) material. When current flows through the coil a magnetic field is produced. When the current stops flowing the magnetic field collapses. If the coil is connected to a d.c. supply, a steady current will flow, and the opposition to the flow will be mainly due to the resistance of the wire used to make the coil.

However, at the moment when the current is switched on or switched off the rising or falling magnetic field also opposes the flow of current. This means that if an alternating supply is connected to the coil the opposition to the flow is greater than that due to the resistance alone.

The amount of opposition to a.c. depends upon the wire used, the number of turns, type of material inside the coil etc., and the effect is known as the inductance of the coil. Inductance is measured in henrys, and a small inductor may have a value of, say, 10mH.

There is also some capacitance associated with the coil, and this too affects the way it behaves with a.c. So the whole effect due to the resistance of the wire, the inductive effect and capacitive effect is summed up by referring to the impedance of the coil. Impedance is the total opposition to a.c. and will depend upon the a.c. frequency.

You will probably know that one of the important loudspeaker measurements is its impedance. If your amplifier has an output impedance of 8Ω, then you need a speaker of 8Ω impedance if you wish to extract the maximum power.

Inductors are often used to reduce voltage spikes in a circuit – in fact you often see ferrous material wrapped around mains leads or other leads associated with computers, video recorders etc. Inductors are also used in radio tuning, and combined with capacitors can form a “tuned circuit” i.e. one which resonates with a particular frequency – to tune in your favourite radio station for instance.

TRANSFORMERS

A transformer normally consists of two or more coils of wire wound around a common core. Transformers which are designed to operate on 50Hz or 60Hz (the European/US mains frequencies) have cores made from laminated soft iron. The laminations (insulated sections) prevent the core acting like a coil of wire and conducting electricity.

When a.c. is applied to one coil known as the primary, a voltage of the same frequency is induced in the other coil known as the secondary. The voltage produced is in exact proportion to the ratio of turns. In other words:

$$\frac{\text{Output voltage}}{\text{Input voltage}} = \frac{\text{Secondary turns}}{\text{Primary turns}}$$

If the secondary coil has more turns than the primary, the transformer is known as a “step-up” type. However, the power output can never be greater than the power input (that’s a law of nature – you can’t get something for nothing!), and so the current available from the secondary coil is reduced by the same ratio.

The majority of electronics projects that require a transformer employ a “mains type”. These generally step down the voltage. For example, a mains transformer with a ratio of 20:1 will change an input of 230V a.c. down to 11.5V a.c.

Remember that transformers only work with a.c., and the current available from the secondary will be determined by the thickness of the wire used. If you require a large current, you need to obtain a larger, more expensive transformer.

A 20:1 ratio transformer which offers a current of, say, 1A from its secondary will consume 1/20A from the mains supply. These figures assume that the transformer is 100% efficient. In practice they are around 98% or worse.

Small mains transformers – the type often needed in projects – have quite poor “regulation”. This means that the output voltage claimed will only be correct when the current used from the secondary is near the maximum allowed. If less current is used, the output voltage will rise – by up to 25% or more. So a 12V transformer may supply a voltage of 15V or more when “off load”.

DIODES

A diode allows current to flow in only one direction. Sounds easy – but whole books have been written on the development of the diode, including such classics as the thermionic radio valve and the “crystal and cats whisker”. Our present solid state diodes owe their existence to the latter device, although their development took a surprisingly long time.

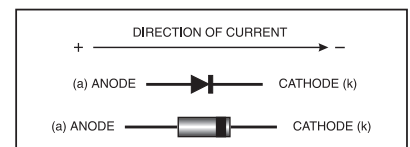


Fig.1.4. Diode symbol and polarity markings.

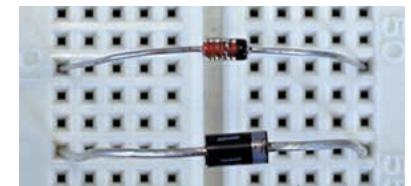


Photo 1.10. A 1N4148 (top) signal diode and a 1N4001 rectifier diode.

The symbol for a diode is shown in Fig.1.4. Note the direction of the current through the diode. Fig.1.4 also shows how the band around the real life diode corresponds with the cathode end of the symbol. Two common diodes are shown in Photo 1.10. The upper is a type 1N4148, and the lower is type 1N4001.

In all the following experiments, a type 1N4001 diode has been employed.

USING DIODES

- Protecting against reverse polarity
- Steering applications
- Radio detection
- Rectification
- Protection from back e.m.f.

Protecting against reverse polarity

Most electronic circuits will be damaged if you connect the power supply or battery the wrong way round. You can protect against this event by connecting a diode in series with the power supply as shown in Fig.1.5.

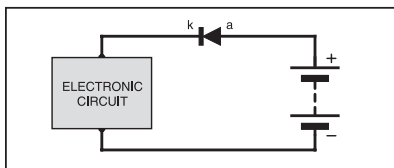


Fig.1.5. Common method of using a diode to protect a circuit against reverse power supply connection.

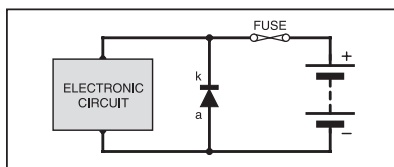


Fig.1.6. Another method of protecting a circuit, using a diode and a fuse.

If the battery is reversed, the diode will prevent any current flowing. The only problem with this arrangement is that the diode loses about 0.7V. So if you are using a 3V battery, the voltage applied to your circuit will be only 2.3V.

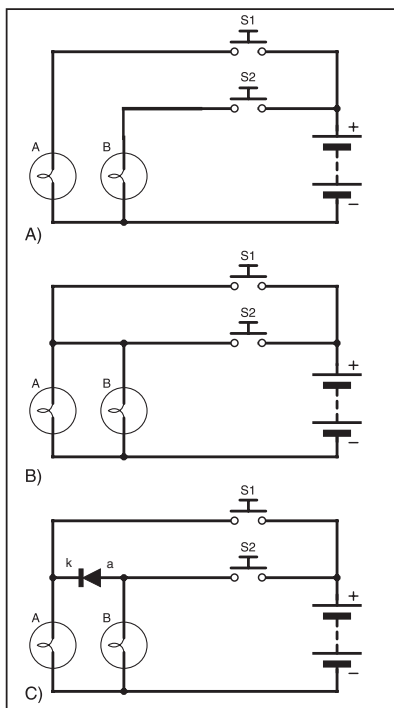


Fig.1.7. Using switches to control lamps, (a) individual switching, (b) dual-control of both lamps, (c) controlling lamp A by S1, but both lamps by S2, by using a steering diode.

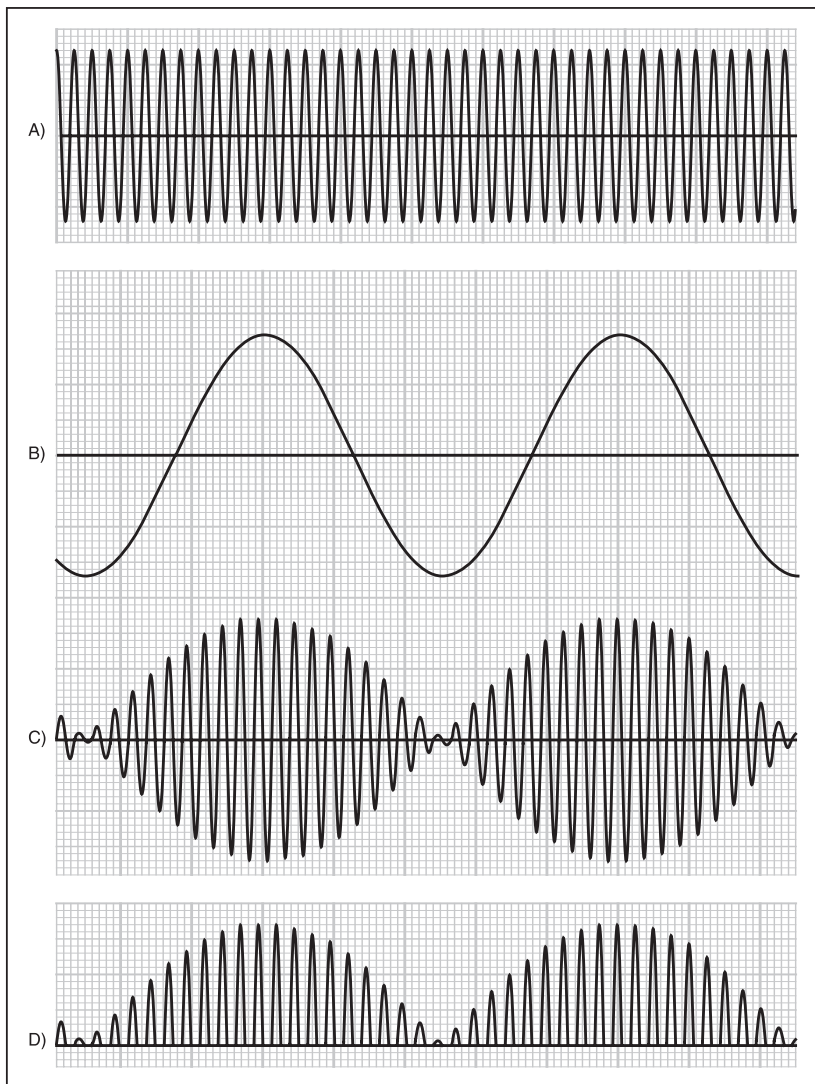


Fig.1.8. Principle of amplitude modulation (AM), (a) the carrier signal, (b) modulating signal, (c) the effect of modulating a by b, (d) half-wave rectification of c.

Hence the arrangement shown in Fig.1.6 is sometimes used. The diode will be “invisible” when the battery is connected correctly, but if the supply is reversed, the diode will short-circuit the current and the fuse will blow. A blown fuse is a much better option than a destroyed circuit.

Steering

Steering applications probably account for the greatest use of diodes, particularly in logic circuits. An example will illustrate the point:

The circuit in Fig.1.7 show two lamps A and B controlled by means of two pushbutton switches, S1 and S2. We require button S1 to light lamp A, and button S2 to light both lamps. The wiring for dedicated lamp switching is shown in Fig.1.7a.

However, when S2 is connected to both lamps (Fig.1.7b), we find that S1 lights both lamps as well. The solution is shown in Fig.1.7c. A diode is used to steer the current so that S2 can light lamps A and B, but S1 can only light lamp A.

Radio detection

A full description of radio is beyond the scope of this article, but the principle of Amplitude Modulation (AM) is easily explained.

A radio wave can carry audio information (e.g. speech or music) by superimposing or modulating the radio wave (known as the carrier) with the audio signal. The graphs in Fig.1.8 illustrate the point.

An example radio wave is shown in Fig.1.8a. This is simply a sinewave oscillating at high frequency. Fig.1.8b shows an audio signal – in this case a sinewave of much lower frequency than the radio wave. Fig.1.8c shows the radio wave modulated by the audio signal – its amplitude pulses up and down in synchronisation with the audio signal.

When the modulated radio wave is received by a radio set, the audio signal is recovered by removing all the waves below the centre line, i.e. removing the negative part of the signal. This is the part played by the diode in the “detection” circuit.

We now have the signal as shown in Fig.1.8d – which resembles quite closely the original audio signal. The high frequency radio signal is ignored by your headphones or loudspeaker, which responds to the “tops” of the signal. In practice, the high frequency radio signal can be removed by a capacitor, leaving the audio signal, which is similar to that shown in Fig.1.8b.

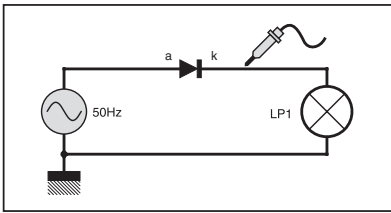


Fig.1.9. Experiment illustrating half-wave rectification.

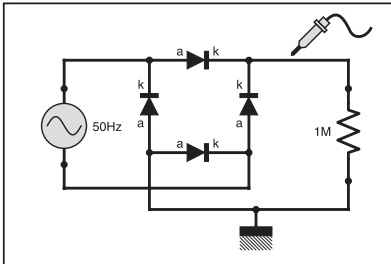


Fig.1.11. Experiment illustrating full-wave rectification.

Rectification

In the previous example, the diode removes the negative parts of the radio signal. In other words we are changing the signal, which pulses above and below 0V, into a signal that pulses only above 0V. This is illustrated in Fig.1.9 and Fig.1.10.

In Fig.1.9 an a.c. generator is shown connected via a diode to a lamp. The upper graph in Fig.1.10 shows the a.c. waveform, and the lower graph shows the effect of the diode, which removes the negative parts of the waveform. Hence, we are left only with the positive part of the waveform i.e. a half-wave.

A single diode can therefore be used as a half-wave rectifier. Note that the half-wave is d.c., i.e. it always flows in the same direction, even though it is pulsing. This type of d.c. is inefficient, and full-wave rectified d.c. is generally preferred.

Full-wave d.c.

There is more than one way of converting a.c. into full-wave d.c., but since diodes cost just a few pence, a useful method is by wiring the diodes into a "bridge" formation, hence the term *bridge rectifier*.

The four diodes are connected as shown in Fig.1.11, and the resulting graph is shown in Fig.1.12. Notice that unlike the previous graph, the gaps have been filled to

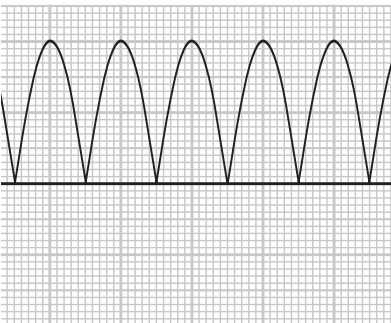


Fig.1.12. Full-wave rectification converts an a.c. signal into d.c. but retains the "ripples" of the a.c. waveform.

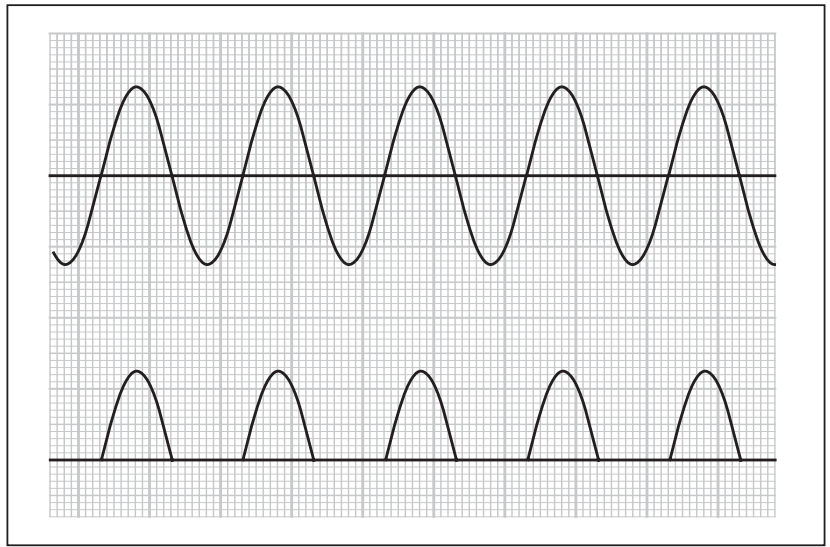


Fig.1.10. Sinewave before (top) and after half-wave rectification.

make full-wave d.c. Full-wave d.c. still wobbles up and down, but is much more efficient than half-wave d.c. Also, with smaller gaps, it is much easier to smooth into a steady flow of d.c.

WARNING: When experimenting with diodes, ensure that current is able to flow through the diodes by using a lamp (as in the half-wave circuit) or a resistor to provide a "load", as shown in Fig.1.11. Also, with the full-wave circuit, if you are using an oscilloscope (see Panel 1.3 later) to view the waveform, the oscilloscope ground (0V) must be connected only to the d.c. side of the bridge. You cannot, for example, use a double beam oscilloscope to monitor the a.c. and d.c. sides of the circuit at the same time.

The 4-diode bridge circuit is so often required that bridge rectifiers are available as single packages containing the four diodes, as shown in Photo 1.11. Notice that the positive and negative connections are marked on the top of each rectifier. The larger device can handle several amps, the smaller is rated at just over 1A.

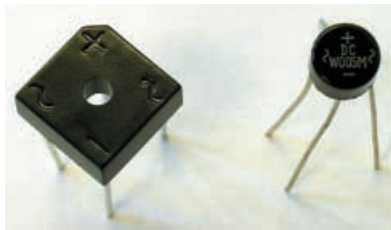


Photo 1.11. Examples of bridge rectifiers.

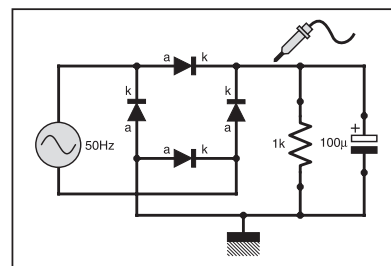


Fig.1.13. Smoothing a full-wave rectified signal.

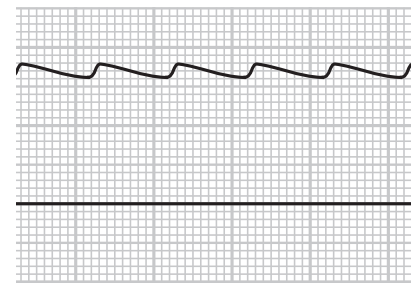


Fig.1.14. A ripple signal remains if inadequate smoothing is given to a full-wave rectified signal.

Smoothing

Electronic circuits require a smooth d.c. supply – the type provided by a battery. With rectified d.c. this is achieved by means of a capacitor as shown in Fig.1.13.

If a capacitor value of 100µF is used and the load is 1MΩ, then the graph will be a perfectly straight line, since very little current flows through the 1MΩ resistor. However, if the resistor value is reduced to 1kΩ, then several milliamps flow through the resistor and noticeable ripple occurs. The difference is illustrated in Fig.1.14.

A larger capacitor value will reduce the ripple, but if the amount of current required by your circuit (as represented by the resistor) is 1A or more, then very large value capacitors are required. Hence the capacitors inside your hi-fi power amplifier will be very large indeed.

Back-e.m.f. protection

Many output devices produce a high voltage spike when they switch off. This includes all magnetic devices such as

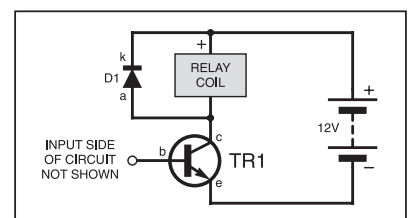


Fig.1.15. Using a diode to eliminate back-e.m.f.

motors, relays and solenoids. The high voltage spike, known as back-e.m.f. (e.m.f. = electromotive force), can damage sensitive components such as transistors and integrated circuits (i.c.s).

The circuit shown in Fig.1.15 illustrates the point. Here a transistor is used to switch a relay on and off. We won't worry about the input side of the circuit. When the transistor turns on, current flows through the relay coil. When the transistor turns off, the current through the relay coil stops, but the magnetism remains for a moment.

As the magnetic field collapses it is like pulling a magnet out of a coil at high speed – and this induces a voltage (e.m.f.) across the coil. Most transistors can only tolerate voltages of 30V or so but the e.m.f. (which is in the opposite direction to the normal supply voltage – hence “back-e.m.f.”) may be 50V or more, so the transistor is destroyed.

Diode D1 acts as a short-circuit to the back-e.m.f. and so removes the danger. However, the diode faces the wrong way for the normal supply voltage, and so does not affect the circuit in any other way.

It is possible to detect the high voltage produced when a relay switches off by placing your finger across the contacts connected to its coil. Connect one side of a power supply (e.g. 12V) to one side of the coil, connect a second lead to the other side of the power supply, and touch its end against the spare side of the relay coil.

Each time you brush the lead against the coil connection you should feel a small current. It helps if you use a large old-fashioned relay such as that shown in Photo 1.12.

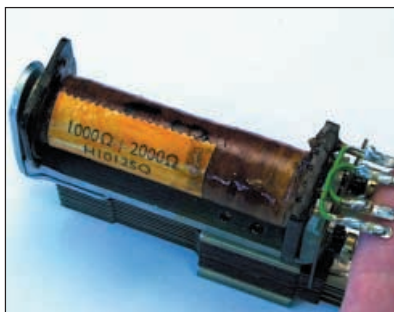


Photo 1.12. An old-fashioned relay, suitable for a back-e.m.f. experiment.

SELECTING A DIODE

When selecting a diode the following considerations apply:

Forward voltage drop (V_F)

When current flows through a diode, there is a voltage drop across it. In other words, some of the voltage is lost. The figure of 0.7V quoted earlier applies to silicon diodes. If this is too large a value, and you are dealing with small currents, you can employ a germanium diode such as type OA91, whose voltage drop is about 0.3V. Hence this type is more appropriate for simple radio receivers.

Forward current (I_F)

Diodes are rated according to the current they can pass. For example, type 1N4001 can carry up to 1A. Type 1N4148 can carry 150mA.

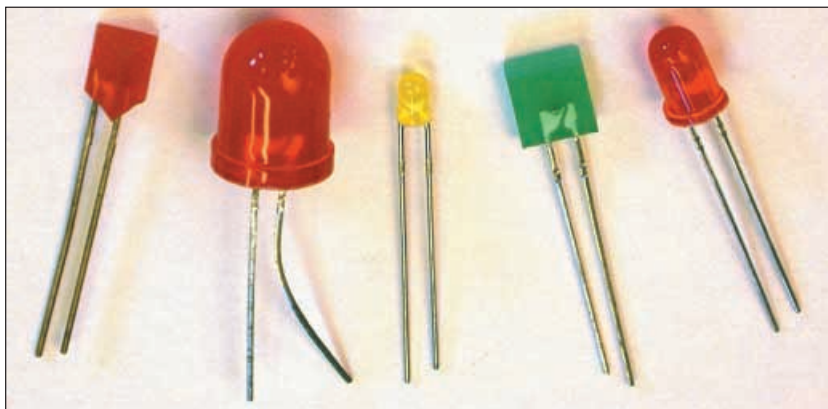


Photo 1.13. Examples of l.e.d. types.

Peak Inverse Voltage (PIV)

The peak inverse voltage is the maximum voltage a diode can withstand in the reverse direction. For example, the 1N4001 diode can tolerate up to 50V. Type 1N4002 has a PIV of 100V, type 1N4003, 200V, and type 1N4004 has a PIV of 400V – making it useful for mains voltages. The popular 1N4148 has a PIV of 75V.

LIGHT EMITTING DIODES

A light emitting diode (l.e.d.) is a special type of diode that emits light when current flows through it. L.E.D.s can be obtained in a range of colours and sizes, as illustrated in Photo 1.13. Note that the longer lead indicates the anode (positive) side of the l.e.d.

Most general purpose l.e.d.s require a current of around 10mA to 20mA, though special “low-current” l.e.d.s are available. The PIV is typically 5V (something to watch as it is much lower than an ordinary diode) and the forward voltage drop is around 1.7V for red l.e.d.s, 2.3V for yellow and green, and over 4V for blue.

A diode provides a low-resistance path in its forward direction. Hence if you connect a diode, including an l.e.d., across a power supply in the forward direction, a short-circuit current will flow, destroying the l.e.d. in the process. So a resistor is required as shown in Fig.1.16.

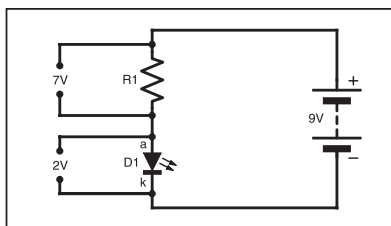


Fig.1.16. A resistor must be used in series with an l.e.d. to prevent excessive current flow.

Calculating the resistor value

We calculate the resistor value by means of Ohm's Law, namely,

$$\text{Voltage} = \text{Current} \times \text{Resistance}$$

where Voltage is the voltage across the resistor, and Current is the current flowing through the resistor (and the l.e.d.).

A catalogue itemising the l.e.d. might tell us that the forward voltage drop across the l.e.d. is 2V (probably about 1.8V, but we will call it 2V). Assuming a 9V supply, this leaves 7V across the resistor.

We know from the catalogue that a suitable current through the l.e.d. is about 10mA. The same current flows through the resistor. So we have 7V across the resistor, and 10mA (i.e. 0.01A) flowing through it.

From Ohm's Law:

$$R = V/I, \text{ so } R = 7/0.01 = 700 \text{ ohms.}$$

The nearest conventional resistor value available is 680 ohms.

The calculation can be reduced to a single formula:

$$R = \frac{V_s - V_d}{I}$$

where

R = resistor value

V_s = supply voltage

V_d = l.e.d. voltage drop

I = current through l.e.d.

The assumption of 2V forward voltage drop is adequate for red, green and yellow l.e.d.s, but if you use white or blue the forward voltage is much higher.

Remember that the series resistor is required because the l.e.d. has little forward resistance. Virtually all other output devices such as buzzers, bulbs, motors etc., have their own resistance and do not require a series resistor.

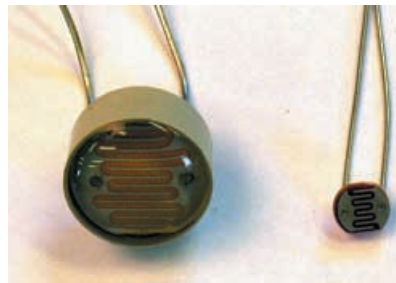


Photo 1.14. Examples of l.e.d.s, left a “standard” type, e.g. ORP12, and right a more responsive miniature version.

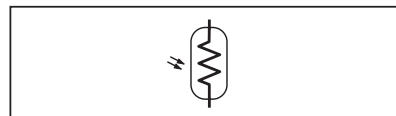


Fig.1.17. Symbol for an l.d.r.

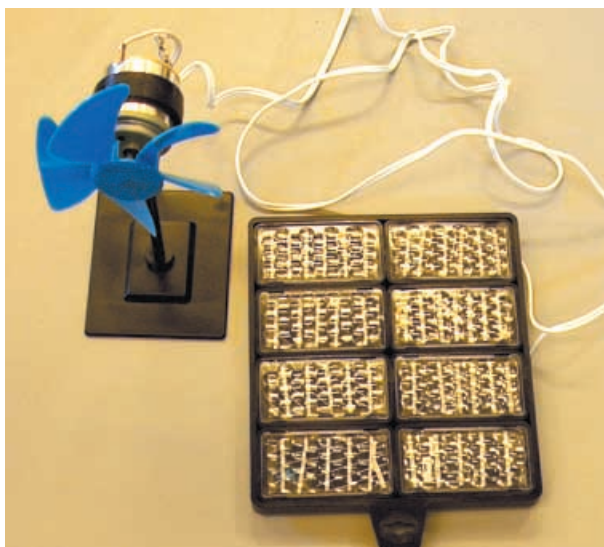


Photo 1.15 (above). A set of solar cells capable of powering a small fan.

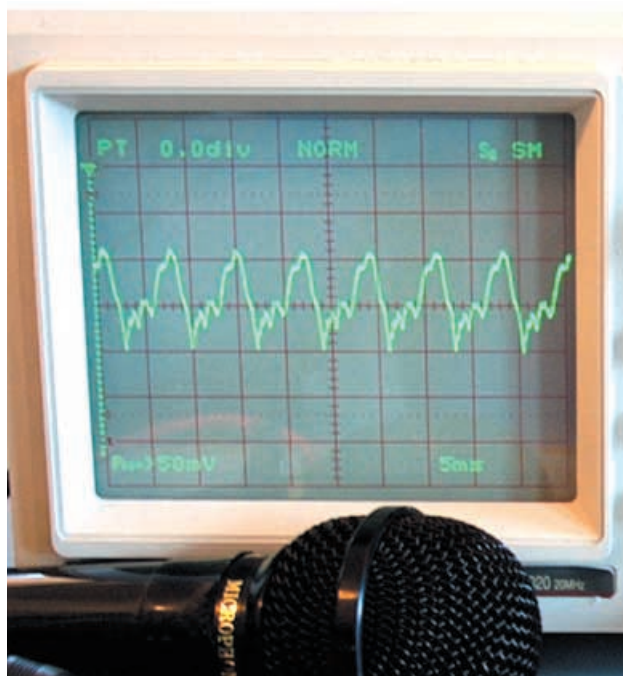


Photo 1.18 (right). Oscilloscope display of the signal output from a dynamic microphone.

INPUT DEVICES

Input devices are often referred to as transducers or sensors. The flow of current through the transducer depends upon an external influence such as light or temperature. Some transducers are passive, i.e. they do not generate electricity; others are active, i.e. they *do* generate electricity. We will examine the most common examples.

Light dependent resistor (passive)

A light dependent resistor (l.d.r.) is simply a variable resistor whose resistance changes according to the light intensity hitting its surface. Its resistance changes from about 200 ohms in bright sunlight, to over 1M ohms in total darkness. A "standard" l.d.r. is shown in Photo 1.14, together with a miniature type that is more responsive and cheaper. The schematic symbol is shown in Fig.1.17.

You can watch the resistance of an l.d.r. change if you connect it to a multimeter set to ohms (or k-ohms or M-ohms).

Note that an l.d.r. reacts quite slowly to a change of light; for example, it may take several seconds to fully change to its new value. This is of no consequence in automatic dusk triggered projects, since daylight changes very slowly anyway, but it can be a problem in some circuits, and so faster devices such as photo-diodes or photo-transistors should be considered.

Solar cell (active)

A solar cell generates electricity when exposed to light. Its cost makes it less suitable as a sensor, but if you require power in remote locations a solar cell may provide an answer. The set of cells shown in Photo 1.15 generate enough electricity to power a very small motor when exposed to strong direct sunlight.

Thermistor (passive)

A thermistor is a variable resistor whose resistance changes according to its temperature. The "-t" notation shown in Fig.1.18,

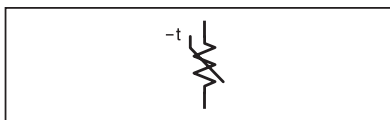


Fig.1.18. Symbol for an n.t.c. thermistor.

indicates a negative temperature coefficient (n.t.c.). In other words, as the temperature rises the resistance of the thermistor falls. The opposite is a positive temperature coefficient (p.t.c.) type.

Thermistors are generally given a resistance rating according to their resistance at about 25°C.

Try connecting a 5kΩ thermistor (n.t.c.) to a multimeter set to a range of 20k ohms. When you touch the thermistor, the warmth of your fingers will make its resistance fall a little.

When choosing a temperature sensor, also consider the range of "integrated circuit sensors" (i.e. complete circuits inside the sensor package) now available, which provide an exact voltage change per degree Celsius. These make accurate calibration of your circuit very easy.

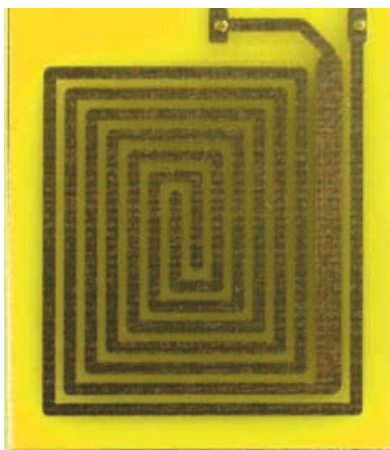


Photo 1.16. P.C.B. tracking used as a moisture sensor.



Photo 1.17. Commercial moisture sensor.

Moisture sensor (passive)

A pair of bare wires, or the tracks of a piece of stripboard or p.c.b. can be used as an adequate moisture sensor. The p.c.b. shown in Photo 1.16 has a sensor made of two tracks close together but not touching each other. When you breathe on the sensor the moisture in your breath causes the resistance between the tracks to fall from over 10MΩ to less than 100kΩ. In a later part we will look at a transistor circuit that will cause a warning buzzer to sound with your breathe on a moisture sensor.

A more professional moisture sensor is shown Photo 1.17. It works the opposite way in that moisture causes the resistance between the wires to increase. This is useful in applications where the sensor is normally wet, since less current is wasted.

Microphone (dynamic = active; electret = passive)

A dynamic microphone senses sound energy, and converts it into electrical energy. You can connect a high-impedance headphone to a microphone and receive sound without a battery or power unit.

The signal from a microphone is very small, and so an amplifier is generally required to boost the signal to an acceptable level. It is possible to connect a dynamic microphone directly to an oscilloscope to display your voice as shown in Photo 1.18.



Photo 1.19. Electret microphone handset.

PANEL 1.3. OSCILLOSCOPE DISPLAYS

Throughout this series we use oscilloscope photographs to display the signals at the input and/or output of a circuit. An oscilloscope can show what is happening when a voltage is quickly rising or falling; it shows the voltage by means of a graph or trace on a screen. Some of the images used in this series are displayed on a "dual beam storage oscilloscope".

A dual beam oscilloscope has two channels, one for each trace. This allows you to compare waveforms. For example, you may wish to check that an amplifier does not distort your sound signal, and so

you could display the output signal below the input signal and check that their shapes are identical.

However, a cheaper single beam oscilloscope is almost as useful. The reason that the author used a storage oscilloscope is that photography was made much easier! Some of our displays are also produced by a computer simulation.

A digital multimeter is a much cheaper alternative to any oscilloscope and will cover many of the experiments in this series.

If an oscilloscope is not available, you can use a multimeter set to "a.c. voltage". This will provide a guide to the signal level being generated.

An electret microphone requires a power supply, and the microphone module houses a tiny amplifier. The microphone in Photo 1.19 contains a battery that supplies power to the amplifier module. Hence a signal is produced which is similar to the effect of using a dynamic microphone.

Expensive electret microphones do not contain a battery and so require "phantom power". This is (generally) a 48V supply that is fed down the microphone cable from the main microphone mixer/amplifier.

Dynamic microphones can be bought for as little as £5, though good quality dynamics costing around £100 are often used in stage shows. Electret microphones are often used in professional recording studios. They should be placed above the faces of the performers so that air is not puffed into the microphone, to avoid popping noises.

Microphone Inserts

Dynamic and electret microphones are available as inserts, i.e. the microphone module without the housing. The one

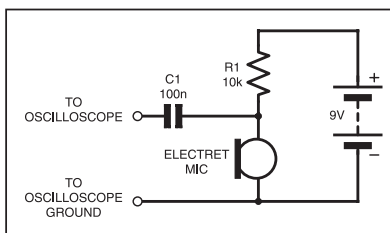


Fig.1.19. Experimental electret microphone circuit.

shown in Photo 1.20 is an electret type, available for about 50p and ideal for project work.

Try setting up the circuit in Fig.1.19 on a breadboard. Notice that resistor R1 is required in series with the microphone and the power supply. The signal from the microphone is normally connected to an amplifier circuit via a capacitor, C1. This blocks the d.c. supply, so leaving just the a.c. sound signal. The value of the capacitor is not critical and any value above 100nF should work.

If you use an electrolytic type then its positive connection should be nearer the

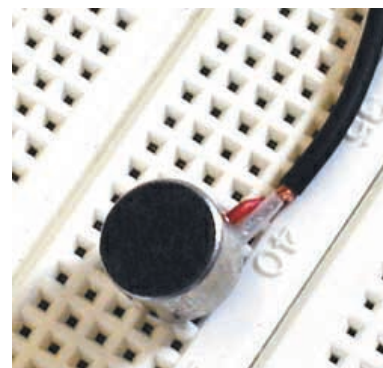


Photo 1.20. Electret microphone insert.

resistor. If you monitor the a.c. signal on an oscilloscope, you may also find that a "load resistor" is necessary – say 100kΩ – connected between the oscilloscope side of C1 and ground (0V). (Note that you can omit the capacitor and set the oscilloscope to "a.c. input".)

When you speak into the microphone you should see your voice on the oscilloscope screen, in the same way as illustrated in Photo 1.18.

OUTPUT DEVICES

Output devices are best dealt with as their need arises, and we will examine many during this series. They include:

lamps, i.e.d.s, heaters, bells, buzzers, speakers, electromagnets, solenoids, relays and motors.

Many output devices require a significant current and you generally need to amplify the current available from a sensor before an output device will respond adequately.

NEXT MONTH

Next month we will show how simple transistor circuits can provide the appropriate current and voltage for an output device.

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New Technology Update

A new Floating Gate Analogue (FGA) technology is claimed to be setting the standards for accurate voltage references, reports Ian Poole.

DEVELOPMENT of new chips to fill the ever-growing need for voltage references is always ongoing. In one advance, Xicor, an analogue and mixed signal i.c. manufacturer, has developed a novel technology that eliminates the need for laser trimming often used in the production of precision devices to enable them to meet their final required output voltage.

It is known as Floating Gate Analogue (FGA) technology and is an extension of the thick oxide Fowler-Nordheim Tunnelling technology that the company owns. This allows devices to retain a precision charge level on a floating gate within the device.

The company states that the advantages of the new technology enable the voltage reference to outperform other existing analogue technologies. By storing the voltage on the floating gate it is possible to produce a reference voltage that provides a very high level of initial accuracy, temperature stability and long term stability

Basic Circuit

The basic circuit contained within the new voltage reference is quite standard, although the way in which the reference is derived and maintained is totally new. The circuit shown in Fig.1 uses two MOSFETs, TR1 and TR2, one employed as a current sink and the other as a current mirror. TR1 is a depletion mode device that is self-biased by the current from TR2. A two transistor current source, TR3 and TR4, also supplies a voltage to the gate of TR2 enabling it to conduct sufficiently to stabilise its gate drain voltage at its threshold.

As the source connections of TR1 and TR2 are connected together the voltage at gate/drain of TR2 is the sum of the two threshold voltages. The unadjusted voltage output is therefore dependent upon threshold implants and can vary by around $\pm 15\%$.

Enhanced Circuit

To achieve the required performance, Xicor have taken the basic CMOS design and by replacing the usual depletion mode MOSFET with a floating gate version, they have enabled the output voltage to be trimmed to the required value. The circuit also exhibits far greater levels of temperature stability and long term

accuracy as a result of the new internal reference source.

The floating gate has an associated capacitance, C1. This stores the charge required to control the gate of the reference amplifier to produce the required output voltage.

The level of charge needs to be adjusted to enable control of the output voltage to be effected. This is achieved using tunnel diodes. There is an isolating area of oxide either side of the gate that forms the tunnel diodes. This requires around ten volts before the tunnelling mechanism allows conduction.

charge is effectively trapped on the floating gate and there is little change. Xicor state that the output voltage will remain intact for between 10 and 100 years.

Internal Feedback

An internal feedback loop is also included in the design and this contains an operational amplifier that is activated during the voltage programming function. By using this approach the device is programmed such that the output accurately reflects the external reference voltage. Once the calibration is complete the operational amplifier is switched off to save power.

Although the calibration circuitry could have been left off the circuit and external reference circuitry used for calibration, it was decided to retain these components on the chip for the possible future developments of a programmable version of the chip.

Slew Rate

The first of the devices to be launched has a very low power consumption. The device is able to provide its specified precision output with a power consumption of only 500nA. However, this also means that its transient response is not as good as devices consuming more power.

Applying a capacitor to the output makes a very large improvement, but where transient response is of particular importance, future devices that consume more power will be available with greatly improved performance. It is purely a matter of choosing what is required.

Using the new technology accuracies of around 250 microvolts and temperature coefficients as low as 1ppm/ $^{\circ}\text{C}$ can be achieved. As the device consumes a very low level of current it is ideal for many of today's portable applications where current drain is of great importance.

First Offerings

Engineering samples of the X60008 became available during the early part of this year, and production volumes are just becoming available. Future devices in the family are also being developed and made ready for production.

More information about radio and electronics technology can be found at www.radio-electronics.com.

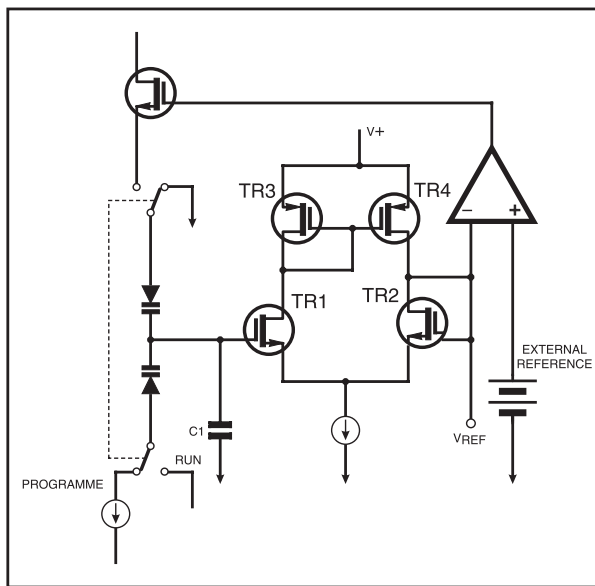


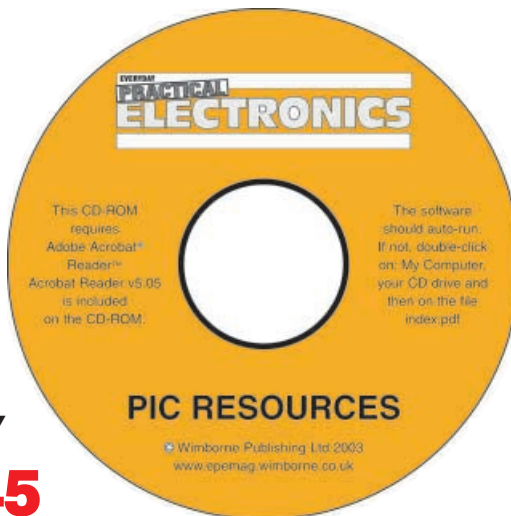
Fig.1. Xicor voltage reference circuit.

In Full Control

To allow full control of the gate charge voltage a current sink pulls charge out of the capacitor, whilst a variable voltage source feeds current in. By controlling the voltage source, it is possible to have complete control over the charge and hence the voltage on the gate capacitor, and the final output.

When the output voltage is set to the required value, the switches either side of the two tunnelling diodes are changed to completely isolate the diodes and the charge capacitor. Although it may appear that there may be some leakage of the charge on the capacitor and a resulting movement of the output voltage, the

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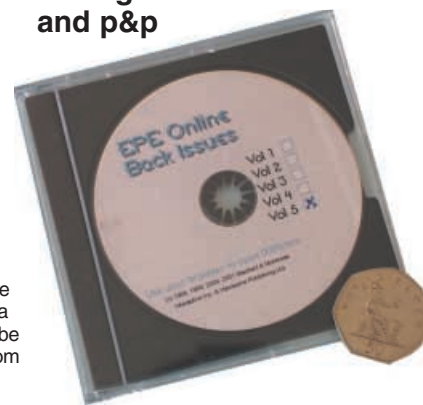
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ANYONE AT HOME?

OWEN BISHOP

Logically deter those shifty characters eyeing up your house!



THIS is a device to switch a mains-powered lamp on and off in a random way, to give a prospective intruder the impression that a house or room is occupied. Other lamps in the same room are switched on permanently, so that the house is never in darkness, but the frequent switching on and off of the controlled lamp will suggest that someone is there.

Constructors please note that part of this project is connected to the domestic MAINS supply and extreme caution must be exercised when building and running this project.

SHIFTY LOGIC

The circuit is driven by a pseudo-random generator, based on an 8-bit shift register. Shift register outputs Q6 and Q7 are connected to a dual-input Exclusive-OR (XOR) gate, whose output is then fed back to the shift register's input. The output from the XOR gate is a long but repeating train of logic pulses.

Table 1 shows the principle in relation to the sequence generated by a 4-bit shift register, feeding back the XOR of its outputs Q3 and Q4. Remember that the logic of a dual-input XOR gate is that if both inputs have the same logic level on them the output is logic 0, whereas if the inputs are at opposite logic levels then the output is logic 1.

If this table is continued the register contents will eventually become 0010 again and then the sequence repeats. If you work it out correctly, you will find that the process takes 15 clock cycles.

The registers show all possible combinations of logic 0 and logic 1, except for

Table 1. Example 4-bit shift register sequence

Clock	Q1	Q2	Q3	Q4	XOR Q3/Q4
1	0	0	1	0	1
2	1	0	0	1	1
3	1	1	0	0	0
4	0	1	1	0	1

0000. Obviously this cannot be allowed to occur for it would result in the circuit being latched to produce an infinite series of zeroes.

However, this does not happen with a 4-bit register feeding back from registers 2 and 3 as in the Table. It *could* happen with the 8-bit shift register used in this project if at switch-on the register is randomly reset to all zeroes, although this is rare. If it does happen, switching off and on again should change the situation.

With the project circuit there are 127 states before the sequence repeats. Although the sequence is obviously not random, it is so long that it is almost impossible to detect the repeating pattern. It thus *appears* to be random, and for the purpose of deceiving an intruder, only the appearance matters.

If one clock cycle takes one minute, the sequence takes 127 minutes to repeat, which is over two hours. A prospective intruder is not likely to wait for two hours and so notice the repetition.

The generator may often produce runs of two, three or more logic 0s or logic 1s, so the lamp may be on or off for periods of as many minutes. You may feel that such frequent switching is not realistic, and may prefer to run the clock more slowly. In this case, increase the value of capacitor C1 to 220µF or more.

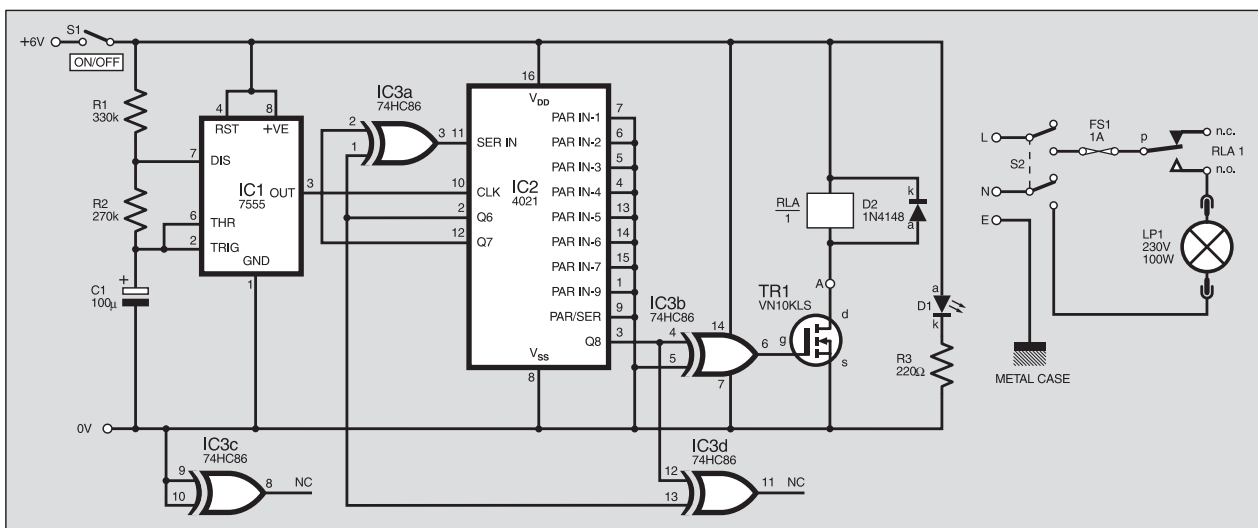


Fig.1. Full circuit diagram for the Anyone At Home?

CIRCUIT DESCRIPTION

The complete circuit diagram for the Anyone at Home? project is shown in Fig.1. The clock generator is based on a CMOS 7555 timer, IC1. Its output cycle rate at pin 3 is set by the values of resistors R1 and R2, and capacitor C1. The rate is approximately one cycle per minute.

Negative-going output changes at pin 3 trigger the 8-stage shift register IC2, which shifts via its pin 11 the logic level from XOR gate IC3a pin 3. Simultaneously, all internal logic levels are shifted along by one stage. Outputs Q6 and Q7 are fed to the inputs of IC3a, whose output logic level changes as appropriate to their logic.

The final stage at Q8 is fed to one input of IC3b, with its other input held at 0V. This XOR gate simply acts as a non-inverting buffer. The other two gates (IC3c and IC3d) within the quad package are unused, their inputs being tied to the most convenient circuit points to prevent them from "floating".

The output from IC3b pin 6 controls MOSFET transistor TR1. When pin 6 is high, TR1 is turned on, activating relay RLA and so connecting lamp LP1 to the a.c. mains supply via fuse FS1 and switch S2 (if switched on). The specified relay can switch a mains-powered lamp rated at up to 200W.

To economise in cost, the logic circuits are powered by a battery, instead of a transformer/rectifier circuit. In the prototype four D-type cells in a battery box were used (supplying approximately 6V d.c.), but if the circuit is to be used only occasionally, it will run for many hours on C-type or even AA-type cells. A lot depends on the resis-

tance of the relay coil, so select one with high resistance (while still being rated for 6V d.c. across its coil).

CONSTRUCTION

This project is connected to the mains and should only be constructed by those who are suitably experienced or supervised.

There are two printed circuit boards for this design, the Logic and Relay boards. These boards are available as a pair from the EPE PCB Service, codes 421 (Logic) and 422 (Relay).

Component layout, assembly and track details for the boards are shown in Fig.2 and Fig.3, respectively. Assemble the boards in ascending order of component

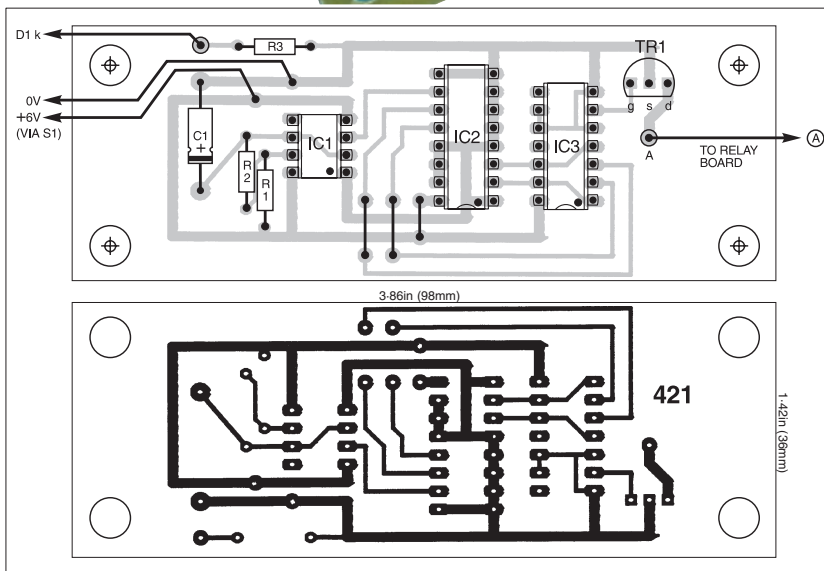
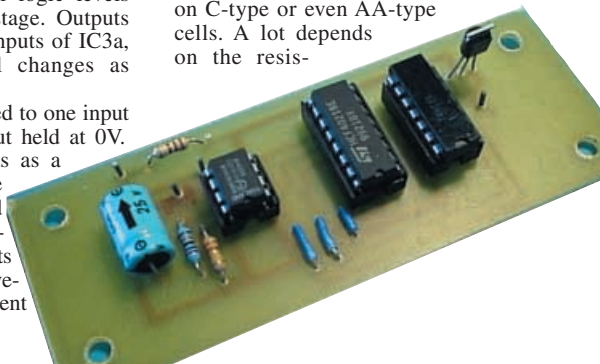


Fig.2. Logic p.c.b. component layout and full-size copper foil master.

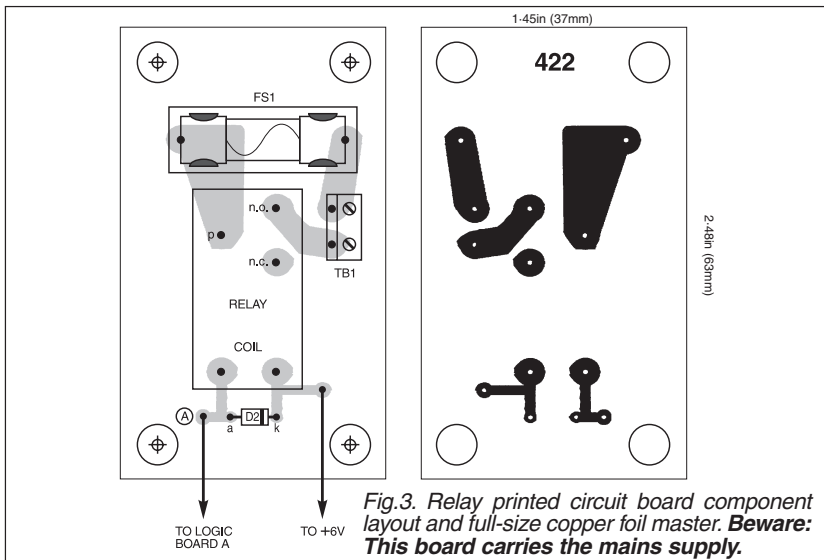


Fig.3. Relay printed circuit board component layout and full-size copper foil master. **Beware: This board carries the mains supply.**

COMPONENTS

Resistors

R1	330k
R2	270k
R3	220Ω

All 0.25W 5% carbon film or better

See
SHOP
TALK
page

Capacitor

C1	100μ axial elect. 25V
----	-----------------------

Semiconductors

D1	red l.e.d., panel mounting
D2	1N4148 signal diode
IC1	7555 low-power CMOS timer
IC2	4021 CMOS 8-stage shift register
IC3	74HC86 quad XOR gate
TR1	VN10KLS low-power n-channel MOSFET, or similar

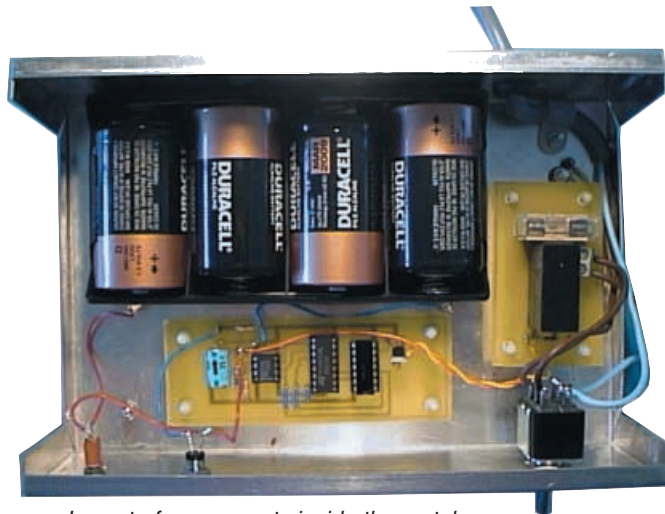
Miscellaneous

RLA1	relay 6V d.c. coil, s.p.d.t. contacts, 3A, 230V a.c., p.c.b. mounting.
S1	s.p.s.t. min. toggle switch, panel mounting, low voltage
S2	d.p.d.t. toggle switch, mains rated
FS1	1A fuse plus fuseholder, p.c.b. mounting type

Printed circuit boards, available as a pair from the EPE PCB Service, codes 421 (logic), 422 (relay); metal case (205mm x 128mm x 65mm); 8-pin d.i.l. socket; 14-pin d.i.l. socket; 16-pin d.i.l. socket; 6V battery holder for four D-type cells; battery clip to suit; plastic p.c.b. spacers, screw-fix, 6.3mm (8 off); solder tag; nylon cable clamp, locking; nuts, bolts and washers for tag, cable clamp and mains socket; stick-on rubber feet (4 off); grommets, 7mm internal hole (2 off); 3-pin mains socket, surface mounting; mains plug; 1mm terminal pins (4 off); single-core insulated connecting wire; stranded light-duty connecting wire; 3-core mains cable (length as required); solder, etc.

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Layout of components inside the metal case. It is essential that the metal case is securely "earthed" by the mains lead, using a solder tag bolted to the case bottom.

As said earlier, it may happen that when switched on all register bits contain zero, the register producing a continuous low output. If this occurs, simply switch off, wait a second or two and then switch on again.

Connect the two boards and test the relay operation, using a multi-meter set on the Ohms range to check the continuity across the relay's contacts (accessible via terminal block TB1) as they open and close.

If all is working correctly, replace the temporary $10\mu\text{F}$ capacitor C1 with the specified value of $100\mu\text{F}$.

ENCLOSURE

The case for this design *must* be all metal and firmly grounded to the Earth line of the a.c. mains, using a solder tag bolted to the floor of the case. The circuit boards have been designed so as to keep the low-voltage logic circuits well away from the relay and its mains connections.

For extra safety the mains switch is a double-pole toggle switch, controlling both the live and neutral lines, and rated at 10A.

It is not expected that the relay contacts will carry such heavy currents and the fuse is rated at 1A. This allows a filament lamp or lamps of up to 200W to be controlled by this project.

Drill the case to accept i.e.d. D1, switches, external mains cables, battery box and the mounting of the a.c. mains socket.

INTERWIRING

The interwiring between the two circuit boards and case-mounted components is shown in Fig.4. Make sure you use suitably rated wires between the mains switch, the relay terminal block and to the lid-mounted mains socket.

Wire in the mains supply to the enclosure, via a cable-clamping grommet. There must also be a grommet in the lid where the mains cable passes out to the lid-mounted mains output socket. Mount the circuit boards on well-secured spacers. Solder the other low voltage and mains voltage connections.

It is important that the connecting tags of the mains On/Off switch should be covered over with insulating sleeving, to protect against any possibility of touching the mains supply on them. The sleeving can be slipped over the wires before soldering them in position. The sleeves can then be pushed in place over the soldered joints.

Double-check all the wiring. Install the batteries into their box and insert a 1A fuse in the fuseholder. Place the lid on the enclosure and bolt it securely in place. Fit a plug to the mains lead.

Only after the lid has been secured in place should a mains test be carried out.

For the testing, plug a table-lamp into the mains socket on the lid. Plug the project into the mains. Switch on both power switches (d.c. and a.c. power). In a minute or so the table lamp should come on. If nothing happens (register contains all zeroes as discussed earlier) when five minutes have passed, switch the low-power switch off, then on. ☐

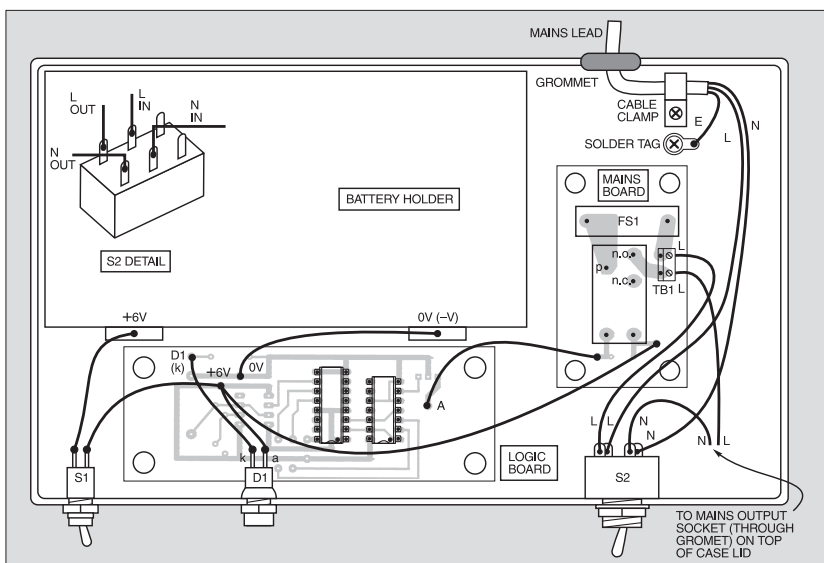


Fig.4. Details of the interwiring from the two circuit boards to the battery pack and off-board components. Wiring to the mains switch is shown inset.

size, observing the correct orientation of the semiconductors and electrolytic capacitor. Do not insert the i.c.s, or apply power until you have thoroughly checked the accuracy of your assembly and soldering.

BOARD TESTING

Test the logic circuit by monitoring the output of IC1. It should change state (alternating between high and low) twice every

minute. Also monitor the voltage at the gate (g) terminal of TR1. This should change state periodically between high and low, but the rate of change will depend on the logic levels within the register, and so not be predictable.

To speed the checking operation you could temporarily use a $10\mu\text{F}$ electrolytic capacitor for C1. This gives a faster clocking rate than the specified $100\mu\text{F}$.



Components mounted on the Relay board.



READOUT

Email: john.becker@wimborne.co.uk

John Becker addresses some of the general points readers have raised. Have you anything interesting to say? Drop us a line!

All letters quoted here have previously been replied to directly.

WIN AN ATLAS LCR ANALYSER WORTH £79

An Atlas LCR Passive Component Analyser, kindly donated by Peak Electronic Design Ltd., will be awarded to the author of the *Letter Of The Month* each month.

The Atlas LCR automatically measures inductance from 1 μ H to 10H, capacitance from 1pF to 10,000 μ F and resistance from 1 Ω to 2M Ω with a basic accuracy of 1%.



★ LETTER OF THE MONTH ★

CLEAR GOGGLES

I have discovered an improved means of preventing misting inside safety goggles. A PTFE spray is sold by Screwfix Direct (telephone 0500 414141) part no. D15152 (currently £3.10). A quick burst is applied to the inside lens of the goggles and wiped round with a soft tissue until the solvent dries to leave an undetectable film. Even in the hot weather goggles resist misting for much longer than without the PTFE treatment.

The spray did not harm the plastic materials of my goggles, but should first be tried on an unimportant area just in case. Although PTFE is extremely inert at room (or even body) temperatures, it would seem sensible not to adopt my suggestion in the unlikely case of someone with a known sensitivity or allergy to this spray.

The same supplier sells likely-looking solder safety goggles, part no. 12907 ("overspecs", currently £1.89) and for more adventurous work a brow guard, part no. 16142 (currently £7.59) offers full-face protection while allowing air-

flow and thus also helping to prevent misting.

No, I've no connection with this company (other than the fact that we enthusiasts shouldn't be without their latest, free, catalogue) but please note that small orders attract a delivery charge on top of the above-quoted (VAT inclusive) prices.

By chance, I have also discovered yet another means of preventing goggle misting and it might do for both terrestrial eye protection and also for use in scuba diving (where misting can be a problem). Speedo produce "lens cleaner anti-fog solution" which comes in 60ml spray canisters, about £5 from sports shops.

Godfrey Manning, G4GLM, Edware, Middx

Although there are "traditional" ("loutish"?) ways of keeping scuba and snorkeling masks and goggles free of condensation, they are not to be recommended for workshop goggles! Thank you Godfrey, and for the interesting private chats we've had on the subject!

CLOUD COVER

Dear EPE,

Congratulations John on yet another masterpiece – your *PIC Met Office* (Aug/Sep '03). I wondered whether you had considered a cloud cover (or sunshine) monitor. Pointing a light sensitive resistor and an infra-red detector diode to the north (northern hemisphere) provides a good indication of cloud cover. High IR indicating sunlight and low IR day/night/general illumination.

Mike Halliday, via email

Thanks for your kind Met words Mike. But, no – dash it all (he exclaims in polite English)! – I didn't think of cloud cover, though daylight monitoring is included. Perhaps clouds for a Mk4? (the current being Mk3, over some 16 years or so). UV sensing I would have also liked to have included but I could not find any low cost sensors – does anyone know of a source?

PIC BREAKPOINT

Dear EPE,

I have found that the *PIC Breakpoint* (Oct '03) software won't work with a PIC16C84. I suspect this is because the "Include" file tries to use data locations 48 to 4F as indicated in the article on page 718. These locations don't exist in the C84 but there's a work around that may work for small programs – change the line **LIST p = PIC16C84, r = dec to LIST p = PIC16F83, r = dec** and then calibrate using an F84.

Although the differences between the i.c.s may introduce other problems, it works for the demo prog.

Roger Warrington, via email

Thank you Roger. No attempt was made to suit Breakpoint for use with a C84 as this is an obsolete device. It's recognised that readers may still have stock of them, but neither I nor Richard Hinckley, Breakpoint's designer, can offer help on any problems that may arise with the C84.

AVR MIGRATION

Dear EPE,

Regarding your August 2003 *Readout* and the suggestion that *EPE* should come up with a toolkit for both programming and development for Atmel AVR microcontrollers. A few years ago I was given an AVR kit whereby you can program chips on a motherboard which plugs into the serial port of your computer.

My knowledge in electronics is growing steadily. I am currently doing an ICS City and Guilds electronic course and over the last few years have been taught bits and bobs by an uncle who served his time in the RAF working on computers and such like.

I feel I'm ready for the next step – programming and using microcontrollers. I've got a hunger for electronics, can you help feed that enthusiasm?

Bob Norman, via email

Thanks for your comments Bob. Despite me recently raising AVRs in Readout you are only the 3rd person to respond, so I guess the majority still are not interested, meaning that we would not feel justified in pursuing them. Which I guess will be a disappointment to you, sorry! But PIC microcontrollers are easy to learn and use, so I recommend that you take that route instead.

Keep on enjoying electronics (and us)!

WITH HONOURS!

Dear EPE,

Thank you for your "well-wishes" in *Readout* July '03. I did indeed pass with Honours – a 2:1 Honours degree in fact. My electronics future looks bright!

Jonathan Grainger, via email

That's great Jonathan – congrats and all best for your future career!

DON'T BLAME BT

Dear EPE,

I feel you were unfair to British Telecom in your *Net Work* article of September 2003. The column used a disparaging and critical tone throughout, and your article seemed more like an irrational rant rather than a reasoned argument. That isn't good journalism, surely?

You are absolutely right that BT's business model is "hard-nosed" and quite rightly so. After all, BT is responsible to its shareholders for making a profit. In my view, the "needs of the nation" are as irrelevant to BT as they are to you. BT has not been a nationalised company for years!

In comparison, numerous rural villages in England have no gas supply. Do the villagers argue that the gas company is morally obliged to provide it because it would be of benefit to their community? No! They put up with it and make do with the alternatives, or they find the several tens of thousands of pounds the gas company charges to install a gas pipeline.

Why should BT provide ANY of its services at a loss? There would be only one reason to do so: if Ofcom made it a requirement in BT's licence. It does just this with its public payphone service, for instance. If BT installed ADSL equipment at exchanges where there is insufficient demand to pay for it, it would then be – in effect – cross-subsidising its own ISP division and it would doubtless be skating on very thin ice with the regulator.

Remember – no-one has the *right* to get a gas supply, and no-one has the *right* to a broadband connection. (Did you know that no-one has the *right* to a dial-up connection, even?)

Ah, I've enjoyed this rant! No hard feelings intended, just a vigorous difference of opinion!

(name and email address supplied.)

Alan Winstanley, author of Net Work, replies:

I do strive to offer a professional and balanced view on topical subjects, my recent analysis of Paypal being one example. Although it would not come across in the September column, I am not unrealistic or unsympathetic about the technical issues that face BT and cable companies. Besides, even if a local exchange has been upgraded for ADSL, if you are too far away or the line quality is too poor, then ADSL still cannot be used anyway.

However, I was really speaking up for all those frustrated users who are never likely to receive ADSL and who are therefore dependent on other more expensive broadband technologies being delivered some time in the future. What I think we are seeing is a land-grab for ADSL customers while the needs of the rest of us are being overlooked. It is only customer pressure that gave us, for example, the flat-rate Internet access that many of us enjoy today. Broadband is beyond reach of many users who could benefit the most from it, and even those without a gas supply have a choice of alternative "always on" energy sources. I do feel it is time that the focus switched to the plight of those who require high speed Internet access in areas where ADSL will never be available.

I recently attended a broadband launch where BT enabled ADSL in 18 exchanges at its own cost, and nearly £1.5 million of public money has also been made available for subsidising the delivery of broadband to 1,800 businesses. So they can do it when they want!

Alan Winstanley, EPE On-Line Editor

STORE WARS

The following thread from EPE contributor and reader Aubrey Scoon recently appeared on our Chat Zone, and deserves repeating here:

It's getting increasingly hard to find any electronics mags in WH Smiths, but often they do have them, but for some inexplicable reason, tend to hide them!

A few months ago I was in a Smith's (I forget which town) looking for EPE when suddenly I heard a commotion. A middle aged gentleman was complaining extremely loudly to a staff member that he couldn't find any electronics magazines. He was talking very loudly so everyone could hear but in a very educated and reasonably polite way. He was telling them that he believed there was a conspiracy amongst the staff to hide electronics magazines and was demanding an explanation. The staff were trying to reassure him that wasn't true, and even the manager was called.

EPE and EW were eventually located right at the back of the magazine stand, completely hidden between a magazine for showjumping and another for pig farming. When the gentleman complained that this was evidence that electronics was being deliberately hidden, the manager assured him this was not the case, and it was solely because electronics was not a popular subject.

Well, I couldn't resist it. I immediately waded in, loudly complaining that the manager was completely unjustified in making such a statement and that electronics was indeed very popular, and if anything, any fall in popularity was probably due to store managers hiding the magazines.

Between us, the gentleman and I were causing quite a fuss and we started to gather a large crowd of spectators. The manager kept trying to wriggle out of the situation but we were demanding an explanation. The best thing was that more

and more people started joining in on our side, complaining that they too could never find electronics magazines and demanding to know why the manager had such a prejudice against electronics hobbyists!

The poor manager, extremely embarrassed by all this attention, which by this time had brought virtually the whole store to a halt, eventually caved in and promised that the magazines would be placed in a prominent and consistent position in future, which raised a boisterous cheer from the assembled crowd.

Funny thing was, loads of people immediately snapped up the remaining copies, whereupon someone else started complaining that there were not enough copies to meet demand, leading to further concessions from the manager, who by that time clearly wished he'd stayed in bed that morning instead of going to work!

Anyway, the point is that it seems there are quite a few of us who suffer in silence and that it only takes a bit of consumer activism to bring out some support.

On that note, I strongly advise the proletariat to make their feelings known to WHS. I doubt if the store in question is still hiding the EPEs!

**Aubrey Scoon,
via the Chat Zone**

A splendid tale Aubrey! It's another very strong reason for taking out subs or buying online. Via the Chat Zone, On-Line Editor Alan commented to Aubrey:

To clear up any confusion, AFAIK from previous discussions with Ed., each WHS store has a particular "level" or rating which determines the range of titles it will stock. You only have to look at the vast array of frivolous titles all competing for shelf space to know that each branch can't stock every title.

However, WHS should still be able to order it for you and put it away in the "Call Fors", a

personal folder reserved for a customer. If this is not the case I would very much like to know, if only because I used to work for WHS in Brigg as a lad... and doing the Call Fors formed part of my crashting dull routine on a Saturday morning.

It's the same sort of thing in other retail sectors as well. My firm used to have to pay Halfords thousands in order to get our products included in their (compulsory) advertising, and profit was calculated per square inch of retail space.

It is getting more and more difficult for a manufacturer or publisher to get their product into the High Street.

Alan Winstanley, via the Chat Zone

FLOW CHARTS

Dear EPE,

I must comment on what Jon Rigter writes in *Readout* August '03. I started with flow charts before I did any formal training in computers, and found them easy to use. Then I studied for an MS in computer science. There I was told flowcharts are out, with the same sort of reasoning Jon espouses. I tried the "more modern" methods, both during course projects and "real" projects. I never bought them.

Eventually, I started to learn about PICs. I read various magazine articles, and found myself floundering with them. Then I bought *PICtutor*, and all became very clear! I reverted to flow charts, and never looked back. In disagreeing with Jon I think it might just be a case of not everyone thinks the same way. But I should say a former work colleague, a relatively recent bachelor graduate, and much younger than me(!), definitely preferred flow charts.

**John Waller, USA,
via email**

Thank you John. As I've said before, I just don't get on with them and prefer to jump straight in to the assembly code stage.

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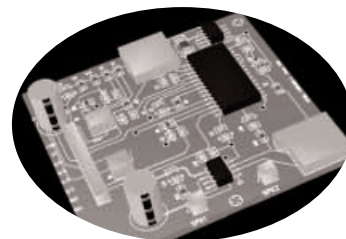
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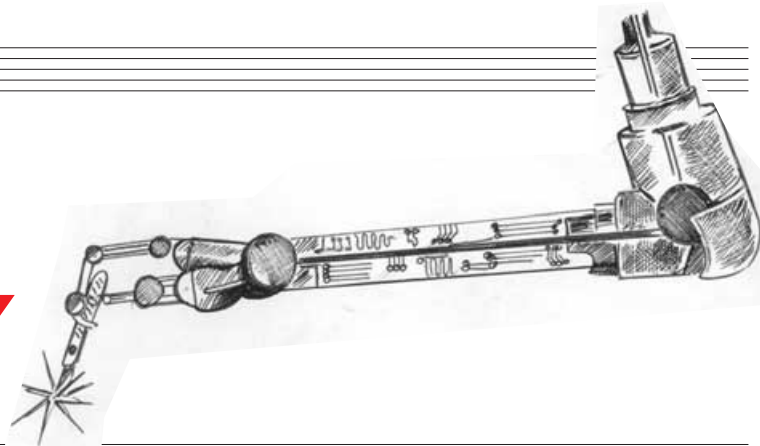
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CIRCUIT SURGERY

ALAN WINSTANLEY
and IAN BELL



Our surgeons offer advice on creating long delays with the 555, they give equipment cooling fans a whirl and introduce aspects of high-side current detection.

The Time is Nigh?

I want to use a 7555 CMOS version of the 555 timer in monostable mode. Is it possible to obtain long output periods? What is the maximum value of timing resistor that can be used in the timing component? Should I use a high-value resistor and small capacitor, or vice versa? Thanks from Ivy Li in the EPE Chat Zone message board (www.epemag.wimborne.co.uk).

In the mid 1980s the CMOS 7555 was introduced as a low power replacement for the universal bipolar 555, the world's most popular timer i.c. The CMOS type is usually a direct plug-in alternative, though it is worth remembering that there are differences in some areas – I resort to the bipolar 555 when I need higher output currents (say 100mA to 150mA), or some form of buffering, using say a MOSFET transistor, is useful at times.

However, the CMOS device tends not to cause spikes or "crowbar" the power supply when switching, and it has a much lower bias current (say 10 picoamps) than the bipolar type. A typical CMOS device is the Texas Instruments TLC555 and a data sheet can be downloaded by searching www.ti.com.

A Long Delay

In order to generate large delays of, say, an hour or more, then obviously a high RC time constant is needed. Larger resistors can be used up to a point, but the need for larger capacitors as well implies that electrolytics must be used.

These can have a terrible leakage current characteristic, which affects the accuracy of the timer. I try to utilise tantalum bead types for longer delay periods. The CMOS version of the timer provides for higher resistance values, meaning smaller capacitors can be used.

The monostable time period is defined by $t = 1.1 RC$ (t in seconds, R in ohms, C in farads). A high resistor coupled to a "leaky" timing capacitor will introduce serious timing errors because the charge leaks away to 0V, so the best approach is to use as large a resistance and as small a capacitance as possible.

In the past, some practical experiments produced reasonably consistent delays (>30 minutes) using say 100 μ F to 220 μ F maximum with up to 10M resistance or more. There seems to be no published figures for maximum RC values, because results would be highly variable between different RC components, especially due to the timing capacitor leakage and stability.

The main difficulty of using high RC combinations is the reproducibility of timing results. You can select values empirically in individual projects, but to create accurate, repeatable lengthy delays, a better technique is to use a digital method instead.

It is much better to use a 555 timer in astable mode to create a reasonably accurate clock signal, or quartz controlled oscillators can be built for higher accuracy. This clock can drive a digital counter circuit that can trigger after a preset number of pulses have been clocked; a variety of such circuits have appeared in *Ingenuity Unlimited* from time to time.

Some timer chips used these digital techniques including the interesting and long-lamented Ferranti ZN1034E that could time for up to a year! After scouring catalogues and the web, I could not find a readily-available long-range timer chip.

Today a microcontroller would be another way of generating accurate delays using a custom programmed chip. The Managing Director of Magenta Electronics Ltd. pointed out that a Microchip PIC microcontroller costs today only the same sort of price that a simple 555 cost in its heyday, which is a sign of what will probably happen in years to come. Is the end nigh for the 555? A.R.W.

Let's Talk Hot Air

When one decides to use forced air in cooling audio power amps, how does one go about choosing the efficiency of a cooling fan?

If you have a fan capable of "X" CFM (cubic feet per minute), is it more efficient to let it blow air over the

components i.e. heatsinks inside the equipment or let it remove the heat from inside the equipment? One is assuming the fan is operational from switch-on and does not operate on thermal conditions.

I have been a reader of your magazine for many years. The names may have changed, but the contents are as interesting as ever. Thanks from Bill McCleod, by email.

The fan actually does both things – it blows (well, sucks) air over the components and it exhausts the hot air as well! The efficiency depends a lot on the internal layout of the equipment and what there is in terms of heatsinks, power components and ventilation inside. I would say the most efficient way would be to blow air out the rear of the equipment, and suck it in from the front, having constructed a suitable path for the cold air to be passed over power components.

The formula I have for reference is taken from that best-known of electronics textbooks, *The Art of Electronics* (Horowitz and Hill):

air temp. rise ($^{\circ}$ C) = $1.6 \times \text{Power (W)} / \text{airflow (CFM)}$

so you can work out the likely acceptable temperature rise.



Internal view of a power supply that uses fan cooling to draw cooler air over a heatsink.

Rule of Thumb

The rule of thumb quoted is that a 100 CFM fan will adequately cool instruments running 100 watts or more. The fan efficiency also depends on the back pressure that the fan will experience and other physical factors. Many catalogues don't quote the volumetric airflow, but an 80mm fan may be good for say 20-30 CFM roughly.

You will usually need a heatsink to enable power components to dissipate heat at maximum power without overheating, and it may be better to mount that on the rear of the cabinet; it is hard to give blanket recommendations. If you have large internal heatsinks then a fan may be best on an enclosed case. The idea is also to control the airflow by forcing air to be sucked in from e.g. the front and vented out of the rear, passing over hot components in the process.

Personal computers make very good case studies of how to control airflow properly. They usually have intake slots at the front (especially around hard drives, which get extremely hot), and one or more fans mounted at the back to blow exhaust air through the rear grilles. The processor and graphics card may have its own extractor fan as well.

Internally, round cables rather than ribbon cables are preferable for allowing cool air to pass over hot, fast hard drives.

I was recently asked to fix a PC problem and discovered that whilst the fan blew dirt out of the rear, every ventilation hole was blocked and it had sucked dirt in from the front, eventually wrecking the CD-ROM and floppy drives by clogging them solidly as well. The use of an airduster aerosol at regular intervals is recommended to ensure efficiency is maintained, and to avoid more costly repairs later on. It is a simple task for any computer users to lift off the cover and dust out the vent holes with an aerosol. And you can now brighten up your projects using transparent fans that contain glowing i.e.d.s or cold cathode tubes! Glad to hear you enjoy the magazine. A.R.W.

Another Flavour of Spice

Following our item on PSpice (September and October 2003), we were very pleased to receive feedback from Cadence themselves:

I must congratulate you on the great mini-series on circuit design using the PSpice Student Download. As you know PSpice is a professional tool widely used throughout the electronics industry and last year won an Easit educational award.

You can find more information on PSpice and the OrCAD products on <http://orcad-pcb.com> and <http://orcad.com>. These websites contain a wealth of information as well as application papers and useful links to vendor model websites.

I would draw readers' attention to the article on the Hubble Space Telescope which uses PSpice to model and simulate the electrical power system for the telescope. Dennis Fitzpatrick, Lead Support Applications Engineer, Cadence Design Systems.

Many thanks for the additional web links. We were pleased to major on PSpice Student Download, which we consider to be an excellent all-round circuit simulator. Products such as this used to

cost professionals tens of thousands of pounds and could only run on a main-frame computer, and were totally beyond the reach of the amateur user. We applaud the availability of the PSpice Student Download which we hope will encourage newcomers to try creating circuits in this environment for themselves.

Some users may struggle with such a large download though, and reader **Nick de Smith** reminded us about LTspice (also known as SwitcherCAD III) from Linear Technology. This is optimised for op.amps and switched-mode power supplies, but it does a fine job with ordinary Spice simulation tasks. Cadence's PSpice undoubtedly offers a far greater range of overall capabilities and functionality however.

LT produced the simulator because many other Spice simulators struggled with switch-mode circuits due to the complexity of waveforms involved. LTspice is also more efficient at dealing with parasitic components, such as the resistance of an inductor, than some other Spice versions. Parasitics are particularly important in switch mode circuit design.

For many readers one advantage of LTspice in that download size is reasonably small for a CAD tool, at around 5MB. It is available in its full form from the Linear Technology web site, www.linear.com/software/. It comes with a set of models of LT devices, particularly op.amps (over 200 of them) and regulators, but other "standard" Spice models will work with it if you have them available. There are quite a few LT enthusiasts online in newsgroups, so you can find helpful discussions and information.

LTspice has an easy to use user interface and it is very straightforward to change something in a circuit and run the simulation again to see what difference it makes. LT's philosophy in designing the simulator was to allow a lot of flexibility; whilst providing sufficient warning messages if circuits are badly flawed.

The basic idea is very similar to using PSpice (and any other Spice software with schematic capture) so we will not describe step by step how to use LTspice. If you want to use it, read through last month's description with screenshots of using PSpice to get a general idea of what you should be doing, then have a look at the help file for LTspice and you should be able to work it out.

Circuit Problem

Our thanks to **R. D. Thompson** who wrote to us about a problem with a circuit that detects failure of a vehicle light bulb. The bulb in question uses a 12V supply and draws 2A. The sensor is required to indicate when the bulb fails to draw any current. Mr. Thompson suggests a solution of using a small value sense resistor in series with the bulb, choosing 0.1 ohms, which will drop about 200mV (leaving 11.8V for the bulb) and consume only a few milliwatts.

We agree that this is a viable approach, and we also agree with the reader's suggestion that an op.amp can be used to process the small voltage drop across the sense resistor. We need a single supply op.amp, as the op.amp should be powered from the 12V supply, again Mr. Thompson had spotted this requirement.

Our reader tried the circuit shown in Fig. 1. The idea is that the op.amp, which has a very high gain (around 100,000), should amplify the voltage difference across the sense resistor. Thus the output should be around 12V when the bulb draws current, and zero otherwise. Unfortunately the suggested circuit failed to work!

There are a number of possible problems. First, if the op.amp has a gain of 100dB or $\times 100,000$ then it only takes 120 microvolts across the sense resistor to switch the op.amp to positive saturation. It is not impossible that there would be leakage current or other noise of this magnitude present, particularly when the bulb is absent.

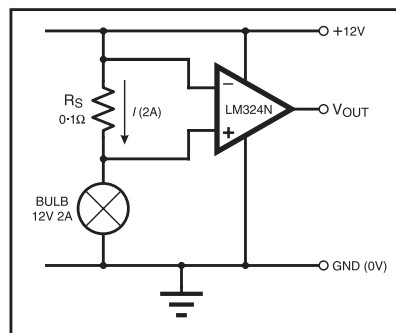


Fig.1. First circuit for a bulb failure monitor. As explained in the text, it may not work with the op.amp initially specified.

The op.amp gain is far higher than needed (200mV to 12V only requires a gain of 60). Opamps also have a widely varying open loop gain (the term used for an op.amp circuit when no feedback is applied), which makes it difficult to predict exactly what might happen with an individual device. Usually an op.amp amplifier uses **negative feedback** to set the gain of the circuit. This gain then depends mainly on the feedback components and not on the actual value of gain of the op.amp itself (which just has to be a very large value).

Potential open loop instability is not the only problem we face; a particular difficulty with this kind of circuit, which is known as a **high side current sensor**, is that the op.amp must have a **common mode input range** that includes the power supply. The common mode voltage is basically the average voltage at the two inputs. In effect what we have here is a $\pm 100\text{mV}$ square wave (for bulb OK/not OK) with a common mode signal of 11.9V.

Unfortunately the common mode input range specified on the LM324's datasheet (from National Semiconductor, available on line at www.national.com) only goes to 1.5V below the positive supply. This circuit exceeds that requirement and therefore the LM324 is very unlikely to function correctly (although no damage should occur).

So the basic conclusion is that we should use a differential amplifier with negative feedback around the op.amp, setting a maximum gain of 60, and we must select a device with a common mode input range that includes the positive supply voltage. We will continue with this circuit next month and will hopefully simulate it in Spice as well. I.M.B.

SHOP TALK

with David Barrington

PIC Random L.E.D. Flasher

The only criterion to be taken into account when shopping for components for the *PIC Random L.E.D. Flasher* project is size, particularly if you wish to wear it as a "festive or disco badge".

The 3mm blue, high intensity, diffused l.e.d. was purchased from **Rapid Electronics** (☎ 01206 851166 or www.rapidelectronics.co.uk), code 55-1460. Miniature 6mm square-shaped tactile switches should be fairly easy to locate and appear in most catalogues now. The one in the model also came from the above company (code 78-0605) and has an extended 5mm actuator (button). You may find that component suppliers only stock cermet type presets in the 6mm size specified. These are not too expensive and can, of course, be used in this circuit.

For those readers unable to program their own PICs, a ready-programmed PIC16F84 microcontroller can be purchased direct from the author for the sum of £6 (add £1 for overseas). Orders (mail only) should be sent to **Andy Flind, 22 Holway Hill, Taunton, Somerset, TA12HB**. Payments should be made out to **A. Flind**. The software is available on a 3.5in. PC-compatible disk (Disk 6) from the *EPE Editorial Office* for the sum of £3 each (UK), to cover admin costs (for overseas charges see page 803). It is also available for free download from the *EPE* ftp site, which is most easily accessed via the Downloads click-link option on the home page when you enter the main web site at www.epemag.wimborne.co.uk, then enter the **PIC Microcontroller source codes** folder and select **PIC Random Flasher**.

The small circular printed circuit board is available from the *EPE PCB Service*, code 424 (see page 803).

Practical Radio Circuits-7

Some readers may have problems finding the BF199 high frequency transistor called for in the *Direct Conversion Receiver*, this month's *Practical Radio Circuits* project. We understand that **Cricklewood Electronics** (☎ 0208 452 0161) have plenty in stock. The author indicates that most low power rectifier diodes can be pressed into service as a "varicap" diode for D1. Readers who prefer to use a true varicap could fit the BB105 from an earlier project in this series.

As previously, the Toko coils are available from **Sycom, Dept EPE, PO Box 148, Leatherhead, Surrey, KT33 9YW** (☎ 01372 372587 or www.sycomcomp.co.uk). They need to be ordered by quoting their type numbers as listed in the parts list and on the circuit diagrams.

The author says almost any polyvaricon (polythene dielectric) variable capacitor designed for a.m./f.m. portable radios will work in this circuit. They will normally be found listed as "transistor radio" types and consist of an antenna and oscillator section, plus trimmers. They are currently stocked by **ESR Components** (☎ 0191 251 4363 or www.esr.co.uk), code 896-110 and **Sherwood Electronics** (see page 808), code CT9. The one in the prototype was obtained from **Maplin** (☎ 0870 264 6000 or www.maplin.co.uk), code AB11M.

The two printed circuit boards are available from the *EPE PCB Service*, codes 423 (Direct Con. Rec.) and 406 (T/Cap - optional), see page 803.

Anyone At Home (Top Tenner)

Only two items used in the *Anyone At Home* project, this month's *Top Tenner* offering, could prove troublesome. The relay used in the prototype and shown in the photograph appears to be one with a low voltage d.c. coil and single-pole contacts rated at 10A 250V a.c. We do not have any source details for this particular relay, however, most components advertisers should be able to suggest a suitable one. It may mean "hard wiring" it to the p.c.b.

We have searched for the VN10KLS *n*-channel low power MOSFET device and, surprisingly, only **Sherwood Electronics** (see ad. on page 803) appear to carry it in their current listing, coded as the type number. No doubt other low power, general purpose *n*-channel MOSFETs will work in this simple circuit.

The two printed circuit boards are available as a pair from the *EPE PCB Service*, code 421 (Logic) and 422 (Relay), see page 803.

Cardboard Clock

We do not expect any buying problems to arise when putting together parts for the *Cardboard Clock* project. The hardware bits and pieces, such as the obeche and balsa wood, should be obtainable from most good model craft shops.

The 15mm diameter disc magnets were purchased from **Maplin** (☎ 0870 264 6000 or www.maplin.co.uk), code SF19V - two required. The 32s.w.g. (30a.w.g.) enamelled copper wire for the coil was obtained in a 50g (2oz) reel from **ESR Components** (☎ 0191 251 4363 or www.esr.co.uk).

Teach-In 2004

Apart from a couple of semiconductor devices and some "Miscellaneous" items in the new *Teach-In 2004* tutorial series Components Box, most components should be readily available from advertisers. The "difficult" parts will be dealt with as and when they appear throughout the series.

The microcontroller chips will be offered by the author ready-programmed when they appear in the published instalment.

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CARDBOARD CLOCK

MICHAEL McLOUGHLIN

An intriguing way in which you can watch time passing!

THIS article describes how you can build an accurate low-cost electro-mechanical clock, using the minimum of component parts and normal household tools.

The Cardboard Clock uses a simple battery-powered circuit to control a pendulum and thus turn three gear wheels which double as "time dials". There are just five moving parts, including the cardboard gear wheels. The clock keeps time to within 15 seconds a day.

A normal pendulum clock that is accurate when fully wound will lose time towards the end of the week as the spring runs down and the error can reach about 30 seconds per day.

COIL PARAMETERS

The author's intention was to build a pendulum clock with a magnetic drive. However, the conventional historic Kienzle circuit in Fig.1 was not felt to be suitable as it uses two coils of fine wire, with about 4500 turns altogether. Such a quantity and its required accuracy of winding, completely excludes amateur construction. In the design presented here, only one coil is used, having just 100 turns of 32s.w.g. wire, which is reasonably thick and easy to handle.

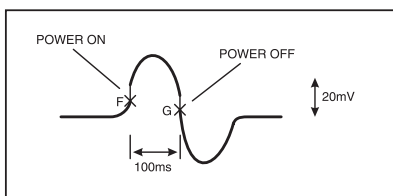


Fig.2. Trace of coil voltage as the magnet passes. It is roughly an induced sinusoid, with current/resistance jumps as the power switches on and off. Voltage measured at S in Fig.4.

Two disc magnets are used, each having a diameter of 15mm and thickness of 6mm, to form the bob of the pendulum. As the magnet passes over the coil, a voltage proportional to the rate of magnet movement is generated across the coil. The peak voltage is about 20mV and produced at intervals of 100 milliseconds, as illustrated in the waveform of Fig.2.

DRIVER CIRCUITS

As so small a voltage is needed, the circuit can be powered by a single 1.5V cell, but the 20mV induced voltage must be current-amplified to produce a 2mA pulse. The 1.5V supply, though, rules out the use of op.amps as an amplifier. They have a

ELECTRICAL TIME

In 1841 Alexander Bain took out the first patent for an electric clock. His pendulum worked a switch, which operated an electromagnet to pulse the pendulum. J. T. Gent of Leicester used the idea in his master clock, which could switch hundreds of slaves throughout a building.

In 1948 the transistor came along and the switch on the pendulum became replaced. The system was extended to drive balance wheels in watches. A circuit that was widely used is known as the Keinzle, Fig.1.

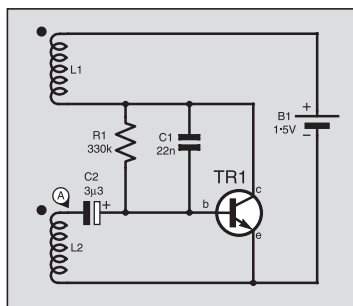
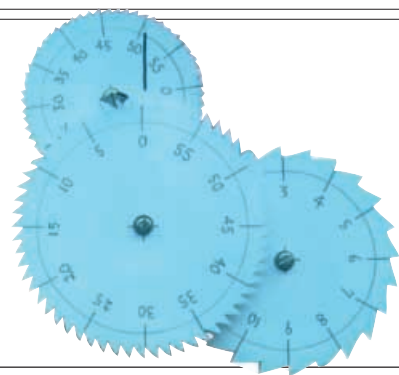


Fig.1. Kienzle clock circuit. The coils lie together, and the magnet travels past them.

Note the electrolytic capacitor, C2. For most of the cycle it charges gently, via resistor R1. On the balance wheel there is a magnet, and ten times a second it passes the coil assembly L2, inducing a voltage that raises point A upwards by about 500mV. This triggers transistor TR1 into conduction and the resulting magnetic field generated by inductor L1 gives the magnet a regenerative "push".



class B output stage which puts in series two base-emitter drops of 0.7V. As the output of a single cell falls to around 1.1V before it is considered to be exhausted it cannot drive such an arrangement.

Consequently we are forced back to circuits that use individual transistors. The classical monostable is a good starting point, as shown in Fig.3a. When a magnet passes coil L1 a voltage is produced. If this is in the direction of the arrow, the voltage at H will fall. The resulting negative-going pulse through capacitor C1 causes transistor TR1 to turn off and TR2 to turn on, triggering an even larger pulse through the coil.

The classical circuit meets a difficulty, though. We need to trigger the current early in the induced pulse, perhaps at point F in Fig.2, when the induced voltage might be around 5mV. Transistor TR1 must be given twice the base current needed to saturate it, but its current gain may turn out to be five times its quoted minimum and so could be saturated tenfold. The magnetically induced negative-going pulse at H then needed to bring TR1 out of saturation and trigger the circuit could be as much as 60mV, whereas the available voltage at point F is only 5mV.

MILLIVOLT DRIVER

The millivolt monostable circuit shown in Fig.3b can handle this problem. Here the stable state relies on the comparative values of resistors R1 and R2. Resistor R1 is only about five times larger than R2, but it carries less than one hundredth of the current. Thus the voltage across R1 is small, and the voltage at point K is clamped very near to that at point J, at around 0.6V.

A voltage of about 1.0V is dropped across R2, resulting in a further drop of about 0.25V across R3. The resulting voltage at L holds transistor TR2 turned off, and so the state is stable.

In this circuit TR1 does not become saturated, and it will amplify any pulses applied at J, according to the "four percent" rule. This states that a 1mV drop at the base cuts the collector current by four percent. Thus, when the activated coil reduces the voltage at J by 5mV, TR1's collector current will fall by 20%, raising the voltage at point L enough for TR2 to conduct and trigger pulse regeneration.

With this circuit the sensitivity is much greater, and is independent of transistor gain.

SCHMITT TRIGGER

The millivolt circuit in Fig.3b drives the clock well. But as the battery gets older its internal resistance exceeds that of the coil, causing an additional voltage drop at *J* during the induced "power stroke". Consequently, the circuit can fail to return reliably to a stable state.

As we are only interested in feeding a.c. signals to the base of TR1, though, the circuit can be reconfigured as shown in Fig.3c, in which it behaves as a Schmitt trigger.

When the magnet induces a positive voltage at *S*, current through TR1 is reduced, switching on TR2, which further raises *S* to cause the required regeneration. Here TR2 is controlled by TR1, which is controlled by its base-coil-emitter loop. The troublesome battery resistance is now outside this loop. The circuit works as before, and battery life is extended.

Capacitor C2 in Fig.3b and Fig.3c is effectively connected across the coil and is there to inhibit resonance. Without it the circuit would oscillate in the 250kHz region. In all three circuits potentiometer VR1 is used to adjust the sensitivity.

CLOCK CIRCUIT

In the circuit of Fig.3c, TR2 passes 2mA or so, but only for one-fifth of the time, giving an average consumption of 0.4mA. But resistor R2 takes that much current on a continuous basis. If the current through R2 could be abolished, battery life would be doubled.

It is tempting to increase the value of R2, but then it will not provide enough current to drive TR2 into regeneration when the battery is low. A better solution is to operate the circuit at much higher impedance, and follow with a *pnp* transistor, as shown in Fig.4. It is this circuit that is used in the Cardboard Clock.

Notice in Fig.4 that the coil connections have been reversed, compared to Fig.3c, producing the waveform shown at the top. Also, the value of capacitor C1 has been much reduced. The first half cycle now

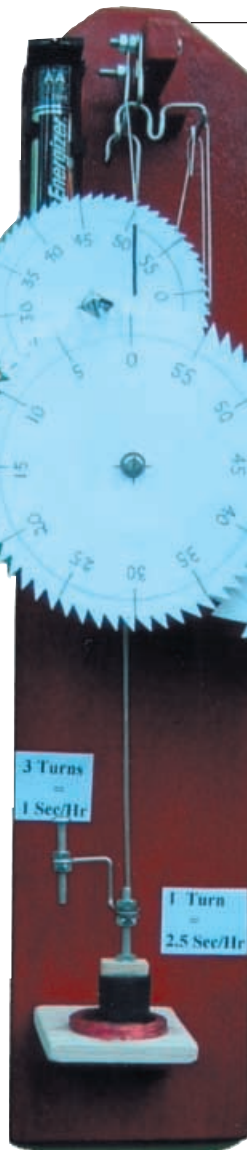


Fig.4. Cardboard Clock three-transistor switch circuit diagram. Average current consumption is 0.5mA.

MECHANICAL CLOCKS

No one knows for sure who invented mechanical clocks, although it is believed that the Chinese did. They began to appear in Europe from about 1310 onwards.

At first they had no hands and just struck a bell on the hour. They were fearsome objects, made by blacksmiths, and driven by a weight whose descent was controlled by an escapement. This was based on a vertical T-piece, made of iron and about the size of an average table. One arm spun the T-piece around its vertical axis by 30° one way, and then another arm returned it. This was a cycle and the cycles were "counted" by gears. The working clock made about as much noise as the blacksmith!

The accuracy was poor, however, and a clock set correctly at sunrise might be half an hour out at sunset. Nevertheless, such a clock was a great asset to any town.

In 1494 Leonardo da Vinci made a drawing of a clock with a pendulum and in 1581 Galileo observed that a pendulum of a given length seemed to move through its cycle in a given amount of time. However, it was Galileo's son Vincenzo who first made a working model of a pendulum clock, in 1649, although he never completed it.

It was not until 1656, though, that Christian Huygens actually made the pendulum clock practical. After a few improvements, it turned out to be about a thousand times more accurate than its medieval predecessors.

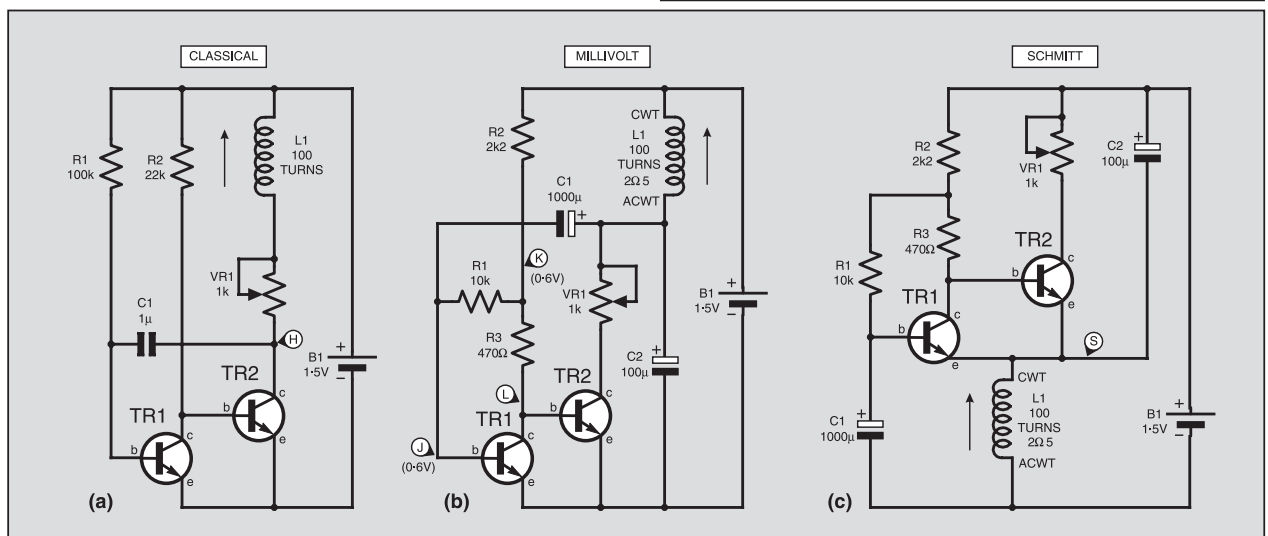
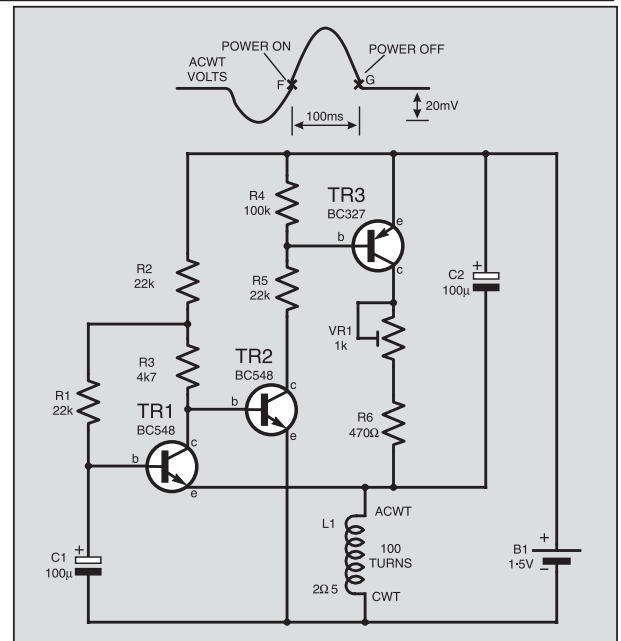


Fig.3. Three monostables. CWT is the clockwise tail of the coil, when viewed from above, and ACWT is anticlockwise.

COMPONENTS

Resistors

R1, R2,	
R5	22k (3 off)
R3	4k7
R4	100k
R6	470Ω

All 0.25W 5% carbon film or better.

Potentiometer

VR1	1k min. preset, side adjustment, p.c.b. mounting
-----	--

Capacitors

C1, C2	100μF radial elect. 6V (2 off)
--------	--------------------------------

Semiconductors

TR1, TR2	BC548 npn transistor (2 off)
TR3	BC327 pnp transistor

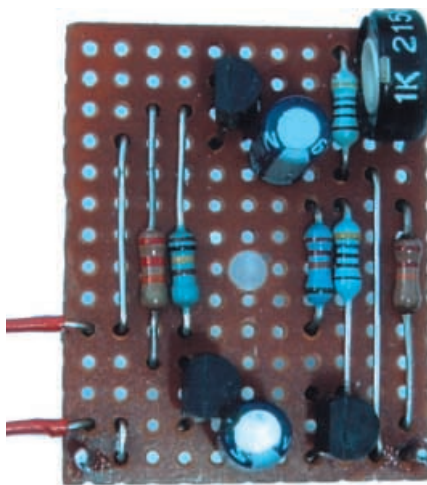
Miscellaneous

Stripboard, 14 holes x 11 strips; disc magnet 15mm diameter, pre-drilled and counter sunk (2 off); AA size battery and holder; 16 s.w.g. enamelled copper wire; 32 s.w.g. enamelled copper wire; M3 25mm bolts, nuts and washers (25 each); robust white card; Blu-tack; balsa wood sheet, 5mm x 75mm x 1 metre; obeche strut, 10mm x 13mm x 1 metre; balsa cement; solid insulated connecting wire; solder, etc.

Approx. Cost
Guidance Only

£15
excl. battery

See
SHOP
TALK
page



Completed circuit board.

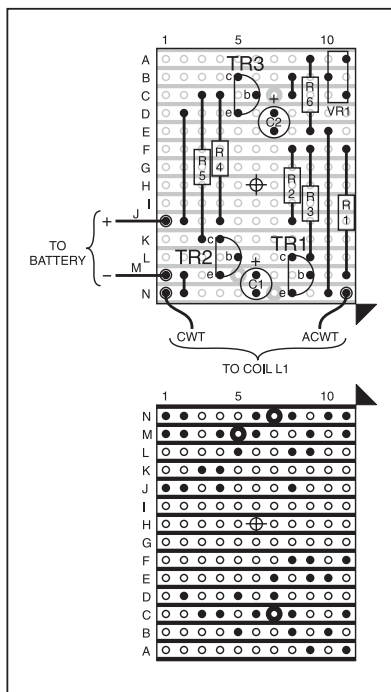


Fig.5. Stripboard layout and track breaks for the three-transistor circuit. There should be no substantial border adjacent to row N. Drill out H6 to 3mm diameter.

of which is outside the scope of this article. Its constructional method is outlined in Fig.6.

Carefully cut a sheet of 5mm thick balsa wood to a size of 45mm x 55mm and drill a 3mm diameter hole at point X, 10mm

from the edge of the shorter side. This is the "coil table".

Mark out on white card a circle of 32mm diameter, and cut it out with care. Knead well some Blu-tack, and form eight spheres of about 1mm diameter. Place them symmetrically around a £1 coin (or other object having a diameter of 22mm), about 1mm from its edge. Turn the coin over and press it very firmly onto the centre of the card. If any trace of Blu-tack shows, remove it with a pin.

Form a neat Blu-tack sphere of 5mm diameter, and locate it centrally on the coin. Turn the whole structure over, and press it very firmly onto the coil table. The coin (not the card) should be just clear of hole X. There must be no gap between coin and table. If there is, rotate the coin under slight pressure, or use less Blu-tack.

COIL WINDING

The coil requires 100 turns of 32s.w.g. insulated copper wire. Take care to avoid tangles or kinks in it. Pass the first 60cm of this wire down through hole X, and fix it below with Blu-tack.

Going slowly, wind 100 turns of the wire onto the coil former. Winding may be in either direction. Keep one eye in the plane of the coil table and make a serious attempt to wind parallel to this plane, but move laterally when necessary, to keep roughly even depth, neglecting neither front nor rear of the coil.

Check regularly that the coil is winding evenly on its hidden side. Wind with minimum tension, or the wire may pull the coin away from the table. If these precautions are observed, the winding is neither a critical nor a lengthy operation.

If you do create a kink, do not attempt to pull it out, but unwind it carefully backwards.

After 100 turns trap the wire at the coil with Blu-tack, and cut it 60cm further on. Drill hole Y well clear of the coil, and pass the wire tail through this hole.

Prepare four "straps" of Blu-tack as long as a matchstick, but twice as thick. Peel the cardboard disc back gently from the coil to its halfway point. Run two of the straps radially across the coil, and pin it down securely. Remove the cardboard completely, and use the remaining two straps to pin down the remainder of the coil. Check that it really is fully pinned down.

Drizzle some balsa cement on the top of the coil, and down its outside, being sure to deliver a good blob to the balsa table. Check that there is a visible flow of cement down the side of the coil, and onto the table. Without delay apply a piece of paper

discharges C1 a little via resistor R1, so that point F on the waveform is now nearer to 0V. This tunes the circuit to favour the waveform shown and helps at low battery voltages.

The battery can now fall to about 1.1V before the clock fails, and average consumption is reduced to 0.5mA. An AA size cell when new produces about 1.6V, and if it is an alkaline type will give about 2100mA-hours before it falls to 1.1V. Hence, it will drive the clock for 4200 hours, or about six months.

CONSTRUCTION

The clock circuit of Fig.4 is built on a piece of stripboard measuring 14 rows by 11 holes, as shown in Fig.5. Drill a 3mm diameter hole at position H6, through which a mounting bolt will be inserted later.

Ensure that the transistors and electrolytic capacitors are inserted the correct way round, and that the four link wires are inserted. After soldering is completed, scrape firmly past each side of each joint with a small screwdriver, to test for solder bridges.

COIL ASSEMBLY

The coil's optimum size and position were found by computer simulation, a discussion

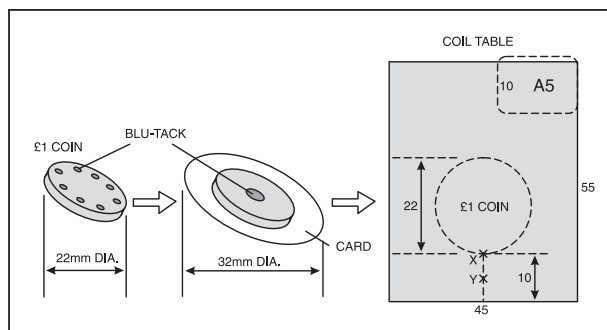


Fig.6. Making the coil former. For the dotted piece A5 see the text. The completed coil is shown in the photograph.

to smooth away the cement lying on top of the coil, so that it will not project. Repeat the procedure at three other points, and allow to dry for an hour.

Once the cement has dried, carefully remove the coin and the Blu-tack, then drizzle more cement down the inside of the coil.

HARDWARE

Details of the wood and metalwork assembly are shown in Fig.7 and Fig.8. They should be used in conjunction with the photographs.

The strut in Fig.7a is made from obeche wood, just slightly harder than balsa but

still easy to work. Drill 3mm holes in the strut at points B, C and E, and cut the five sections, A1 to A5.

Cement section A5 below the coil table, but 1mm proud, as shown in Fig.6.

The backboard in Fig.7b is made from balsa wood. Carefully drill 3mm holes at G, H and I, and then drill out hole G to

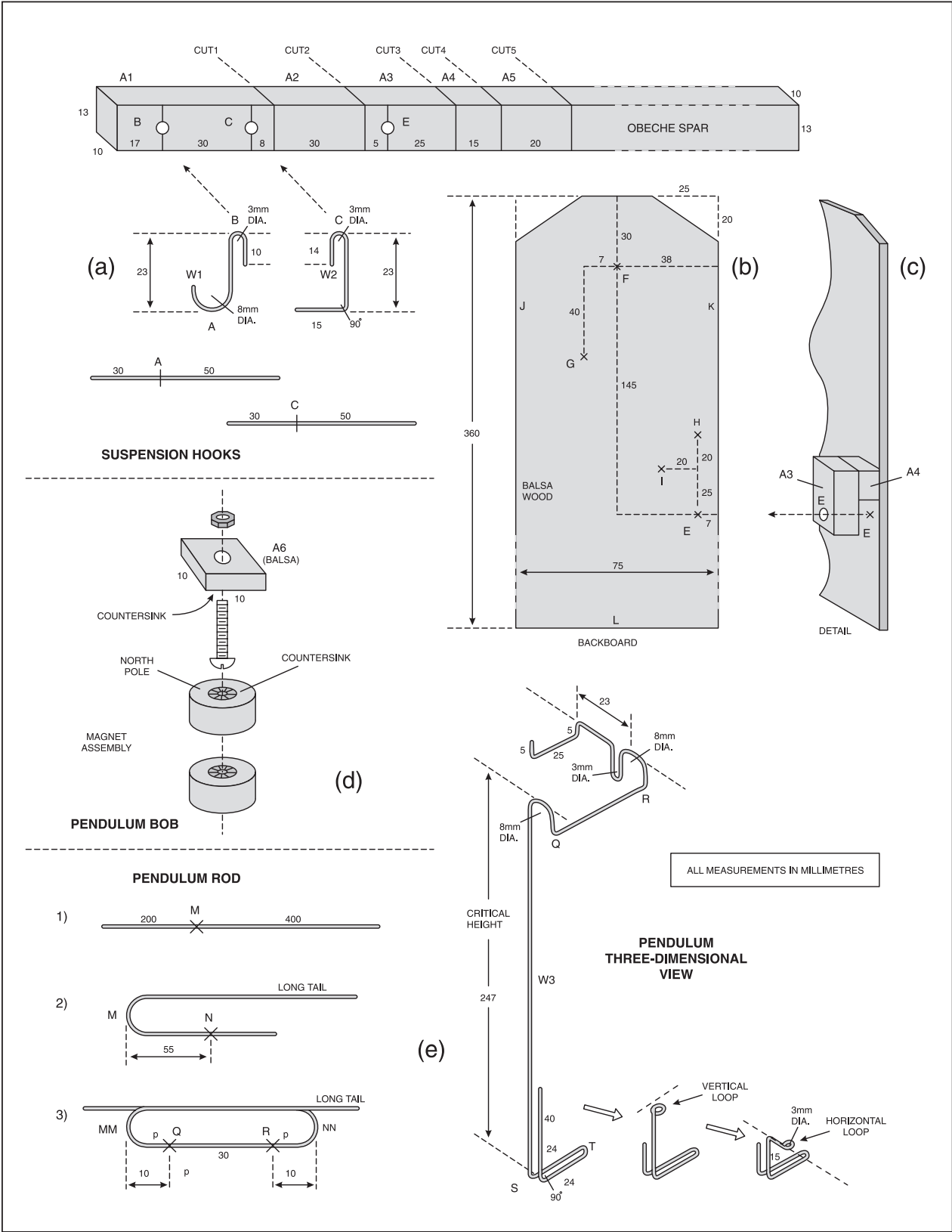


Fig.7. Backboard and pendulum construction details (not to scale).

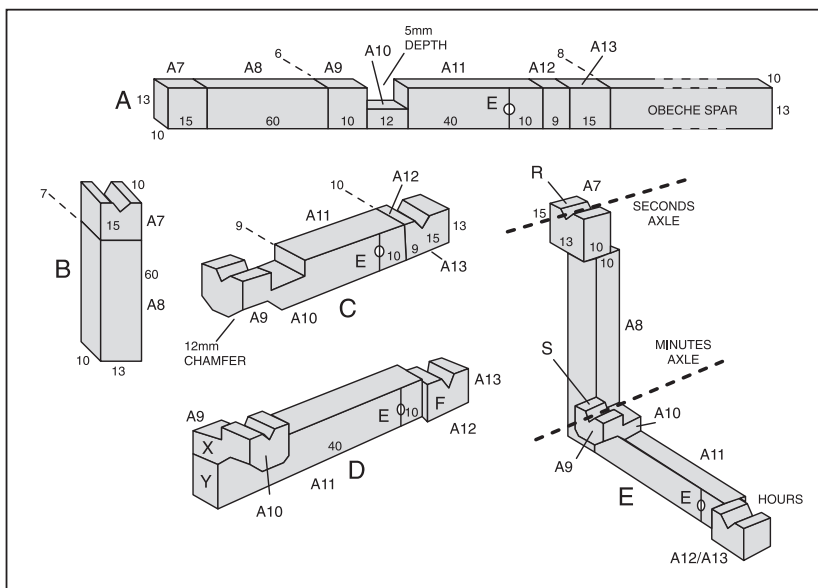


Fig.8. Wheel bearings (not to scale).

10mm. Fix the battery holder as shown in the photograph. Cut a matchstick into three parts and cement the pieces behind the board at J, K and L, with each piece parallel to the nearby edge.

Cement sections A3 and A4 as shown in Fig.7c. Point E on the board should be visible through hole E in section A3. Cement section A1 end on centrally at point F, and then cement section A2 to its right as a support, as in the photograph.

Suspension hooks W1 and W2 (Fig.7a) are bent from 80mm lengths of 16s.w.g. enamelled copper wire. Pendulum rod W3, Fig.7e, is formed from a 600mm length. The bends can be formed around screwdrivers having shafts of about 3mm and 8mm diameter as appropriate.

Note that the pendulum rod requires a loop to be formed at its lower end. First form it while the end is in a vertical position, and then bend the last 15mm sideways. This will be used for timing adjustment, as described later.

Pendulum bob suspended above the coil.



Pendulum suspension hooks and wooden support bar.

ASSEMBLY

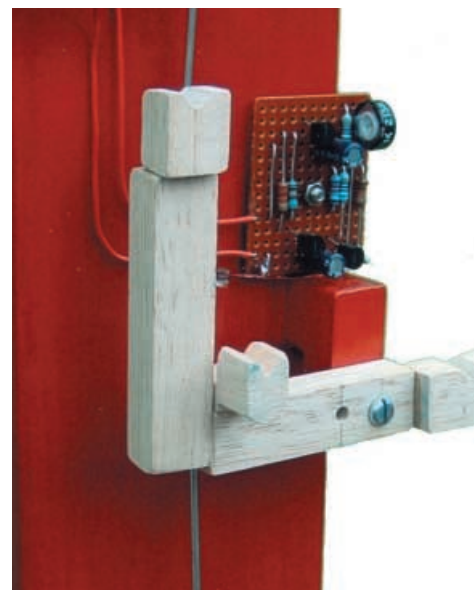
Starting from behind the backboard, pass a bolt through hole H, and through hole H6 in the electronics stripboard assembly. Secure the stripboard to the backboard and run its power supply connections over the front of the board to connect to the battery holder, using solid-core insulated connecting wire.

From the rear of pendulum post A1, insert bolts through holes B and C. Mount suspension hooks W1 and W2 onto these bolts, using washers under the nuts. Hold the backboard vertical and adjust the hooks carefully so that the 15mm length at W2 point D is horizontal and tangential to W1 bend A.

From the 5mm thick balsa cut a 10mm × 10mm square, section A6 in Fig.7d. Drill a central hole, countersink it slightly and attach a bolt and nut. Cement together the magnets, which are supplied with countersunk holes, and the board as shown to form the pendulum bob. The magnets should have their North poles facing uppermost.

The clock should hang on a wall where it is unlikely to be jolted. To obtain proper balance insert the battery/holder and secure the backboard via 10mm hole G.

Use nuts and washers to suspend the bob from bend T on the pendulum (W3), with



Time wheels axle bearing assembly mounted on the backboard.

equal amounts of thread showing on the suspension screw above and below its fixing point. Hang the pendulum on its W1 and W2 hooks. It has two large (8mm diameter) bends from which it hangs. Check that the planes of these bends are parallel, and perpendicular to their axis of rotation.

Select a suitable rubber band and pass it around the backboard and section A4 on the coil table, as a temporary fixing.

Bend the pendulum rod and adjust the position of the coil table so that when the magnet is at rest it sits squarely over the coil, and when it moves it must clear the coil by one millimetre. A smaller gap is not advisable because air resistance increases sharply. Note that the coil table will not be central. Mark its position.

Looking down on the coil and going around it clockwise leads to the clockwise tail, CWT – make a mark on it for identification. Drill a hole in the backboard 5mm below the coil table and take both coil wires through it to the back. Then pass them both through hole I, pull them tight, and cut to about 15cm.

Clean the enamel from the ends of the wires, then tin and solder them to the allocated pins on the stripboard. Draw all surplus wire back through hole I, and trap it behind the backboard with adhesive tape.

WHEEL BEARINGS

The axle for each toothed wheel is a 3M bolt 25mm long. Each bearing is a V-shaped groove, so that there are two points of contact with the bolt. This eliminates any tendency for the wheel to roll backwards. Drill, cut and assemble the obeche sections as in Fig.8. The cuts are indicated by the numbered dotted lines, 6 to 10.

Mount section A12/A13 3mm forward as in Fig.8d, and ensure that there is no step between surfaces X and Y of A9/A10 and A11.

Cement the sections as shown in Fig.8e. Before the cement dries lay the structure on its back, and adjust the vertical post (A7/A8), to produce exactly 52mm centre to centre between the axles of the seconds and minutes wheels. This measurement is

critical. It is best taken between the nearby edges marked R and S.

When dry, push a bolt through holes E in Fig.8e and Fig.7c and tighten a nut on it, with the seconds wheel support span (A7/A8) vertical.

MARKING TIME

Maximum accuracy is needed for all wheels. A geometry compass, protractor and sharp HB pencil are needed. In place of the protractor, the template shown in Fig.9 could be used. The 60 dots at the perimeter are 6° apart.

First cut out from card three circles having a 20mm radius, for use as backing plates for the time wheels.

For the hours wheel draw two concentric circles of radius 40mm and 45mm, and cut out round the outer circle. Using the protractor or template as a guide, draw radial lines at 15° intervals from the centre to the edge of the disc.

All pencil lines should be drawn on the side that will be hidden when the wheels are assembled. Take this into account when making the "teeth" cuts, so that they face in the correct direction, as shown in the photographs.

Cut in along each of the radials as far as the 40mm circle. Then cut the teeth at an angle between the outer rim and this circle.

For the minutes wheel draw circles of radius 45mm and 50mm, and then repeat as for the Hours wheel, only this time at 6° intervals.

The seconds wheel requires maximum accuracy. Draw circles of radius 33mm and

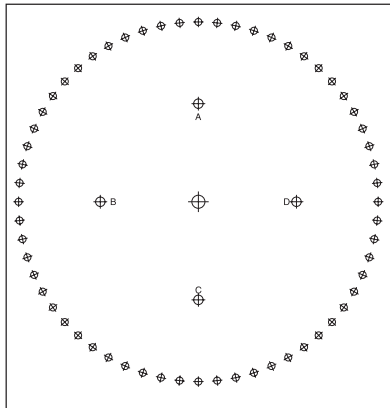


Fig.9. Template (half-size) for the clock wheels.

35mm, and radial lines again at 6° intervals. Cut out the circle and teeth. Beware that one badly placed cut is enough to compromise the wheel.

Notate the front of the discs with their time-indicating lines and numerals.

With each toothed wheel, use a pencil to enlarge its central hole and that of a backing plate to accept a bolt. Lay down a thin continuous track of balsa cement inside the circumference of a backing disc.

Load the wheel and backing disc onto a bolt and press them together. Remove the bolt, ensure that the wheel is lying quite flat, and allow the cement to dry. Then fit the bolt again, using a washer on either side (two washers for the front of the

seconds and minutes wheels), and secure the bolt with a nut. Add a further four nuts at the end of the bolt, place the wheel on its bearing and adjust these nuts to give 0.5mm of play. With the seconds wheel the nuts also act as a counter weight.

SECONDS OUT

The seconds actuators are made from solid connecting wire, shaped as shown in Fig.10.

Hang the ratchet, Fig.10a, from its draw-bar. Place the seconds wheel on its bearing, adjusting its counterweight nuts to allow 0.5mm play. Rotate the axle support system at its fixing bolt, so that the seconds wheel teeth at their extremities just touch the ratchet.

Connect the battery to the circuit board, set the wiper of preset VR1 to midway and swing the pendulum to start the clock.

Having observed the pendulum for while, if necessary stop it swinging and then slightly reduce the 30° angle on the ratchet, so that it tilts towards the wheel to drive it correctly.

When satisfied, adjust VR1 so that the ratchet swings back and forth over a distance of (ideally!) 1.7 teeth, so optimising the circuit's efficiency.

Disconnect the battery before progressing with the next stage.

WHEEL ASSEMBLY

The minutes wheel is driven by a spike on the front of the seconds wheel. This is made from solid connecting wire, as shown in Fig.10b.

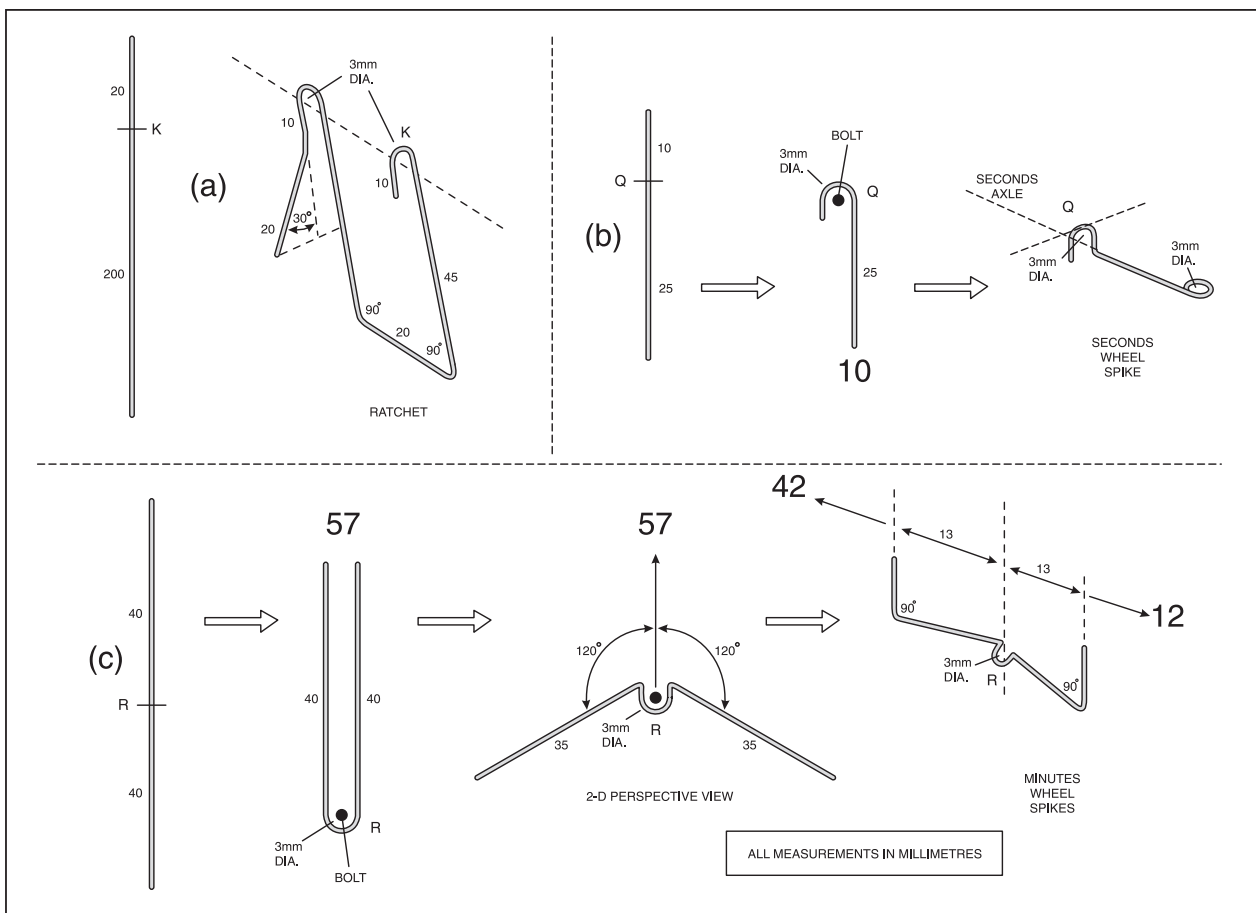
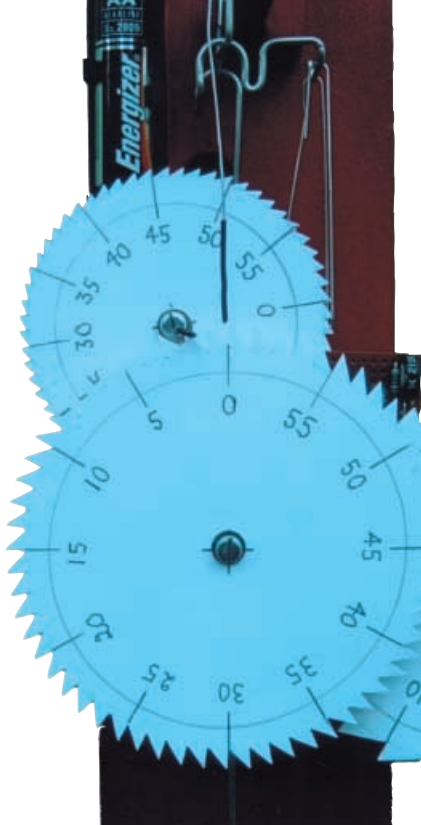


Fig.10. Three actuators, made from connecting wire. The large numerals indicate direction of installation, by referring to teeth numbers on the wheels.



Timewheels assembly.

Mount it between the two washers in front of the seconds wheel, so that it points towards numeral 10. Bend the spike forward where it leaves the washers so that it runs parallel to the axle, and form a small vertical loop at the end. Adjust the spike so that its loop enters three-quarters of the way into the minutes wheel teeth. Check its action at different positions.

The hours wheel is driven by a double spike (Fig.10c) behind the minutes wheel. Fix it between the two washers immediately behind the minutes wheel, so that both arms point to numeral 57.

Bend the spike arms back by 120° where they leave the washers, and form a 90° bend on each at exactly 13mm from the centre of the bolt, to form the "working" arms.

View the arms in line with the axle, and adjust them to align with wheel numerals 12 and 42. Place the wheel on its bearing and trim the working arm lengths so that they clear the horizontal spar by 2mm. Check that the arms do not foul the seconds wheel.

Place the hours wheel on its bearing, and rotate the minutes wheel clockwise, to check for proper operation. If more friction is needed on the minutes wheel, make its V bearing steeper, or balance it better by adding a small piece of card.

KEEPING TIME

Seconds are read at the ratchet, minutes and hours at the top of their wheels.

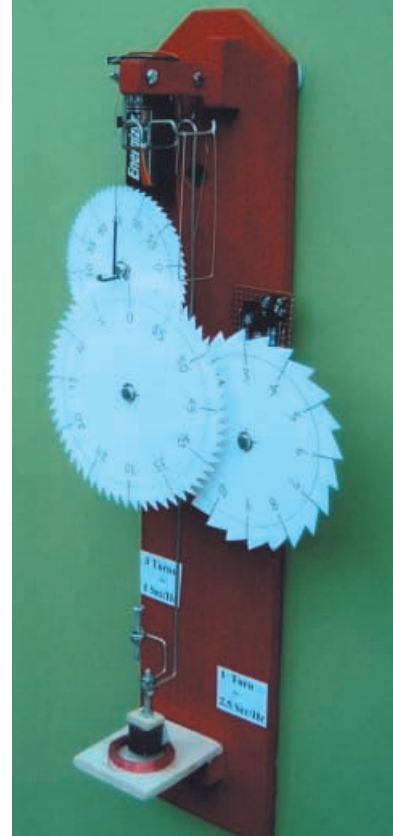
Hang a piece of insulated wire from the front screw on the pendulum post to act as a pointer to the minutes.

Run a nut halfway up a 25mm bolt and rest this assembly in the last loop on the pendulum wire (W3, Fig.7a). Fix the nut to the wire with two spots of cement, but avoid fouling the thread. This screw is the fine adjuster.

The main adjuster is that provided by the bolt on the magnet assembly (see Pendulum Bob photograph). Lowering this assembly by one turn of its supporting bolt will slow the clock by 2.5 seconds per hour.

To make adjustments, loosen the upper bolt (at the end of the pendulum) and hold the lower one (on the magnet bolt) while rotating the magnet. Then readjust the coil table, using the bolt through hole E in section A3 (Fig.7c).

Using this method, bring the clock error within ± 2 seconds per hour. Then apply cement to section A6 under the coil table, and press it onto the backboard in the correct position. The rubber band (see earlier) must continue to press it firmly home while the cement dries, or the necessary right angle can be compromised. From now on the suspension hooks should not be undone.



To check that all is well, allow the clock to run while the cement dries.

Clock error should now be within the range of the fine adjuster on the pendulum assembly. Lowering that bolt by three complete turns slows the clock by one second per hour, but only if the pendulum is handled gently!

Timing depends slightly on the rolling point of the pendulum, and this depends slightly on how it is started. To minimise surprises, follow a standard starting drill. Use a pencil to move the pendulum almost as far as it will go to the right, and release. Set the time after the swing has stabilised.

Do not allow anything magnetic to come near the coil or the timekeeping property of the pendulum will be severely affected.

You may find it difficult not to clock-watch! ☐

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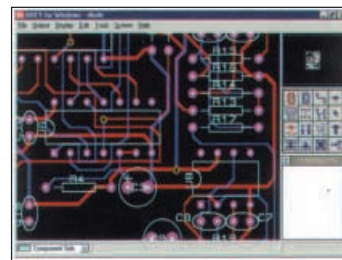


Logic Probe testing

Electronic Projects is split into two main sections: **Building Electronic Projects** contains comprehensive information about the components, tools and techniques used in developing projects from initial concept through to final circuit board production. Extensive use is made of video presentations showing soldering and construction techniques. The second section contains a set of ten projects for students to build, ranging from simple sensor circuits through to power amplifiers. A shareware version of Matrix's CADPACK schematic capture, circuit simulation and p.c.b. design software is included.

The projects on the CD-ROM are: Logic Probe; Light, Heat and Moisture Sensor; NE555 Timer; Egg Timer; Dice Machine; Bike Alarm; Stereo Mixer; Power Amplifier; Sound Activated Switch; Reaction Tester. Full parts lists, schematics and p.c.b. layouts are included on the CD-ROM.

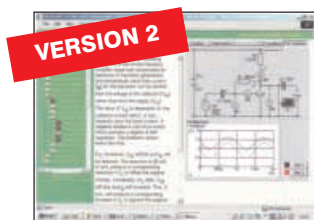
ELECTRONICS CAD PACK



PCB Layout

Electronics CADPACK allows users to design complex circuit schematics, to view circuit animations using a unique SPICE-based simulation tool, and to design printed circuit boards. CADPACK is made up of three separate software modules. (These are restricted versions of the full Labcenter software.) **ISIS Lite** which provides full schematic drawing features including full control of drawing appearance, automatic wire routing, and over 6,000 parts. **PROSPICE Lite** (integrated into ISIS Lite) which uses unique animation to show the operation of any circuit with mouse-operated switches, pots, etc. The animation is compiled using a full mixed mode SPICE simulator. **ARES Lite** PCB layout software allows professional quality PCBs to be designed and includes advanced features such as 16-layer boards, SMT components, and an autorouter operating on user generated Net Lists.

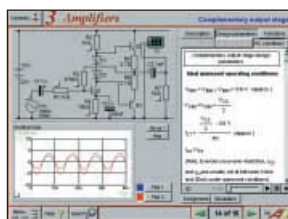
ELECTRONIC CIRCUITS & COMPONENTS V2.0



Circuit simulation screen

Provides an introduction to the principles and application of the most common types of electronic components and shows how they are used to form complete circuits. The virtual laboratories, worked examples and pre-designed circuits allow students to learn, experiment and check their understanding. Version 2 has been considerably expanded in almost every area following a review of major syllabuses (GCSE, GNVQ, A level and HNC). It also contains both European and American circuit symbols. Sections include: **Fundamentals**: units & multiples, electricity, electric circuits, alternating circuits. **Passive Components**: resistors, capacitors, inductors, transformers. **Semiconductors**: diodes, transistors, op.amps, logic gates. **Passive Circuits**. **Active Circuits**. **The Parts Gallery** will help students to recognise common electronic components and their corresponding symbols in circuit diagrams. Included in the Institutional Versions are multiple choice questions, exam style questions, fault finding virtual laboratories and investigations/worksheets.

ANALOGUE ELECTRONICS

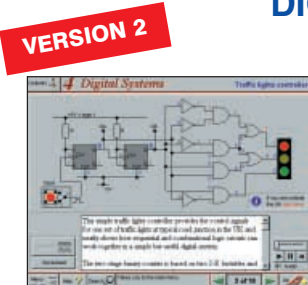


Complimentary output stage

Analogue Electronics is a complete learning resource for this most difficult branch of electronics. The CD-ROM includes a host of virtual laboratories, animations, diagrams, photographs and text as well as a SPICE electronic circuit simulator with over 50 pre-designed circuits.

Sections on the CD-ROM include: **Fundamentals** – Analogue Signals (5 sections), Transistors (4 sections), Waveshaping Circuits (6 sections). **Op.Amps** – 17 sections covering everything from Symbols and Signal Connections to Differentiators. **Amplifiers** – Single Stage Amplifiers (8 sections), Multi-stage Amplifiers (3 sections). **Filters** – Passive Filters (10 sections), Phase Shifting Networks (4 sections), Active Filters (6 sections). **Oscillators** – 6 sections from Positive Feedback to Crystal Oscillators. **Systems** – 12 sections from Audio Pre-Amplifiers to 8-Bit ADC plus a gallery showing representative p.c.b. photos.

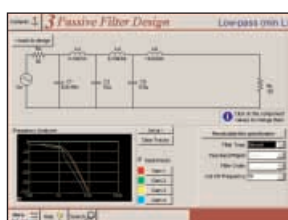
DIGITAL ELECTRONICS V2.0



Virtual laboratory – Traffic Lights

Digital Electronics builds on the knowledge of logic gates covered in *Electronic Circuits & Components* (opposite), and takes users through the subject of digital electronics up to the operation and architecture of microprocessors. The virtual laboratories allow users to operate many circuits on screen. Covers binary and hexadecimal numbering systems, ASCII, basic logic gates, monostable action and circuits, and bistables – including JK and D-type flip-flops. Multiple gate circuits, equivalent logic functions and specialised logic functions. Introduces sequential logic including clocks and clock circuitry, counters, binary coded decimal and shift registers. A/D and D/A converters, traffic light controllers, memories and microprocessors – architecture, bus systems and their arithmetic logic units. Sections on Boolean Logic and Venn diagrams, displays and chip types have been expanded in Version 2 and new sections include shift registers, digital fault finding, programmable logic controllers, and microcontrollers and microprocessors. The Institutional versions now also include several types of assessment for supervisors, including worksheets, multiple choice tests, fault finding exercises and examination questions.

FILTERS



Filter synthesis

Filters is a complete course in designing active and passive filters that makes use of highly interactive virtual laboratories and simulations to explain how filters are designed. It is split into five chapters: **Revision** which provides underpinning knowledge required for those who need to design filters. **Filter Basics** which is a course in terminology and filter characterization, important classes of filter, filter order, filter impedance and impedance matching, and effects of different filter types. **Advanced Theory** which covers the use of filter tables, mathematics behind filter design, and an explanation of the design of active filters. **Passive Filter Design** which includes an expert system and filter synthesis tool for the design of low-pass, high-pass, band-pass, and band-stop Bessel, Butterworth and Chebyshev ladder filters. **Active Filter Design** which includes an expert system and filter synthesis tool for the design of low-pass, high-pass, band-pass, and band-stop Bessel, Butterworth and Chebyshev op.amp filters.

ROBOTICS & MECHATRONICS



Case study of the Milford Instruments Spider

Robotics and Mechatronics is designed to enable hobbyists/students with little previous experience of electronics to design and build electromechanical systems. The CD-ROM deals with all aspects of robotics from the control systems used, the transducers available, motors/actuators and the circuits to drive them. Case study material (including the NASA Mars Rover, the Milford Spider and the Furby) is used to show how practical robotic systems are designed. The result is a highly stimulating resource that will make learning, and building robotics and mechatronic systems easier. The Institutional versions have additional worksheets and multiple choice questions.

- Interactive Virtual Laboratories
- Little previous knowledge required
- Mathematics is kept to a minimum and all calculations are explained
- Clear circuit simulations

PRICES

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PICmicro TUTORIALS AND PROGRAMMING

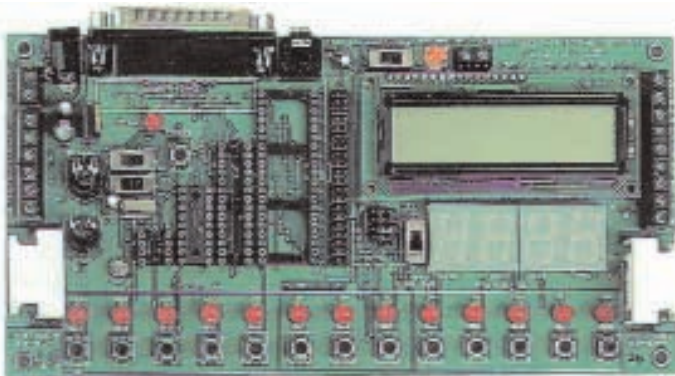
HARDWARE

VERSION 2 PICmicro MCU DEVELOPMENT BOARD

Suitable for use with the three software packages listed below.

This flexible development board allows students to learn both how to program PICmicro microcontrollers as well as program a range of 8, 18, 28 and 40-pin devices. For experienced programmers all programming software is included in the PPP utility that comes with the development board. For those who want to learn, choose one or all of the packages below to use with the Development Board.

- Makes it easier to develop PICmicro projects
- Supports low cost Flash-programmable PICmicro devices
- Fully featured integrated displays – 13 individual I.e.d.s, quad 7-segment display and alphanumeric I.c.d. display
- Supports PICmicro microcontrollers with A/D converters
- Fully protected expansion bus for project work
- All inputs and outputs available on screw terminal connectors for easy connection



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12V 500mA plug-top PSU (UK plug) £7
25-way 'D' type connecting cable £5

SOFTWARE

Suitable for use with the Development Board shown above.

ASSEMBLY FOR PICmicro V2 (Formerly PICtutor)

Assembly for PICmicro microcontrollers V2.0 (previously known as PICtutor) by John Becker contains a complete course in programming the PIC16F84 PICmicro microcontroller from Arizona Microchip. It starts with fundamental concepts and extends up to complex programs including watchdog timers, interrupts and sleep modes. The CD makes use of the latest simulation techniques which provide a superb tool for learning: the Virtual PICmicro microcontroller. This is a simulation tool that allows users to write and execute MPASM assembler code for the PIC16F84 microcontroller on-screen. Using this you can actually see what happens inside the PICmicro MCU as each instruction is executed which enhances understanding.

- Comprehensive instruction through 39 tutorial sections
- Includes Vlab, a Virtual PICmicro microcontroller: a fully functioning simulator
- Tests, exercises and projects covering a wide range of PICmicro MCU applications
- Includes MPLAB assembler
- Visual representation of a PICmicro showing architecture and functions
- Expert system for code entry helps first time users
- Shows data flow and fetch execute cycle and has challenges (washing machine, lift, crossroads etc.)
- Imports MPASM files.



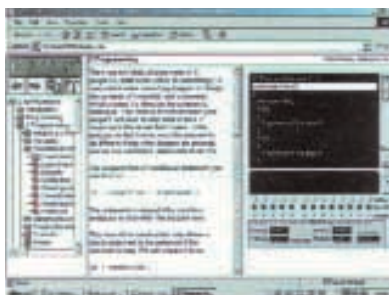
Virtual PICmicro

'C' FOR PICmicro VERSION 2

The C for PICmicro microcontrollers CD-ROM is designed for students and professionals who need to learn how to program embedded microcontrollers in C. The CD contains a course as well as all the software tools needed to create Hex code for a wide range of PICmicro devices – including a full C compiler for a wide range of PICmicro devices.

Although the course focuses on the use of the PICmicro microcontrollers, this CD-ROM will provide a good grounding in C programming for any microcontroller.

- Complete course in C as well as C programming for PICmicro microcontrollers
- Highly interactive course
- Virtual C PICmicro improves understanding
- Includes a C compiler for a wide range of PICmicro devices
- Includes full Integrated Development Environment
- Includes MPLAB software
- Compatible with most PICmicro programmers
- Includes a compiler for all the PICmicro devices.



Minimum system requirements for these items: Pentium PC running Windows 98, NT, 2000, ME, XP; CD-ROM drive; 64MB RAM; 10MB hard disk space.

FLOWCODE FOR PICmicro

Flowcode is a very high level language programming system for PICmicro microcontrollers based on flowcharts. Flowcode allows you to design and simulate complex robotics and control systems in a matter of minutes.

Flowcode is a powerful language that uses macros to facilitate the control of complex devices like 7-segment displays, motor controllers and I.c.d. displays. The use of macros allows you to control these electronic devices without getting bogged down in understanding the programming involved.

Flowcode produces MPASM code which is compatible with virtually all PICmicro programmers. When used in conjunction with the Version 2 development board this provides a seamless solution that allows you to program chips in minutes.

- Requires no programming experience
- Allows complex PICmicro applications to be designed quickly
- Uses international standard flow chart symbols (ISO5807)
- Full on-screen simulation allows debugging and speeds up the development process
- Facilitates learning via a full suite of demonstration tutorials
- Produces ASM code for a range of 8, 18, 28 and 40-pin devices
- Institutional versions include virtual systems (burglar alarms, car parks etc.).



Burglar Alarm Simulation

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TEACH-IN 2000 – LEARN ELECTRONICS WITH EPE

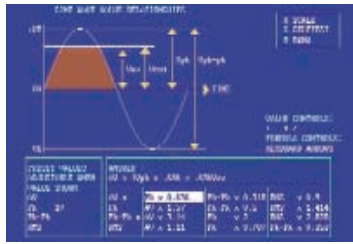
EPE's own *Teach-In* CD-ROM, contains the full 12-part *Teach-In* series by John Becker in PDF form plus the *Teach-In* interactive software covering all aspects of the series. We have also added Alan Winstanley's highly acclaimed *Basic Soldering Guide* which is fully illustrated and which also includes *Desoldering*. The *Teach-In* series covers: Colour Codes and Resistors, Capacitors, Potentiometers, Sensor Resistors, Ohm's Law, Diodes and L.E.D.s, Waveforms, Frequency and Time, Logic Gates, Binary and Hex Logic, Op.amps, Comparators, Mixers, Audio and Sensor Amplifiers, Transistors, Transformers and Rectifiers, Voltage Regulation, Integration, Differentiation, 7-segment Displays, L.C.D.s, Digital-to-Analogue.

Each part has an associated practical section and the series includes a simple PC interface so you can use your PC as a basic oscilloscope with the various circuits.

A hands-on approach to electronics with numerous breadboard circuits to try out.

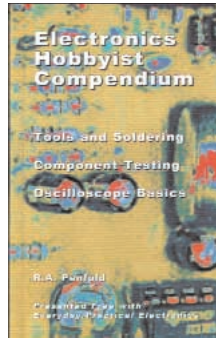
£12.45 including VAT and postage. Requires Adobe Acrobat (available free from the Internet – www.adobe.com/acrobat).

FREE WITH EACH TEACH-IN CD-ROM – *Electronics Hobbyist Compendium* 80-page book by Robert Penfold. Covers Tools For The Job; Component Testing; Oscilloscope Basics.

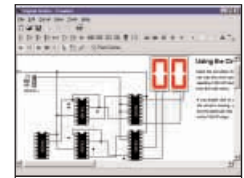


Sine wave relationship values

FREE BOOK WITH TEACH-IN 2000 CD-ROM



DIGITAL WORKS 3.0



Counter project

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VERSION 3

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PRACTICALLY SPEAKING

Robert Penfold looks at the Techniques of Actually Doing It!

UNLESS you are into building valve equipment, at least one semiconductor will feature in every project that you build. It is too soon to write-off discrete transistors and diodes, but they are used relatively little in modern designs.

These days most projects are based on integrated circuits (i.c.s). Locating the correct integrated circuit in component catalogues tends to be problematic for beginners, and can occasionally give problems to "old hands".

Integrated circuits tend to be divided into various categories in catalogues, so you have to look in the right category in order to stand any chance of finding a given device. There might be a complete list of all the semiconductors on offer, but locating a device in a list having many thousands of entries could be difficult and quite time consuming.

In There Somewhere

Beginners tend to be nonplussed by the markings on many integrated circuits, and also those on some other components. The problem is the "extras" that seem to be included on every device (see Fig.1).

There will usually be a manufacturer's logo, and the country of manufacture might also be included. Anything else is unlikely to be of any significance.

Typically there is a batch number or the date of manufacture in some cryptic form such as the number of days since the factory was opened. It can be confusing at first, but you soon get used to picking out the type number from the extraneous characters.

Locating the right device is much easier if you understand the fundamentals of integrated circuit type numbers. No doubt there are exceptions, but virtually all integrated circuits type numbers consist of three sections. The first part of the type number indicates the manufacturer, and it usually consists of two or three letters. Matters are complicated by the fact that a manufacturer may use more than one set of identification letters. The prefix for linear devices could be different to the prefix for logic types for example.

A further complication is that integrated circuits are often second-sourced. Industrial customers prefer not to be tied to a single source of supply, so integrated circuits are often produced under license by a second or even a third manufacturer. In some cases the second-source components retain the original type

number, but the prefix is often changed to that of the second-source manufacturer.

What this means in practice is that there is no need to panic if the first two or three letters in the type number of a device you obtain are not what you were expecting. If you require an MC1458CP but are supplied with a CA1458E they will actually be the same device from different manufacturers. They are manufactured by Motorola and RCA respectively.

The most popular devices are actually manufactured by several companies, and can be obtained with a range of prefixes in the type number. While this state of affairs is far from ideal, and it does leave room for errors, you soon get used to it.

With some European devices the first three letters of the type number indicate the kind of integrated circuit rather than the manufacturer. These are the devices that have prefixes such as TBA, TCA, TDA, TEA, etc. Clearly with these it is essential to obtain a device that has the right prefix, and a (say) TDA820 is definitely not the same as a TBA820.

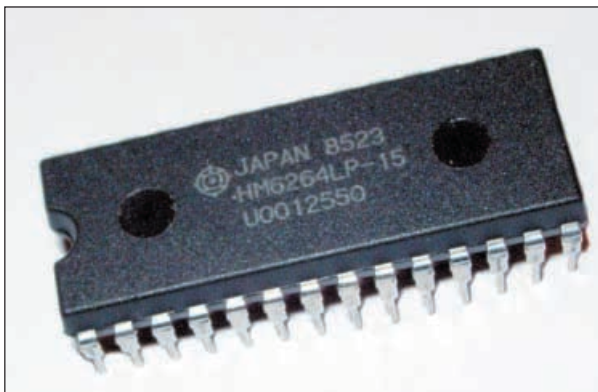


Fig.1. This is a 6264 memory chip. Unusually, there is a suffix to the suffix (-15) that indicates the chip's speed.

The middle part of a type number is what you have to regard as the real type number. It is usually from three to five digits in length, and consists entirely of numeric characters. It is highly unlikely that you would encounter a semiconductor that has the type number you require but is actually the wrong device.

However, there is no harm in looking at the description of a device to check that it ties in correctly with the required device. If the specified device is a PIC microcontroller but the device in the catalogue is an operational amplifier, you have obviously not found the right component. A further search through the catalogue should soon locate the correct device.

Tail Piece

The final part of a type number is important, and potentially confusing. It indicates the package type, and usually consists of one or two letters. A wide range of package types are used in the electronics industry, but the integrated circuits used in designs for the home constructor are almost invariably housed in d.i.l. (dual in-line) plastic encapsulations. Dual in-line just means that the device has two lines of pins, one along each side of the body.

Unhelpfully, a given package often has several different suffix letters, with each manufacturer tending to do "its own thing". In the previous example the suffix letters were "CP" and "E". The CP suffix is quite common, with the "C" and "P" respectively indicating a dual in-line package and plastic construction. In the second example the single letter E means exactly the same thing. Devices having "CN", "C", "N", "CS", "P", and "G" suffixes all have a plastic d.i.l. encapsulation, and no doubt there are many more alternatives.

The suffix used to be of little importance, because the devices available to amateur users always had plastic d.i.l. encapsulations. In some catalogues you will probably still find that few devices, if any, are offered in an alternative type of case.

However, it is becoming increasingly common for surface-mount versions to be included, so more care is needed when ordering devices that are listed in two versions. The component catalogue should make it perfectly clear which device is which.

You also need to take care when ordering integrated circuits from a company that is primarily supplying components to industry (RS and Premier Farnell for instance).

Popular devices are often available from these sources in a range of case styles. The catalogue or web site usually indicates the case style of each version, so there should be no problems provided you check this point prior to ordering.

The range of integrated circuits on offer from the main suppliers is so vast that they are categorised. This makes it easier to find a given device, but only if you understand the way devices are categorised.

There are usually two main categories of logic device, which are the 4000 series CMOS integrated circuits and the 74 series TTL chips. The CMOS chips have basic type numbers starting at 4000. The "A" suffix chips are

now long obsolete so you should only be offered the current "B" series devices. Provided the basic type number is right, you should be supplied with the correct chip.

Family Differences

Matters are more convoluted with TTL integrated circuits. The original range is now largely obsolete, as are many of the "turbo charged" ranges. A few of the improved ranges are still in common use though.

The main type number of the original devices has "74" as the first two digits, followed by a two or three digit serial number. Essentially the same method is retained in the current devices, but two or three letters are added between the "74" and the serial number. These letters denote which family of "super" devices the chip comes from.

Some of the letters are: "LS" for low-power Schottky; "HC" for high-speed CMOS and "HCT" for the high-speed CMOS devices that operate at normal TTL voltage levels. The original 7432 is therefore available as the 74LS32, the 74HC32, and the 74HCT32.

While there is not a total lack of compatibility between the various TTL families, it is definitely in short supply. Consequently, it is very important to ensure that you always obtain the correct version.

There are many digital chips that are not 4000 or 7400 series. These include such things as microcontrollers, and interfacing chips. These are usually listed in two or three subcategories, so there should be no difficulties provided you have some idea of the chip's purpose.

The non-logic devices tend to be lumped together in the general category of "linear" integrated circuits. The range of devices covered is pretty huge, and includes audio and other low frequency chips, radio and communications chips, timers and oscillators, special purpose devices, etc.

There will usually be a few devices that are not, strictly speaking, linear type, but do not really fit properly into any of the main categories. If you are looking for a chip that is not a standard logic device or computing chip, it will probably be listed in the linear devices.

Voltage Regulators

Voltage regulators might appear in the linear section, but this ever growing range of devices usually has a category of its own. The popular voltage regulators are produced by a large number of manufacturers, so they are usually referred to by their basic type numbers with no prefixes or suffixes included. Actually, in some cases the type numbers might be abandoned altogether. In both component lists and catalogues the voltage and current ratings are sometimes used instead.

Matters are much easier if you understand the way in which the type numbering operates for the standard regulator chips. Devices for operation with positive supplies have type numbers

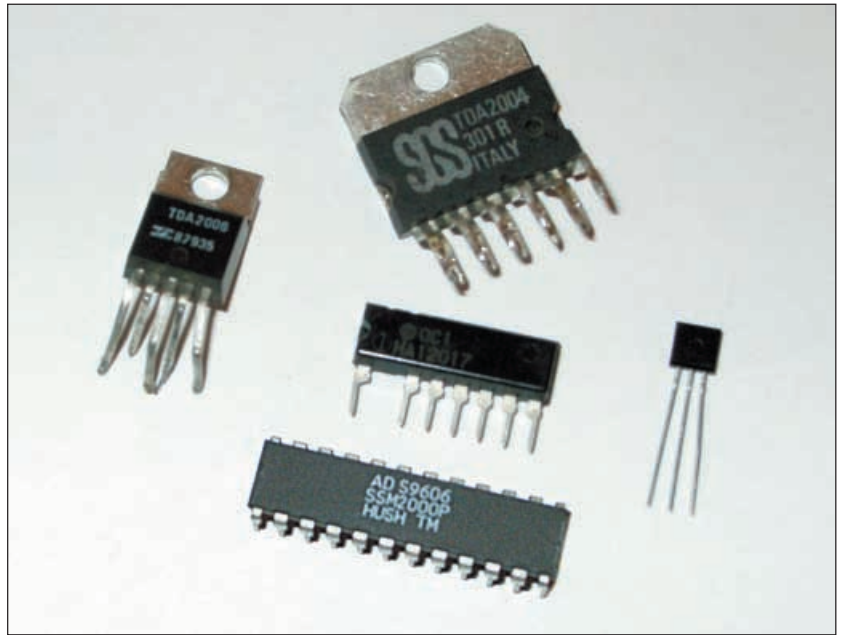


Fig.2. Integrated circuits come in a variety of shapes and sizes. The d.i.l. devices are by far the most common though.

that begin with "78", and those for operation with negative supplies have type numbers that start with "79".

The normal regulators operate at a current of up to one amp, and with these the next part of the type number is two digits that indicate the output voltage. A 7805 is therefore a 5-volt positive regulator, and a 7912 is a 12-volt negative type. There are about half a dozen standard output voltages from five to 30 volts.

Chips with other maximum operating currents are available, and a letter inserted in the middle of the number indicates the current rating. An "L" is used for 0.1A (100mA) chips, an "M" for 0.5A types, and an "S" for 2A chips. A device marked 78L15 is therefore a 15V, 100mA positive voltage regulator, and one having 79M05 as the type number is a 5V 0.5A (500mA) negative regulator.

These days there are a number of improved voltage regulators that use very low supply currents or will operate with the input voltage very close to the output potential. Where a project requires a "special" of some kind, the exact requirements should be made clear in the article concerned.

With many projects now based on a special chip of some description, it is always advisable to check the article and components list for any helpful information. Do not overlook the *Shoptalk* feature when building *EPE* projects. This will always give a source of supply for any awkward or unusual components, including semiconductors.

Getting Physical

As d.i.l. integrated circuits are symmetrical it is possible to fit them the wrong way round. Doing so is likely to have dire consequences for the chip, and possibly for other components as well.

The supply pins are usually at opposite corners, so getting a device fitted the wrong way around results in it being fed with a supply of the wrong polarity. Although this is unlikely to "zap" a modern device, it is likely to cause a very high supply current to flow. Unless you switch off the project fairly quickly the device will probably overheat. Toasted semiconductors often explode with a loud "crack".

The orientation of d.i.l. i.c.s is usually indicated by a notch in what is normally considered to be the top edge of the component and (or) a dimple next to pin one (see Fig.1). There is an alternative method that is becoming increasingly common, and this is to have a white bar marked across the top end of the case. This method is particularly common amongst logic integrated circuits. Some devices take the "belt and braces approach", with all three types of marking used.

Do not be misled by moulding marks, manufacturer's logos, and other irrelevant markings on the case. Mostly these are easily distinguished from the "real thing", but some devices appear to have notches at both ends of the case! Close inspection should reveal that one notch is just a moulding mark. The real notch is usually much smaller and deeper than the moulding mark.

By no means all integrated circuits have d.i.l. encapsulations (see Fig.2). Small voltage regulators look like ordinary transistors, and the larger types have the same appearance as power transistors. Most audio power amplifier devices look like large power transistors with more leadout wires. A few devices have s.i.l. (single in-line) encapsulations. When an unusual device is used, the article concerned should always have diagrams that make the correct orientation of the component perfectly clear.

PRACTICAL RADIO CIRCUITS

RAYMOND HAIGH



Part 6: Single-sideband and direct conversion.

Circuits for the set builder and experimenter

SUPPRESSED carrier single-sideband (s.s.b.), a highly efficient method of transmitting speech by radio, will be considered this month. A popular and simple technique for receiving these signals is known as direct conversion, and a circuit is included.

CARRIERS

Radio frequency transmissions cannot, by themselves, convey information. They are no more than *carriers*, and the speech or music has to be impressed upon them by a process known as *modulation*.

The amplitude of a carrier can be varied in sympathy with a speech signal, and the process is known as *amplitude modulation*. This is the oldest and still the widest used method of transmitting speech and music by radio. It was described in Part One of the series.

If a 1000kHz carrier is amplitude modulated by a 3kHz signal, two sidebands, each 3kHz wide, are produced. The radio transmission then occupies a bandwidth of 6kHz, extending from 997kHz to 1003kHz.

Assuming a reasonable depth of modulation, some 50% of the total power supplied by the transmitter is expended on the carrier and 25% on each of the sidebands. Just one sideband is carrying all of the information in the signal. The other sideband is, in

effect, a mirror image of reverse polarity removed by the rectifying action of the detector in the receiver. With conventional amplitude modulation, around 75% of the transmitter power is, therefore, wasted. By suppressing the carrier and one of its side bands, transmitter efficiency is greatly increased and bandwidth halved.

RECEPTION

Equipment for the reception of single-sideband transmissions must include an oscillator to replace the missing carrier. When the carrier has been restored, a diode or some other non-linear detector can make the signal intelligible in the usual way.

Simple regenerative receivers are capable of resolving single-sideband transmissions if the Q-Multiplier is made to oscillate and restore the missing carrier. An Amateur Bands Regenerative Receiver was described in Parts Three and Four.

Better performance can be obtained from a mixing circuit that combines the signal and local oscillation and, at the same time, recovers the wanted audio. Circuits of this kind are known as *product detectors*. They function in the same way as mixers in superhet receivers, but the output is at audio frequencies.

A simple technique adopted by radio amateurs involves feeding signals picked up by the aerial straight into a product detector and amplifying the audio frequency output. Sometimes the signals are amplified before being passed to the detector, but the crucial feature of the technique is the direct conversion of the radio frequency transmissions to an audio frequency signal, hence the term *direct conversion*.

PASSIVE DETECTOR

Passive product detectors use an arrangement of between one and four diodes to combine the two radio frequency inputs and produce an audio output. A typical circuit diagram is given in Fig.6.2. Its operation will be described later, but the important features are simplicity, low cost, and immunity to overloading by strong signals. On the down side, the circuit attenuates the signal by about 6dB.

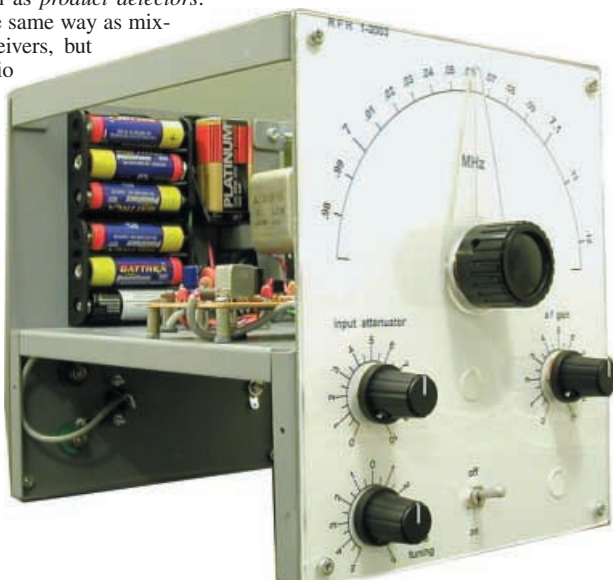
The simplest receivers place a passive detector of this kind immediately after the aerial tuned circuit. There is no amplification at radio frequencies, and a very high gain audio amplifier is needed to overcome detector losses and make the signals audible.

HISTORY

Single-sideband transmission was invented by John R. Carson, an American engineer. Initially, the technique was used to conserve channel space in carrier-current telephone systems, but, by the late 1920s, it was being deployed at low (60kHz) radio frequencies for the transatlantic telephone service.

During the Second World War, single-sideband transmitters were used, by the American forces, for long distance radio communication. The British avoided the technique, claiming it was technically too demanding for a battlefield environment, but they adopted it after the war.

American amateurs began to test the system in the 1940s, and it was taken up, by amateurs, world-wide, during the sixties. At the present time it is the standard mode of speech transmission on all of the high-frequency amateur bands.



Even when an efficient aerial is available to deliver the strongest possible signals to the receiver, results are likely to be disappointing. Moreover, the high levels of audio frequency amplification are usually accompanied by hum pick-up and microphony problems.

The microphony arises because the receiver components and wiring act as a microphone, picking up vibrations. This manifests itself as clanging and ringing sounds when the receiver is touched or adjusted, the sounds growing into howls as feedback from the loudspeaker takes over.

The situation can be improved by preceding the passive detector with a stage of radio frequency amplification. The improved gain distribution does a great deal to overcome the problems outlined above, but receivers of this kind still require high levels of audio amplification.

ACTIVE DETECTOR

An active product detector, which gives signal amplification rather than attenuation, will usually transform the performance of these simple receivers. A drawback with this arrangement is the

possibility of cross modulation being caused by overloading.

When this occurs, weak signals are modulated by strong ones within the product detector and the strong signals seem to spread across the entire band. Careful use of the receiver's input attenuator will do much to prevent this.

Unwanted envelope detection, or rectification, of powerful, amplitude modulated transmissions is a more prevalent cause of breakthrough with simple active or passive product detectors. Again, the strong signals spread across the band and cannot be tuned out.

DIRECT CONVERSION RECEIVER

A sensitive, single-sideband, amateur band set

The full circuit diagram for an amateur bands Direct Conversion Receiver is shown in Fig.6.1. A radio frequency amplifier, consisting of TR1 and TR2, precedes the product detector, TR3. The carrier replacement oscillator is TR5, its output being buffered and amplified by TR4. Audio amplification is provided by TR6 and TR7.

R.F. STAGE

Field-effect transistors, TR1 and TR2 form a cascode where TR1 is configured in the common source and TR2 in the grounded gate mode. This combination gives about 20dB of gain. Input and output impedances are high and damping on the tuned circuits, L1/C4 and L2/C5, is minimal.

Source bias to TR1 is provided by resistor R3 which is bypassed by capacitor C6. The gate (g) of TR2 is held at half the supply voltage by resistors R1 and R2, and grounded at radio frequencies by capacitor C3. The stage is decoupled from the supply rail by resistor R4 and capacitor C2.

All of the windings of coil L1 are connected in series to provide an appropriate tapping ratio for Input Attenuator potentiometer VR1. This helps to maintain the *Q* factor and selectivity of the tuned circuit. The aerial is connected to the circuit via capacitor C1, which is included to protect any preamplifiers or converters against shorting by VR1.

The tuned circuit formed by coil L2 and capacitor C5 acts as the drain (d) load for TR2, and the output is coupled to the gate (g) of TR3, the product detector, by capacitor C7.

Despite the isolation between the input and output ports afforded by grounding the base of TR2, the cascode r.f. stage is not unconditionally stable. Indeed, because of the light loading on both tuned circuits, the stage will come close to oscillation when they are precisely aligned to the same frequency.

Accordingly, resistor R5 is connected across the coupling winding L3 to provide additional damping. This increases the stability margin and the problems are avoided. When the alternative passive detector circuit (described later), given in Fig.6.2, is used, the damping imposed by the diodes and balance potentiometer serves the same purpose.

PRODUCT DETECTOR

Field-effect transistor TR3 is configured as a product detector. Signal input is to the gate, oscillator input to the source through capacitor C11, and the audio frequency output is taken from the drain.

The drain load resistor is R8 and R7, C8 and C9 decouple the stage from the supply rail at audio and radio frequencies. Source bias for TR3 is provided by resistor R9, and the d.c. potential on the gate is held at 0V by R6.

OSCILLATOR

A Colpitts oscillator, TR5, replaces the carrier suppressed at the transmitter. The capacitance tap across tuning coil L4 is formed by capacitors C20 and C21, and feedback is developed across emitter resistor R17. The stage is biased by resistors R18 and R19, and heavily decoupled by R15, R16, C14 and C15.

All sections and windings of oscillator coil L4 are connected in series to obtain the required inductance, and it is brought to resonance within the 7MHz amateur band by capacitor C22. Main tuning is by VC1, one of the 5pF to 25pF f.m. gangs of a polyvaricon tuning capacitor, and capacitor C23 reduces its swing to restrict coverage to the 7MHz amateur band.

Without some means of fine tuning, the single-sideband signals will be difficult to clarify. A shift of one or two picofarads is all that is required, and the varactor properties of an ordinary power rectifier diode, D1, can provide this.

Reverse bias (Fine tuning) is controlled by potentiometer VR2. Resistor R20 isolates the signal circuits and capacitor C24 prevents the bias being shorted by tuning coil L4. Increasing the bias reduces the capacitance across the semiconductor junction of D1.

BUFFER STAGE

The output from oscillator TR5 has to be amplified to ensure the correct operation of either the transistor or the alternative diode mixer. The oscillator also needs isolating in the interests of frequency stability.

Buffer transistor TR4 performs these functions. Oscillations are applied to its base by capacitor C16, and the stage is biased by resistors R13, R14 and R12. The output is developed across collector load resistor R11; and R10 and C10 decouple the stage from the supply rail.

AUDIO PREAMPLIFIER

The directly coupled preamplifier formed by transistors TR6 and TR7 is an adaptation of the front-end circuitry found in most high-fidelity amplifiers.

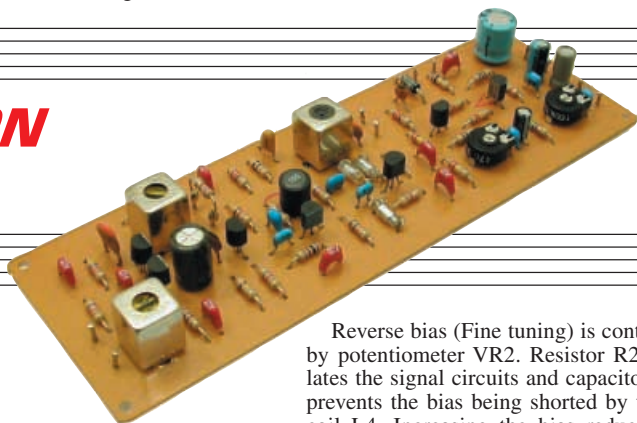
Current through TR6 is kept below 100µA by high-value collector load resistor R22 and d.c. feedback resistor R21. The low collector current reduces the noise introduced by the stage.

Preset VR3 sets the gain of the two transistor combination. The calculated value with VR3 at maximum is approximately 200, and 2000 with it turned to zero resistance.

The biasing of transistor TR7 is determined by resistors R21 and R26. The amplifier's output, developed across collector load resistor R25, is coupled to the signal feedback loop by capacitor C29, and to the Volume control potentiometer VR5 by C30. Supply line decoupling is provided by R24 and C31 and, in view of the high level of gain, is generous.

AUDIO RESPONSE

Signal-to-noise ratios are improved, and clarity increased, if the frequency response of a speech communication system is rolled off below 300Hz and above 3000Hz.



The low values of capacitors C17 and C30, and bypass capacitor C27, reduce response to the lower audio frequencies (gain reducing negative feedback, which increases as frequency lowers, is introduced because of the low value of C27). Bypass capacitors, C12, C18, and C28 curtail the high frequency response.

Signal feedback preset VR4 can be progressively shunted by capacitor C26. This increases negative feedback, and reduces gain, at the upper audio frequencies and enables the response of the amplifier to be tailored to suit individual preferences.

ON BALANCE

The active product detector depicted in the circuit of Fig.6.1 is not balanced and this makes the receiver more vulnerable to breakthrough from powerful broadcast transmissions.

An alternative, balanced arrangement is shown in Fig.6.2, where signal diodes D2 and D3 are switched in and out of conduction, by the oscillator voltage, in order to produce the desired mixing action.

To avoid confusion, it should be stressed that the silicon diodes are used here as switches and their poor performance as rectifiers of weak signals is not relevant. The oscillator must, however, be vigorous enough drive the diodes into conduction, and buffer stage TR4 ensures the delivery of sufficient power.

Balancing potentiometer VR6 optimizes immunity to the envelope detection of strong, amplitude modulated signals. Some

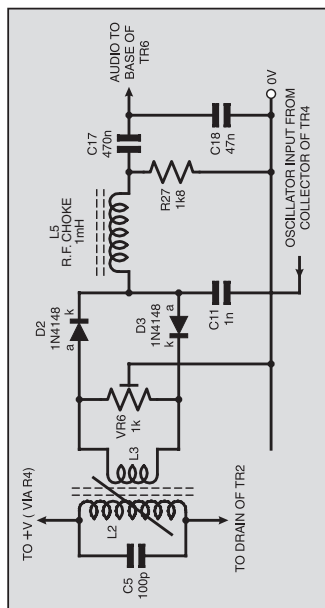


Fig.6.2. Alternative passive balanced product detector. This circuit can be substituted for TR3, the active detector, see text.

advocates of the circuit bring the potentiometer out as a panel control so that it can be adjusted to reduce break-through under varying reception conditions.

The balanced diode arrangement shown in Fig.6.2 attenuates signals by about 6dB. The active product detector included in Fig.6.1 gives about 6dB of gain. The 12dB difference is very noticeable, but readers may wish to try the balanced alternative and the increased protection against break-through that it offers.

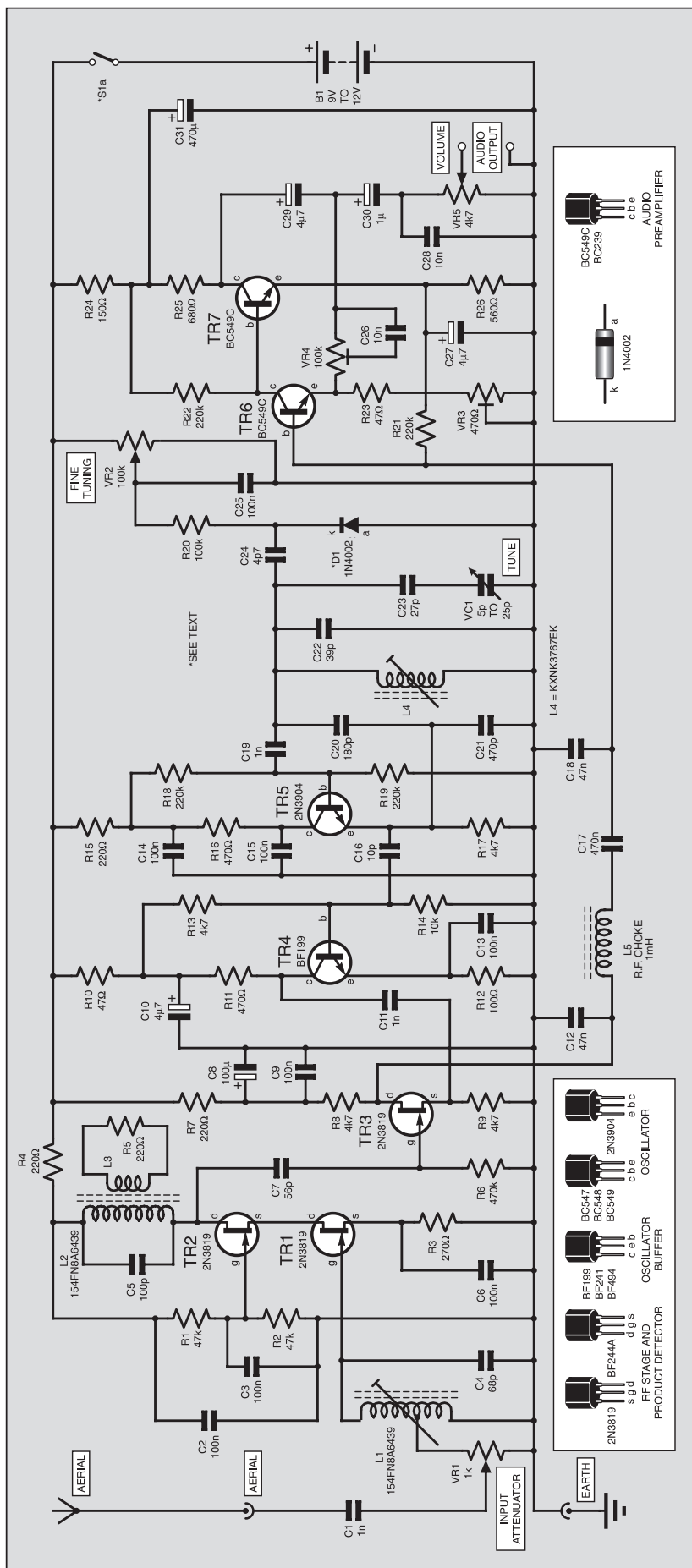


Fig.6.1. Circuit diagram for the Direct Conversion Receiver for the 7MHz (40m) amateur bands.

POWER SUPPLIES

Even small audio power amplifiers impose voltage swings on the supply rails, especially when batteries are ageing. These signal induced fluctuations can cause low frequency instability, and the receiver and power amplifier must have *separate* batteries. This is particularly important when electronic tuning bias is derived directly from the receiver battery.

Switch S1a controls the supply to the Receiver; S1b (the other half of the switch) is used to switch the amplifier battery.

COMPONENTS

Transistor types are not critical and base connections for alternative devices are shown inset in Fig.6.1. In the interests of stability, the r.f. stage field-effect transistors

should have the same lead out sequence as the specified 2N3819. Buffer stage transistor TR4 must be a small-signal r.f. type with an f_T of at least 200MHz.

Almost any small-signal *nnp* transistor in the BC107, BC108 and BC109 families, or their plastic-cased variants, should work in the oscillator and audio preamplifier stages. For best performance, TR6 should be a high-gain, low-noise device such as the BC549C.

The forward resistance of the diodes used in the alternative product detector (Fig.6.2) should, preferably, be matched with a test meter, and it will be easier and cheaper to produce a matched pair if silicon types are used. Most small power rectifier diodes can be pressed into service as a "varactor" diode for D1. Readers who prefer to use a true varactor diode should fit a BB105.

Any miniature 1mH r.f. choke will be suitable for L5. If a wire-ended component is substituted for the bobbin wound choke, mount it vertically and as close as possible to the printed circuit board.

CONSTRUCTION

Most of the components for the Direct Conversion Receiver are assembled on a single printed circuit board (p.c.b.). The tuning capacitor (VC1) has its own small p.c.b. for ease of assembly and mounting. These boards are available from the *EPE PCB Service*, codes 423 (Dir. Conv. Rec.) and 406 (T/Cap).

The Receiver topside p.c.b. component layout, together with the underside copper foil master and interwiring to off-board components, is illustrated in Fig.6.3. Solder pins, located at the lead-out points,

COMPONENTS

Approx. Cost
Guidance Only
excl. case, slow-motion drive, batt. & optional items

£25

DIRECT CONVERSION RECEIVER

Resistors

R1, R2	47k (2 off)
R3	270Ω
R4, R5, R7, R15	220Ω (4 off)
R6	470k
R8, R9, R13, R17	4k7 (4 off)
R10, R23	47Ω (2 off)
R11, R16	470Ω (2 off)
R12	100Ω
R14	10k
R18, R19, R21, R22	220k (4 off)
R20	100k
R24	150Ω
R25	680Ω
R26	560Ω
R27	1k8 (optional – see Fig.6.2 and text)

All 0-25W 5% carbon film or better

Potentiometers

VR1	1k rotary carbon, lin.
VR2	100k rotary carbon, lin.
VR3	470Ω enclosed carbon preset
VR4	100k enclosed carbon preset
VR5	4k7 rotary carbon, log.
VR6	1k enclosed carbon preset (optional – see Fig.6.2 and text)

Capacitors

C1, C11, C19	1n ceramic (3 off)
C2, C3, C6, C9, C13 to C15, C25	100n ceramic (8 off)
C4	68p ceramic "low k" or polystyrene
C5	100p ceramic "low k" or polystyrene
C7	56p ceramic "low k"
C8	100μ radial elect. 25V
C10	4μ7 tantalum bead 35V
C12, C18	47n ceramic (2 off)
C16	10p ceramic
C17	470n ceramic
C20	180p polystyrene or ceramic "low K"
C21	470p polystyrene or ceramic "low k"
C22	39p polystyrene or ceramic "low k"
C23	27p polystyrene or ceramic "low k"
C24	4p7 ceramic "low k"
C26, C28	10n ceramic (2 off)
C27, C29	4μ7 radial elect. 25V (2 off)
C30	1μ radial elect. 25V
C31	470μ radial elect. 25V
VC1	5p to 25p one f.m. gang of a polythene dielectric variable capacitor (see text)

Semiconductors

D1	1N4002 rectifier diode (see text)
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See
SHOP
TALK
page

D2, D3	1N4148 signal diode (2 off) (optional – see Fig.6.2 and text)
TR1, TR2, TR3	2N3819 <i>n</i> -channel field effect transistor (3 off)
TR4	BF199 <i>nnp</i> high frequency transistor or similar (see text)
TR5	2N3904 <i>nnp</i> low power, small signal, transistor
TR6, TR7	BC549C <i>nnp</i> small signal transistor

Miscellaneous

L1, L2/L3	154FN8A6439 Toko screened (metal can) coil (2 off)
L4	KXNK3767EK Toko screened (metal can) coil
L5	1mH r.f. choke (see text)
S1	d.p.s.t. toggle switch

Printed circuit boards available from the *EPE PCB Service*, codes 423 (Dir. Con. Rec.) and 406 (T/Cap); screw terminal for aerial and earth (2 off); slow-motion drive (optional); one large and three small plastic control knobs; audio type screened cable; multistrand connecting wire; p.c.b. stand-off pillars; front panel card and protective 2mm thick Perspex sheet; battery holder and connector; solder pins; solder etc.

Note: Case is Regenerative Radio from Part 3.

SWITCHED 3-BAND VERSION

(Component changes and additions – see Fig.6.4 and Table 6.1)

Capacitors

C20 (14MHz Band)	82p polystyrene or ceramic "low k"
C21 (14MHz Band)	180p polystyrene or ceramic "low k"
C22 (3.5MHz Band) (14MHz Band)	82p polystyrene or ceramic "low k" not required – see text
C23 (3.5MHz Band) (14MHz Band)	200p polystyrene or ceramic "low k" 15p polystyrene or ceramic "low k"
VC1 (3.5MHz Band) (14MHz Band)	5p to 130p polythene dielectric variable capacitor (one a.m. gang of specified cap.) 5p to 25p polythene dielectric variable capacitor (one f.m. gang of specified cap.)

Miscellaneous

L1, L2/3 (3.5MHz Band) (14MHz Band)	154AN7A6440 (2 off) KXNK376EK (2 off)
L4 (3.5MHz Band) (14MHz Band)	154FN8A6439 KXNK3767EK
S2	4-pole 3-way rotary switch

Note: The main circuit (Fig.6.1) and components list covers the 7MHz Band.

Also, you will need two additional main p.c.b.s (code 423) if you go for the switched-band option; but you only build the front end up to, and including, r.f. choke L5 and resistor R20.

will simplify off-board wiring, and they should be inserted first. Follow these with the tuning coils.

Next, solder in place the resistors, then the capacitors, smallest first, and, finally, the diodes and all the transistors. Semiconductor leads should be just long enough to permit the use of a miniature crocodile clip as a heatsink during soldering.

If the alternative product detector (Fig.6.2) is used, mount preset VR6 and diodes D2 and D3 on the p.c.b. solder pins connected to coil L3. Resistors R5 to R9, together with capacitors C7, C8, C9 and C12, and transistor TR3, must be removed from the board.

Failure to remove capacitor C12 will result in the oscillator output being shorted to the 0V rail. Use wire links to connect the buffer stage, TR4, to the diodes via capacitor C11, and the output from the diodes to r.f. choke L5.

SETTING UP

The printed circuit board can be tested before being mounted on a chassis or in an enclosure. First, check the placement of all of the components and examine the printed circuit board for poor soldered joints and bridged tracks.

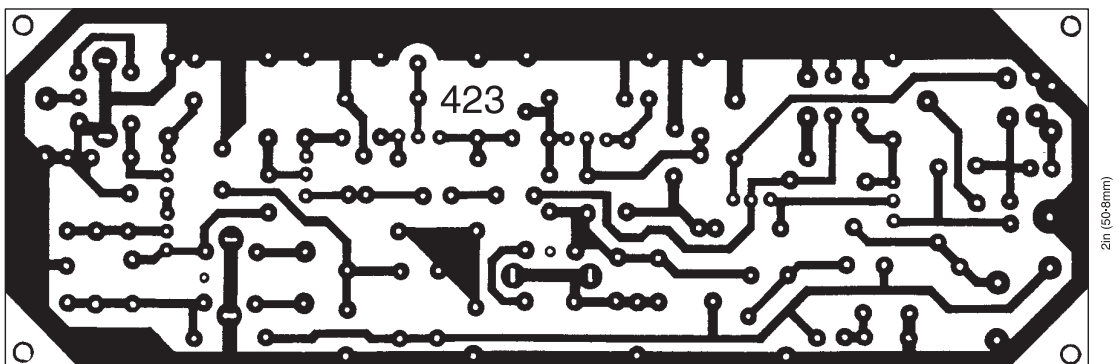
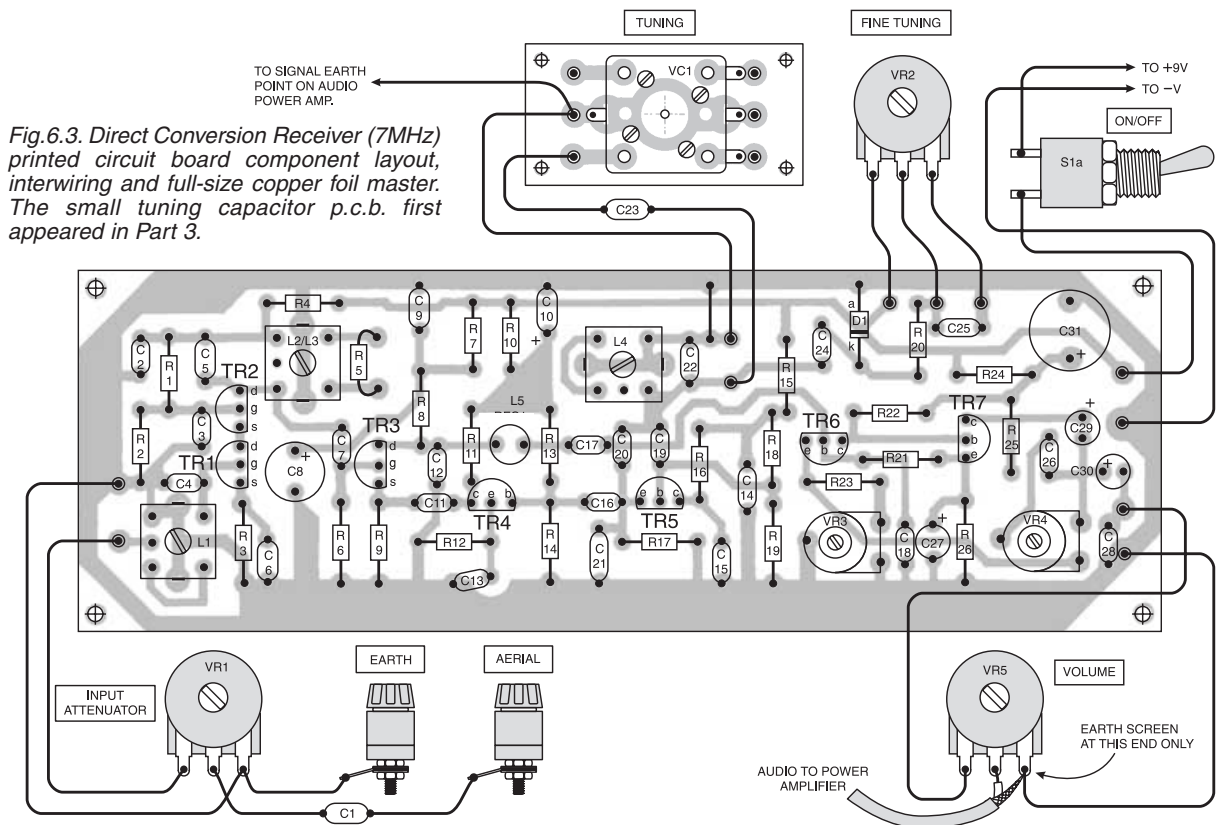
Use the leads of capacitor C23 to make the "hot" connection to tuning capacitor

VC1 and wire up the three off-board potentiometers. Connect the audio output to the Speaker Amplifier described in Part Two with *screened* cable. Receiver current consumption should be approximately 13mA with a 9V supply.

Set the cores of all of the coils about two turns down from the tops of the cans. The core of L4 is particularly brittle and a plastic trimming tool should be used for the adjustments.



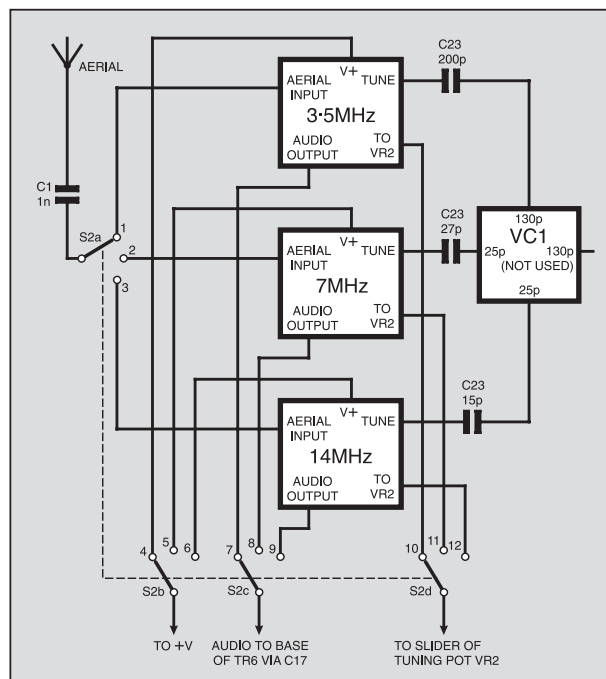
Completed circuit board for the Direct Conversion Receiver.





Receiver p.c.b. mounted on the metal chassis and wired to the tuning capacitor board.

Fig.6.4 (right). Block diagram showing switching of three p.c.b. "front-ends" to give coverage of the 80 (3.5MHz), 40 (7MHz) and 20 (14MHz) metre amateur bands. VC1 is a 4-gang a.m./f.m. variable capacitor, one gang permanently connected to each board. One a.m. gang is not connected.



Connect an aerial (at least 10 metres or 30ft of wire located as high as possible). Set input Attenuation control VR1 for maximum input and turn up Volume control VR5. There should be a faint hissing in the loudspeaker and signals should be heard if Tuning capacitor VC1 is slowly rotated and/or the core of L4 is adjusted.

ALIGNMENT WITH A RECEIVER

If you have access to a Communications Receiver, connect a short aerial wire to it and lay the wire near to the Direct Conversion set. Switch on the communications receiver's b.f.o. (beat frequency oscillator) and tune it to 7MHz.

Turn Tuning capacitor VC1 to maximum capacitance, and slowly adjust the core of L4 until a tone is heard in the speaker of the communications receiver. This receiver is, of course, picking up the signal radiated by the oscillator in the direct conversion set.

With input and volume controls turned up, rotate VC1 towards minimum capacitance. Even if tuning coils L1 and L2 are badly out of alignment, the direct conversion set should pick up some signals.

When a single-sideband transmission has been tuned in, adjust the cores of L1 and L2/L3 for maximum output. It will be necessary to turn back the Input Attenuator and the Volume control as the circuits are brought into alignment.

ALIGNMENT WITH A CRYSTAL MARKER

If a communications receiver is not available, use the simple Crystal Marker described in Part Five. Placing this unit close to the input of the direct conversion receiver will inject a 7.16MHz signal. This is just above the UK upper band limit of 7.1MHz (at the centre of the USA 7MHz to 7.3MHz allocation).

Readers in the UK should set VC1 close to minimum capacitance before adjusting the core of oscillator coil L4 until a tone is heard in the speaker. If necessary, switch the marker on and off to make sure that the correct signal has been identified. Adjust the cores of L1 and L2/3 to peak the response.

Connect the long aerial wire to the receiver, slowly turn VC1 towards maximum capacitance and tune in a single-sideband signal. Adjust the cores of L1 and L2/L3 for maximum output.

ENCLOSURE

The printed circuit board and tuning capacitor must be rigidly mounted, preferably in a diecast or aluminium box. At the very least an aluminium chassis and front panel should be provided.

The accompanying photographs show the board mounted on the chassis and front panel assembly used for the evaluation of most of the receivers in the series. This arrangement works well and microphony (feedback via the speaker) is not a problem at normal volume levels.

Keep the tuning capacitor, VC1, very close to the connecting pins on the receiver printed circuit board. Because of the provision of a fine tuning system, it is not absolutely essential to fit a slow motion drive to VC1. It will, however, make the receiver more pleasant to operate.

MULTIBAND OPERATION

Some readers may wish to extend coverage to the 3.5MHz and 14MHz amateur bands. Attempts to switch the tuning and oscillator coils are likely to result in unstable and erratic operation. A better solution is to construct three separate front-end boards. (Components up to, and including, r.f. choke L5 and resistor R20 are required.)

A block diagram of the arrangement is given in Fig.6.4, where a four-pole, three-way, rotary switch S2 connects the three boards into circuit. The aerial is switched from board-to-board by section S2a, the battery power supply by S2b, the audio output from the product detector by S2c, and the fine tuning voltage from the slider of VR2, by S2d.

The polythene dielectric tuning capacitors used in a.m./f.m. receivers have two



Completed 7MHz version of the Direct Conversion Receiver. If a 3-Band version is to be built, the band change rotary switch is mounted in the blanked-out hole just below the tuning knob.

25pF and two 130pF (or thereabouts) gangs. One of the 25pF f.m. gangs is connected to the 7MHz board, the other to the 14MHz board. The 3.5MHz front-end is tuned by one of the 130pF a.m. gangs.

Providing each board with its own variable capacitor avoids the problems associated with switching high impedance r.f. circuits. Only one r.f. lead, the aerial, is switched. This is at low impedance and can be screened without causing problems.

Connections between the tuning capacitor gangs and the three front-ends must be as short as possible. This calls for a compact arrangement of the boards around the tuning capacitor.

Aerial and audio links between the boards and switch S2 must be screened. Earth the screen at one end only: do not use it to carry the negative supply rail to the board.

Align the additional boards in one of the ways described earlier. Details of amateur

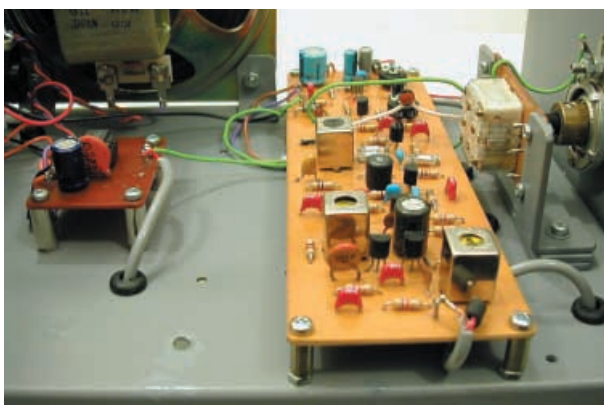
Table 6.1: Toko Coils and Tuning Capacitor Values for three popular Amateur Bands (80, 40 and 20 metre)

Band	L1	C4 (pF)	L2/L3	C5 (pF)	L4	C22 (pF)	C23 (pF)	VC1 (pF)	C20 (pF)	C21 (pF)
3.5MHz (80)	154AN7 A6440	33	154AN7 A6440	47	154FN8 A6439	82	200	130	180	470
7MHz (40)	154FN8 A6439	68	154FN8 A6439	100	KXNK 3767EK	39	27	25	180	470
14MHz (20)	KXNK 3767EK	47	KXNK 3767EK	82	KXNK 3767EK	—	15	25	82	180

Notes.

- (1) Fixed capacitors must be polystyrene or low-k ceramic types.
- (2) 3.5MHz band: the values quoted here will give coverage of the wider USA allocation.
- (3) 7MHz band: the C23 value given here restricts coverage to the UK's 7.1MHz band limit. For the wider 7.1MHz to 7.3MHz allocation, connect VC1 directly across L4.
- (4) The quoted tuning capacitor values are nominal. Measured values for the component used in the prototype receivers are: f.m. gangs, 4pF to 22.5pF; a.m. gangs, 4pF to 127pF.

A small signal r.f. transistor must be used for TR5 on the 14MHz board to maintain oscillator output at the higher frequency. Any of the r.f. types listed in Fig.6.1, together with the 2N2369, should prove suitable.



The Receiver board wired to the Speaker Amplifier (Part 2) using screened cable. These boards must have separate battery supplies.

band allocations were given in Part Four. Toko coil numbers and tuning and swing-reducing capacitor values for the 3.5MHz and 14MHz bands are given in Table 6.1.

OPERATION

Tuning has to be very carefully adjusted to transform the garbled sounds into clear speech. Fine tuning potentiometer VR2 shifts the tuning across just one or two amateur transmissions and is very useful for clarifying signals. Reception may also be improved by an earth connection.

Activity on the amateur bands varies. The 7MHz allocation was chosen for the receiver described here because plenty of signals can usually be heard during the day. When setting up the tuning on 3.5MHz or 7MHz, listen in around 10a.m., when these bands are busy. Activity on 14MHz is more variable, but the early afternoon will usually produce some signals.

Readers who have access to a frequency counter can use it to obtain a digital display of operating frequency. A buffer circuit was described last month. It should be connected, by very short leads, to the emitter of oscillator transistor TR5.

PERFORMANCE

The version with an active product detector is sensitive. Using ten yards of flex as an aerial, quite weak signals can be brought up to a good loudspeaker volume when the sim-

ple power amplifier described in Part Two is used. Gain preset VR3 will probably have to be turned well down. If the passive product detector is used, sensitivity should be adequate if VR3 is set for maximum gain.

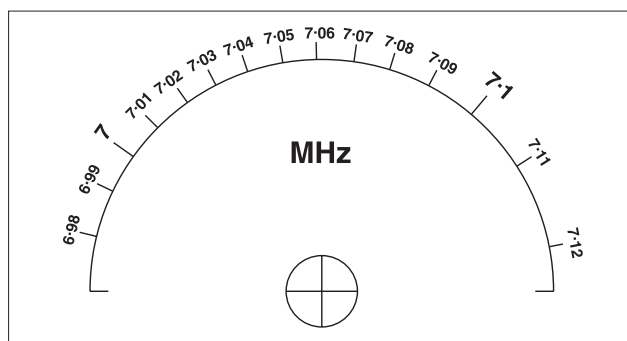
Signals are reproduced with great clarity, and the receiver is not fatiguing to listen to. After a five-minute warm-up period, frequency drift is minimal.

Unlike diodes and other devices that demodulate by a rectifying action, the heterodyning product detector will continue to function down to the lowest signal levels. In theory, therefore, the ultimate sensitivity of receivers with product detectors should be greater. In practice, received and internally generated noise are limiting factors.

The receiver cannot match the selectivity of a superhet. Its performance in this respect is similar to the Regenerative Receiver described in Part Four. When the bands are busy, the severe crowding of transmissions results in a faint background of unintelligible chattering. However, only the wanted signal is clarified, and this makes the interference less distracting.



The two separate power supply battery "packs", one for the receiver and the other for the amplifier, located on the rear panel.

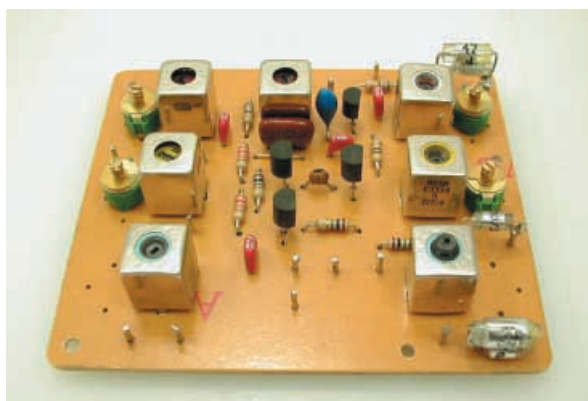


Calibrated tuning dial (half-size approx.) for the 7MHz version of the Direct Conversion Receiver.

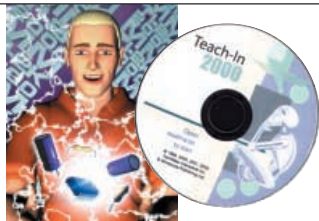
There are no discernible overloading or cross-modulation problems with either product detector. Indeed, the feature which separates this receiver from the regenerative set is its ability to cope with strong signals without the need for adjustment of the input attenuator.

Breakthrough from powerful broadcast transmitters can be a problem after dark, particularly on the 7MHz band. Careful adjustment of the cores of L1 and L2/L3 will usually clear up the problem, and refinements of this kind should be carried out during the setting up process. Keeping the signal input low will also minimize interference of this kind.

Next Month: The Superhet



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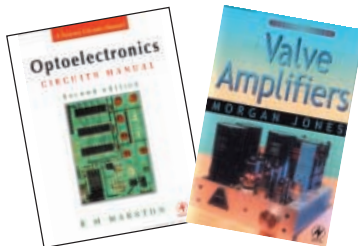
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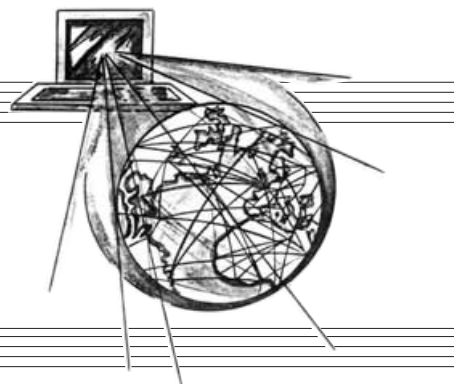
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NET WORK

ALAN WINSTANLEY



If Only I Could...

IT'S a lovely evening, and here I am, sitting in a sun lounge overlooking my quintessential English garden in the Autumnal sun, whilst typing this column into a laptop. Now, if I had broadband Internet, I could readily use the latest 802.11g wireless standards to check my email through a wireless-G router; I could browse the web through my laptop, wirelessly and with ease, ten times faster than 56K dialup, and I could search for data sheets or look through component web sites whilst online.

I could even fetch the screenshot I need for this article in a trice, and copy my text to another machine. At other times I could use a handheld computer such as an iPAQ to record some part numbers when thumbing through printed catalogues, or I could quickly hook into the vendor's online shopping cart to buy online. A simple wireless home network would allow me to fetch documents or files from the other networked computers that I use.

My thanks to Jon Rigter in Canberra, Australia, who emailed to say that "For some businesses, not being net connected and not having a web presence is suicide. We are connected to broadband here and my wife (not a techno addict) has taken to it like crazy. To the extent that we booked our Christmas (summer in Oz) holiday totally over the net. If the accommodation or attraction wasn't on the net we did not even see it no matter how nice it may have been. Any that said "We are great, please phone..." were skipped over. In one place where we recently stayed (booked over the net) the proprietor said that at least 80% of their bookings are over the net and they do not have any other contact (i.e. phone or fax) until the guests arrive."

If the advantages of broadband sound idyllic, that's because for many they are, at least for now. The phone exchanges that have been ADSL-enabled are pretty much known to their subscribers by now, and BT will probably only fill in the odd remaining gap in their network: the rest of us are on our own.

Land Grab

A huge land grab is under way amongst ISPs such as AOL, Tiscali, BT and Freeserve to sign up or switch ADSL (asymmetric digital subscriber line) users, while the rest of us have no choice but to sit it out and struggle on with dial-up Internet access. At least we are not alone in this predicament. One American correspondent in Silicon Valley talks of having similar problems with the frustrating lack of broadband, thanks mainly to the non-dynamic approach of private phone companies.

In the UK at any rate, what I feel is likely to happen in the next two to three years is this: with a huge gap in the market and BT cherry-picking ADSL customers all the time, there are a number of suppliers wanting to deliver alternative solutions such as 54mbps wireless 802.11g (one such company – WRBB – was described last month). I would like to think that some ISPs would provide broadband Internet access for philanthropic reasons, but it is debatable whether any broadband ISP would roll out a service in the hope of eventually gaining sufficient subscribers to make it viable.

Whilst some ISPs may emphasise a commitment to delivering wireless broadband "up front" regardless of initial demand, nevertheless, commercial pressures mean that there must be a certain threshold of firm demand before the service could be considered feasible to begin with. So we get back to those "pre-registration" or "expressions of firm interest" figures again.

The factor that will unlock broadband Internet access for the rest of us in the UK will be the uptake of broadband services by the public sector, including village schools and libraries etc., encouraged by Government and supported by local authorities, allied to demands from local businesses. This will form the stimulus for ISPs to develop a broadband service, probably delivered wirelessly using mesh radio or perhaps by satellite.

The market is still volatile and has yet to settle down: with satellite access for example, word from the trade is that a number of customers have thrown out satellite because it is too unreliable, but for other commercial users it may be a lifeline. If you want broadband Internet access in the regions, unless you can spare an arm or a leg for satellite services, the only solution will be to wait and see what happens. Or move to e.g. Hull.

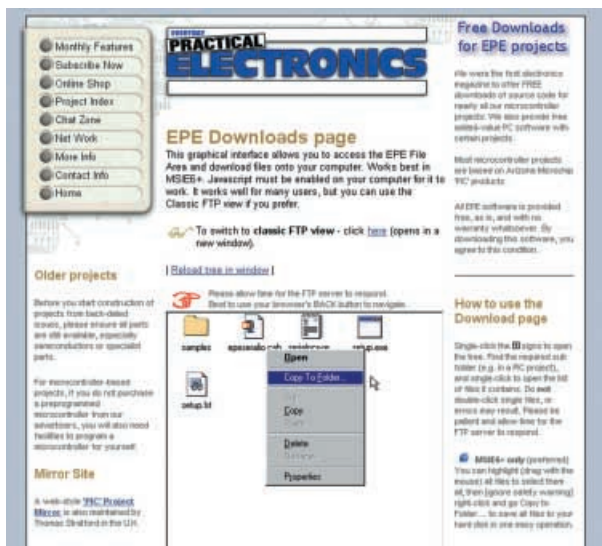
EPE Web Site Downloads

Regular users of the EPE web site (www.epemag.wimborne.co.uk) will have noticed the latest addition to our online services in the form of the new Downloads page. This is accessible using the Downloads link on the home page (half way down the left-hand side) and elsewhere. A new GUI (graphical user interface) "tree" is displayed that offers a web front-end to our traditional FTP site, where our PIC source codes are stored.

This new web page works best in Microsoft Internet Explorer 6.0. It is impossible to fully replicate in a web page the functionality of Windows Explorer that runs on a powerful PC, but the new Downloads page comes close enough and enables you to quickly navigate to the appropriate folder to fetch your source code. By clicking once on the desired sub folder, the available files are displayed. If you have the relevant applications installed (e.g. Winzip) then familiar Windows icons are displayed on our GUI page as well.

Our "tree" GUI has a trick up its sleeve: using MSIE 6, you can left-mouse-click and "drag" around the files to highlight them all; then right-click and a new option opens that may be unfamiliar to most MSIE users: simply choose "Copy to Folder..." and all the selected files will be saved to your hard disk in one slick batch operation.

The page was also tested with a number of other systems and browsers including Netscape and Opera, but the Copy to Folder... option will not be available, so files should be saved individually. A link is also provided that offers a "classic" browser view of our FTP site, should the GUI not work for you. Alternatively, you can use FTP software such as WS_FTP (www.ipswitch.com) and fetch the files by anonymous FTP instead. A number of other web pages and changes are in the pipeline, including a shopping cart upgrade. You can email comments to alan@epemag.demon.co.uk.



The new Downloads page, opened at the Serial Interface project source code. In MSIE6, select all files, then right-click and Copy to Folder to save to your disk.

PCB SERVICE

Printed circuit boards for most recent *EPE* constructional projects are available from the PCB Service, see list. These are fabricated in glass fibre, and are fully drilled and roller tinned. All prices include VAT and postage and packing. Add £1 per board for airmail outside of Europe. Remittances should be sent to **The PCB Service, Everyday Practical Electronics, Wimborne Publishing Ltd., 408 Wimborne Road East, Ferndown, Dorset BH22 9ND. Tel: 01202 873872; Fax 01202 874562; Email: orders@epemag.wimborne.co.uk. On-line Shop: www.epemag.wimborne.co.uk/shopdoor.htm.** Cheques should be crossed and made payable to *Everyday Practical Electronics* (Payment in £ sterling only).

NOTE: While 95% of our boards are held in stock and are dispatched within seven days of receipt of order, please allow a maximum of 28 days for delivery – overseas readers allow extra if ordered by surface mail.

Back numbers or photostats of articles are available if required – see the *Back Issues* page for details. We do not supply kits or components for our projects.

Please check price and availability in the latest issue.

A number of older boards are listed on our website.

Boards can only be supplied on a payment with order basis.

PROJECT TITLE	Order Code	Cost
PIC Toolkit MK3	OCT '01	318 £8.24
★ ★ PIC Toolkit TK3 – Software only	NOV '01	–
4-Channel Twinkling Lights	DEC '01	325 £6.82
Ghost Buster – Mic	326	} Set £5.78
– Main	327	
★ PIC Polywhatsit – Digital	328	} Set £7.61
– Analogue	329	
Forever Flasher	JAN '02	330 £4.44
Time Delay Touch Switch	331	£4.60
★ PIC Magik Music	332	£5.87
Versatile Bench Power Supply	333	£5.71
★ PIC Spectrum Analyser	FEB '02	334 £7.13
Versatile Current Monitor	335	£4.75
Guitar Practice Amp	336	£5.39
★ PIC Virus Zapper	MAR '02	337 £4.75
RH Meter	338	£4.28
★ PIC Mini-Enigma – Software only	–	–
★ Programming PIC Interrupts – Software only	–	–
★ PIC Controlled Intruder Alarm	APR '02	339 £6.50
★ PIC Big Digit Display	MAY '02	341 £6.02
Washing Ready Indicator	342	£4.75
Audio Circuits–1 – LM386N-1	343	£4.28
– TDA7052	344	£4.12
– TDA820M	345	£4.44
– LM380N	346	£4.44
– TDA2003	347	£4.60
– Twin TDA2003	348	£4.75
World Lamp	JUNE '02	340 £5.71
Simple Audio Circuits–2 – Low, Med and High	349	£4.60
Input Impedance Preamplifiers (Single Trans.)		
Low-Noise Preamplifier (Dual Trans.)		
Tone Control		
Bandpass Filter		
Frequency Standard Generator – Receiver	353	£4.12
– Digital	354	£6.82
★ Biopic Heartbeat Monitor	355	£5.71
Simple Audio Circuits – 3	JULY '02	356 £4.60
– Dual Output Power Supply	357	
– Crossover/Audio Filter	358	
Infra-Red Autoswitch	359	£6.50
★ EPE StyloPIC	360	£5.39
Rotary Combination Lock – Main Board	361	£4.91
– Interface Board	–	–
★ Using the PIC's PCLATH Command – Software only	–	–
Big-Ears Buggy	AUG '02	362 £5.71
★ PIC World Clock	363	£5.39
Simple Audio Circuits–4 – Low Freq. Oscillator	364	£4.44
– Resonance Detector	365	£4.28
Vinyl-To-CD Preamplifier	SEPT '02	366 £5.71
★ Freebird Glider Control	367	£4.91
★ Morse Code Reader	368	£5.23
Headset Communicator	OCT '02	369 £4.75
EPE Bounty Treasure Hunter	370	£4.77
★ ★ Digital I.C. Tester	371	£7.14
★ PIC-Pocket Battleships – Software only	–	–
Transient Tracker	NOV '02	372 £4.75
★ PICAXE Projects–1: Egg Timer; Dice Machine;	373	£3.00
Quiz Game Monitor (Multiboard)		
★ Tuning Fork & Metronome		
★ ★ EPE Hybrid Computer – Main Board	374	£5.39
– Atom Board	375	£18.87
– Atom Board	376	£11.57
★ PICAXE Projects–2: Temperature Sensor;	DEC '02	373 £3.00
Voltage Sensor; VU Indicator (Multiboard)	377	£5.07
★ Versatile PIC Flasher	378	£4.75
★ PICAXE Projects–3: Chaser Lights	JAN '03	373 £3.00
6-Channel Mains Interface	381	£5.08
EPE Minder – Transmitter	378	£4.75
– Receiver	379	£5.39
★ Wind Speed Monitor	380	£5.08
Tesla Transformer	FEB '03	382 £5.07
★ Brainbot Buggy	383	£3.00
★ Wind Tunnel	384	£6.02
200kHz Function Generator	MAR '03	385 £6.34
Wind-Up Torch Mk II	386	£4.75
★ Driver Alert	387	£6.35

PROJECT TITLE	Order Code	Cost
★ Earth Resistivity Logger	APR '03	388 £6.02
★ Intelligent Garden Lights Controller		389 £3.96
★ PIC Tutorial V2 – Software only		– –
Door Chime	MAY '03	390 £5.07
Super Motion Sensor		391 £5.55
Radio Circuits–1 MK484 TRF Receiver	JUNE '03	392 £4.44
Headphone Amp.		393 £4.28
★ Fido Pedometer		394 £4.91
★ PICronos L.E.D. Wall Clock		395 £14.65
EPE Mini Metal Detector	JULY '03	396 £4.28
Radio Circuits – 2 Q-Multiplier		397 £4.28
MW Reflex Radio		398 £4.60
Wave Trap		399 £4.28
Speaker Amplifier		400 £4.44
Ohmmeter Adaptor MkII		401 £4.60
Ultimate Egg Timer (Top Tenner)		403 £4.91
★ EPE PIC Met Office	AUG '03	402 £10.46
Alarm System Fault Finder		404 £4.44
Radio Circuits–3 Regen. Radio		405 £5.07
Tuning Capacitor Board		406 £4.28
Master/Slave Intercom (Top Tenner)		407 £4.75
Two-Up (Top Tenner)		408 £4.91
Priority Referee (Top Tenner)	SEPT '03	410 £5.07
Vibration Alarm (Top Tenner)		411 £5.39
Radio Circuits–4 Varicap Tuner		412 £4.44
Coil Pack – General Coverage		413 £5.07
Coil Pack – Amateur Bands		414 £4.75
★ PIC-A-Colour – Software only		– –
Spooky Bug (Top Tenner)	OCT '03	409 £5.07
Radio Circuits–5 Crystal Marker		415 £4.44
Super Regen. Receiver		419 £5.07
Buffer Amplifier		420 £4.44
★★ Serial Interface for PICs and VB6		416 £5.23
★ PIC Breakpoint – Software only		– –
Anyone At Home – Logic Board	NOV '03	421 }Pair £6.35
– Relay Board		422 }
Radio Circuits–6 Direct Conversion Receiver		423 £6.02
★ PIC Random L.E.D. Flasher		424 £4.60

EPE SOFTWARE

Software programs for *EPE* projects marked with a single asterisk ★ are available on 3.5 inch PC-compatible disks or **free** from our Internet site. The following disks are available: **PIC Tutorial V2** (Apr-June '03); **EPE Disk 1** (Apr '95-Dec '98); **EPE Disk 2** (1999); **EPE Disk 3** (2000); **EPE Disk 4** (2001); **EPE Disk 5** (2002); **EPE Disk 6** (Jan 2003 issue to current cover date – excl. Earth Resistivity); **EPE Earth Resistivity Logger** (Apr-May '03); **EPE PIC Met Office** (Aug-Sept '03); **EPE Teach-In 2000**; **EPE Spectrum**; **EPE Interface Disk 1** (October '00 issue to current cover date). ★ ★ The software for these projects is on its own CD-ROM. The 3.5 inch disks are £3.00 each (UK), the CD-ROMs are £6.95 (UK). Add 50p each for overseas surface mail, and £1 each for airmail. All are available from the *EPE PCB Service*. All files can be downloaded **free** from our Internet FTP site, accessible via our home page at: www.epemag.wimborne.co.uk.

EPE PRINTED CIRCUIT BOARD SERVICE

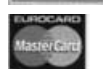
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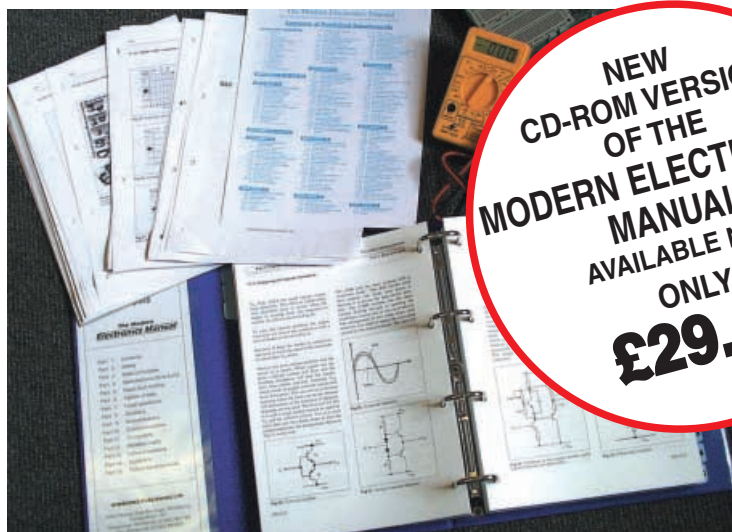
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<http://www.epemag.wimborne.co.uk/shopdoor.htm>

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